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SUBSONIC/TRANSONIC STALL FLUTTER STUDY

FINAL REPORT

by

H. Stargardter





UNITED TECHNOLOGIES CORPORATION Pratt & Whitney Aircraft Group Commercial Products Division

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16. Abstract

The objective of the Subsonic/Transonic Stall Flutter Program was to obtain detailed measurements of both the steady and unsteady flow field surrounding a rotor and the mechanical state of the rotor while it was operating in both steady and flutter modes to provide a basis for future analysis and for development of theories describing the flutter phenomenon. The program revealed that while all blades flutter at the same frequency, they do not flutter at the same amplitude, and their interblade phase angles are not equal. Such a pattern represents the superposition of a number of rotating nodal diameter patterns, each characterized by a different amplitude and different phase indexing, but each rotating at a speed that results in the same flutter frequency as seen in the rotor system. Review of the steady pressure contours indicated that flutter may alter the blade passage pressure distribution. The unsteady pressure amplitude contour maps reveal regions of high unsteady pressure amplitudes near the leading edge, lower amplitudes near the trailing edge, and nodes near the mid chord position. This pattern implies that the work input is concentrated near the leading edge, and that this is the region where design changes would have the greatest potential for preventing flutter. Review of the data shows that the location of the flutter boundary appears to correlate with blade incidence and loading parameters. Steady-state blade deformations were found to agree well with the NASTRAN predictions except that the blade uncambering slightly exceeded the predictions.

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PRECEDENCE PACE DESCRIPTION

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SECTION 1.0

SUMMARY

The objective of the Subsonic/Transonic Stall Flutter Program was to obtain detailed measurements of both the steady and unsteady flow field surrounding a rotor and of the mechanical state of the rotor while operating in both steady and flutter modes. The data were obtained to provide a basis for future analysis and for development of theories describing the flutter phenomenon.

This objective was met using the Pratt & Whitney Aircraft TS22 research fan stage, which was extensively instrumented with high response rate instrumentation and a laser optical system. The stage was tested over a range of operating conditions both in and out of flutter.

A significant result of the program was a new conceptual understanding of the mode of flutter in the rotor system. Previously, fan flutter had been characterized by a single flutter frequency with all blades fluttering with similar amplitudes and equal interblade phase angles. The current program revealed that while all blades flutter at the same frequency, flutter amplitudes are not similar and interblade phase angles are not equal.

The steady pressure contours indicated that flutter may alter the blade passage pressure distribution.

The contour maps of unsteady pressure amplitude revealed regions of high amplitudes near the leading edge, lower amplitudes near the trailing edge, and nodes near the midchord position. This pattern implies that the work input is concentrated near the leading edge. Design changes in this region should, therefore, have potential for preventing flutter.

The data shows that the location of the flutter boundary correlates with blade incidence and loading parameters and is influenced by relative Mach number.

Steady-state blade deformations agreed well with the NASTRAN predictions except blade uncambering exceeded predictions slightly.

SECTION 2.0

INTRODUCTION

Flutter is an aerodynamically self-excited vibration in fan, compressor, and turbine blades. It can cause blades to fail and is of major concern.

The Subsonic/Transonic Stall Flutter Program, an experimental investigation, provided data for use in the formulation of analyses for predicting the onset of stall flutter in high-speed, axial-flow compressors.

The specific objective of the program was to obtain detailed measurements of both the steady and unsteady flow field surrounding a rotor and the mechanical state of the rotor while the rotor operated in the steady and flutter modes. This required testing and detailed performance mapping of a stage known to experience subsonic/transonic stall flutter. The Pratt & Whitney Aircraft TS22 stage met this requirement.

A substantial body of data was obtained. The testing and detailed mapping provided overall and blade element aerodynamic performance, information about the instantaneous flow field entering, passing through, and leaving the rotor, and information on the mechanical state of the rotor blades.

Performance and dynamic data were taken for 16 data points. These data have been used to evaluate the flutter boundaries and to determine details of the flow between blades in both the stable and flutter regimes. Blade stress and deflection data have been studied to evaluate analytical blade deflection prediction techniques for steady state operation and to determine mode structure during flutter.

Sections 3.0, 4.0, and 5.0 of this report describe the program approach, the facility and equipment used, and the data acquisition and reduction procedures. The results of the program in terms of new understandings of the flutter phenomenon are presented in Section 6.0, discussed in Section 7.0, and summarized in Section 8.0. Recommendations for future work are given in Section 9.0, and References are identified in Section 10.0.

The full set of data obtained under the Contract is provided in the appendix. Rotor overall performance and blade element performance are presented in Appendix A. Rotor blade coordinate data, in Appendix B. The steady-state and dynamic data, organized by instrument type, are presented in Appendices C, D, and E.

SECTION 3.0

PROGRAM APPROACH

The TS22 test stage selected for this program had aerodynamic and structural characteristics representative of an advanced fan stage and had exhibited stall flutter at intermediate speeds during prior testing.

Performance data were obtained by means of an automatic data acquisition system coupled with a numerically controlled probe traverse system directly linked to a Sigma 8 computer. The instrumentation for measuring steady-state deflections and flutter characteristics of the rotor blades consisted of strain gages, an optical mirror system, and a speed signal. NASTRAN was used to calculate steady-state deflections.

Kulite pressure transducers were used to measure the pressure fluctuations on the case over the blade tips and on the airfoil surfaces. Traversing hot-film probes measured the time fluctuations of the local mass flow entering and leaving the test rotor. Two traversing probes were installed at each location to provide instrumentation backup. Hot-film anemometers located on the blade surfaces were intended to characterize the unsteady flow over the blades as laminar, turbulent, or separated and to determine the instantaneous location of shocks and separation.

The tests covered a range of flows at speeds from 55 to 85 percent of design. Overall performance and detailed blade element data for the rotor were calculated for 11 16 data points. Detailed structural and dynamic data were calculated for six selected points. Steady-state rotor blade deflections, measured by the optical mirror system data were compared with the deflections calculated using NASTRAN. The unsteady mode shapes, deflection amplitudes, and phase relationships during flutter were determined from the case mounted Kulites, strain gages, and mirror data.

Stability calculations were made for several mode shapes. Pressure distributions over the blade tips were analyzed to determine shock locations and loading changes that occurred as speed and flow were changed. Real and imaginary components of unsteady pressure during flutter were determined as were phase relationships of unsteady pressures. Unsteady velocities into and out of the rotor were determined, and the relative amplitude and phase relationship of unsteady velocities on the blade surfaces were established. The reduced velocity parameter and incidence angle based on measured flow and metal angles were determined.

4.0 TEST FACILITY AND EQUIPMENT

4.1 TS22 FAN RIG DESCRIPTION

The TS22 fan rig combined moderate tip speed with a high pressure ratio, high flow rate per unit annulus area, and good efficiency. The 3.6 blade aspect ratio was aeroelastically aggressive even with a single partspan shroud. The stage, with its 81.8 cm (32.21 in.) rotor tip diameter, was large enough to permit good definition of the unsteady flows, blade deflections, and mode shapes during flutter.

The TS22 rig is schematically represented in Figure 1. Stage design parameters are listed in Table I, and rotor blade specifications, in Table II. Measured vector diagram data and additional performance data are given in Appendix A. Blade coordinates are given in Appendix B.

New rotor blades were obtained for this study in order to minimize the potential of fatigue failure, the original TS22 rotor having operated for many hours in the flutter region. The new blades were inspected and found to be within allowable tolerances. Blade leading and trailing edge angles were determined. The maximum, minimum, and average edge angles at fourteen span locations are compared with design values in Tables III and IV.

The second mode bending frequency of the isolated blades was considered to be representative of blade flutter frequencies. Therefore, the second mode frequency with clamped root and unrestrained shrouds was measured for each of the thirty-two rotor blades. The minimum measured frequency was 241 Hz; the maximum, 249 Hz. The blade positions in the rotor (Figure 2) were selected to minimize differences in frequency between adjacent blades and provide a smooth frequency variation around the rotor.

4.2 TEST STAND DESCRIPTION

The tests were conducted in the X-204 test stand at Pratt & Whitney Aircraft's Willgoos Turbine Laboratory in East Hartford, Connecticut. This stand, shown in Figure 3, consisted of a test section with inlet air and exhaust systems, a drive motor, a computerized supervisory control system with numerous safety devices, a computerized data acquisition system, and a variety of test supporting systems.

The airflow entered the rig through a calibrated orifice and a large-diameter plenum chamber. A wire mesh screen and an "egg crate" structure upstream of the plenum provided a uniform inlet pressure profile to the compressor. Airflow was exhausted into a toroidal collector through a back-pressure valve to the exhaust blowers.

The compressor drive was a variable-speed electric motor connected to the test compressor through a speed-increasing gearbox. Electric power for the drive motor was provided from the laboratory powerhouse by four variable-speed, variable-frequency generators driven by a 6000-hp steam turbine.

4.3 INSTRUMENTATION AND DATA ACQUISITION SYSTEM

Instrumentation provided full documentation of both steady-state and nonsteady aerodynamics and for rotor structural behavior in and out of flutter. The location of instrumentation is shown in Figures 4 and 5. Table V lists the instrumentation and readout systems.

A fully computerized steady-state data acquisition was used during testing. Data were transmitted to a computer located at the control room and then to an automatic data reduction computer which performed a preliminary data reduction and returned the results to the control room. These preliminary data were used to direct the test program. Positioning and readout of all the traverse probes at the rotor inlet, rotor exit, and stator exit were controlled by the rig automatic traverse system.

The steady-state data acquisition system for the stand recorded 232 channels of rig data: 131 pressure channels, 78 temperature channels, and 23 miscellaneous millivolt channels. This system worked in conjunction with a high-response-rate system that recorded the data from the Kulite pressure transducers, hot films, and strain gages.

Unsteady data recording systems for the Kulites, hot films and strain gages recorded a common 1:1 speed signal, common time code, and a common strain gage signal. Before start of testing, a common sine wave and a white noise signal were recorded on all system channels in order to determine frequency and phase response.

Data from the blade mirror system were recorded on still photographs, movie film, and video tape.

4.3.1 Steady-State Aerodynamic Instrumentation

Wedge probes measured total pressure, static pressure, and air angle. Combination probes measured total pressure, static pressure, air angle, and total temperature. Wall taps were used for measuring wall static pressures, and total pressure rakes were used for measuring stator exit total pressures.

Pressures for steady-state operation were measured by a system of scanning valves and 24 pressure transducers with various pressure ranges. Pressure readings were distributed among the transducers to maximize measurement accuracy. Forty close coupled transducers were used to monitor surge. The temperatures were measured in millivolts as differentials from a reference temperature and recorded by the automatic data acquisition system.

4.3.1.1 Pressure

The pressures sensed by the probes, fixed rakes, and static taps were measured by transducers and recorded in millivoits by the automatic data acquisition system. Pressures from sensors upstream of the rctor trailing edge were measured by means of $10.3~\text{N/cm}^2$ ($15~\text{lbf/in.}^2$) full-scale transducers. Pressures from the trailing edge of the rotor and all downstream locations were measured using $34.6~\text{N/cm}^2$ ($50~\text{lbf/in.}^2$) full-scale transducers. The accuracy of the pressure measurements was $\pm 0.1~\text{percent}$ of full-scale value.

4.3.1.2 Temperature

All temperatures were measured with Chromel-Alumel, type-K thermocouples connected to reference junctions attached to uniform temperature reference blocks located in the test cell. The temperatures of these reference blocks were monitored relative to ice-point cells located in the data system room. The resulting data were recorded in millivolts by the automatic data-acquisition system.

Temperature elements were calibrated for Mach numbers over their full operating range. The thermocouple leads were calibrated for each temperature element. Overall rms temperature accuracy was estimated to be $\pm 0.56 \text{K}$ (1.00R).

4.3.1.3 Rotor System

Compressor speed was measured using an impulse-type pickup, which counted gear teeth passing in an interval of time. The data were recorded through a frequency-to-DC converter. Accuracy was +1 rpm.

4.3.1.4 Airflow

Airflow was measured with an orifice calibrated to International Standards Organization/DIS 5167 Standards. Total pressure was measured using a 10.3 $\rm N/cm^2$ (15.0 lbf/in.²) full-scale transducer. Orifice pressure drop was measured using 3.4 $\rm N/cm^2$ (5.0 lbf/in.²) full-scale differential transducers. Orifice temperature was measured by the standard temperature measurement system. Accuracy of the airflow measurement was within one percent.

4.3.2 Structural Instrumentation

Blade deflections were measured by a mirror system consisting of a laser light source, a beam splitter, reflecting mirrors and a screen and were recorded by a video and camera system. Steady state and unsteady deflections were recorded using the techniques described in reference 1 and 4.

One strain gage was placed on each blade to measure unsteady stresses and to detect the onset of flutter. Signals from these gages were transmitted through a slipring and recorded on magnetic tape.

4.3.2.1 Optical Mirror System

It was necessary to accurately measure rotor blade deflections both in and out of flutter. During stable operation these deflections were due to centrifugal and aerodynamic forces. When in flutter vibrational mode shapes had to be determined. A patented system (reference 4) of optical mirrors and reflected laser light was used to measure rotor blade surface angle changes from which blade deflections were determined.

The optical mirror system consisted of an array of mirrors installed on the blades, a laser light source, and a readout and recording system, shown schematically in Figure 6. The laser light was split into a number of beams, each directed to the radial location of one of the mirrors. As the instrumented blade rotated through the beams, the mirrors reflected the beams back to the readout system to separate points that had been selected to avoid pattern interference during flutter.

Twenty mirrors were installed on one blade to provide full coverage of the blade in the region above the midspan shroud and along the leading edge below the shroud. Additional mirrors were mounted on other blades. The complete array of mirrors is shown on Figure 7. Circumferential locations of instrumented blades are shown in Figure 5.

The mirrors were made from silicon wafers 0.244 cm (0.10 in.) square, 0.024 cm (0.0095 in.) thick, sputtered with a 1000-angstrom thick coating of aluminum and over-coated with 2280-angstrom protective coating of silicon dioxide. The mirrors were attached to the blades with epoxy cement. Additional details of the mirror system and mounting techniques are given in reference 1.

The laser light and mirror system for measuring the instantaneous blade surface positions used a 604.5 cm (238.0 in.) optical path directly upstream of the test stage inlet. This path length was sufficiently large to provide adequate light spot deflections for accurate data readout.

Two windows were installed in the inlet section walls of the test facility: one to provide laser light entry; the other to provide a screen for receiving the reflected light beams. The entry port was a 35 cm (12 in.) diameter clear glass window. The exit port was a 50.8 cm x 175 cm (20 in. x 69 in.) semicircular piece of frosted 3.81 cm (1.5 in.) thick Lexan, located 604.5 cm (238.0 in.) upstream of the rotor. The output window was centered about the horizontal plane.

Inside the plenum chamber, the slipring cable container was braced near the rotor at the 12, 3, 6, and 9 o'clock positions. The light was directed to avoid these blockages. The interior of the inlet was frosted in selected locations to prevent secondary reflections from interfering with the laser beam signal.

Two lasers were used simultaneously: a 0.5-watt Hughes provided the reference beam and a 3-watt Spectraphysics provided illumination for the mirrors.

Edmund Scientific variable beam splitters were adjusted to ensure an approximately equal intensity of all the light beams. Each splitter was mounted on a five axis adjustment system to facilitate accurate aiming of the light beams. Glass shims 0.3175 cm (0.125 in.) thick were added to each splitter to block second order images.

The optical data were recorded with a movie camera operating in the streak mode, a Hasselblad still camera, and a television camera. The cameras were placed to receive the maximum scattered light when the beams were on the output window. The cameras were located 9.14 m (30 ft) from the screen. An oscilloscope beneath the output window was photographed simultaneously with the light spots to correlate the time code and rotor speed signals with the mirror deflections. All cameras were rigidly mounted to eliminate blurring due to camera vibrations.

The accuracy of the laser optical system was limited by the resolution of the film. The negative film was Kodak 2484, chosen on the basis of the relative spectral sensitivity, grain size, and contrast. Two copy films for the movies were used: Kodak Hi Con 7362 and Kodak black and white fine grain positive 7302. The former provided the best results, producing more contrast and a much finer grain. The optimum processing speed for the negative was 6.1 m/min (20 ft/min). For the copy, a speed of 10.7 m/min (35 ft/min) was used. Both were processed in Kodak D96. The 2484 film had an ASA number of 800, and the print machine speed and print exposure times were selected to produce a print base density of two. These machine speeds and print exposure values were determined with the actual film and the illumination conditions existing at the time. Uneven copy-process illumination was detected with image processing laboratory equipment and corrected during processing. Still pictures were taken on Kodak Tri-X film.

4.3.2.2 Strain Gage Instrumentation

To ensure safety and measure the response of all blades in flutter, one Micro-Measurements type WDDY-125AD-350 strain gage was installed on each rotor blade immediately above the shroud at the midchord location since this location was sensitive to the second coupled mode expected in flutter.

The frequency response of the strain gage data was limited by the bandwidth of the data recording system. The accuracy of any given strain gage was statistically determined to be approximately +5 percent, representing one standard deviation for typical data.

4.3.3 <u>Unsteady Aerodynamic Instrumentation</u>

The instrumentation for measuring unsteady aerodynamic effects included: 1) Kulites on the case over the rotor blade tips, 2) an array of Kulite high response pressure transducers on the rotor blades, 3) traversing hot-film probes at the inlet and exit locations of the rotor, and 4) an array of hot-film anemometers on the rotor blades.

The fan-case Kulites and the hot-film probe outputs were recorded on two Sangamo III wide band group I FM tape recorders having a capacity to 40 kHz center frequencies and 40 kHz output filters. In addition to the data signals, 60:1 and 1:1 speed signals were recorded along with 1 kHz IRIG B Format Time Code Signal.

Data from all blade-mounted Kulites were recorded on a constant bandwidth frequency-division multiplex system, which provided a frequency response of 2 kHz with a resolution of 690 N/m 2 (14.4 lbf/ft 2) and an error no greater than \pm 1 dB. Each of the 12 tracks on the system recorded six data signals plus a time code signal. One data channel on each track was used to record a reference strain-gage signal for phase determination. The hot-film anemometer data were also recorded on this multiplex system.

4.3.3.1 Case Mounted Kulites

Ten high response Kulite pressure transducers, Kulite Model XCQL-8B-808 mounted over the blade tips (Figure 8), were used to measure unsteady pressures over the blade tips during stable and during flutter type operation. Specifications for these units are given in Table VI.

4.3.3.2 Blade Mounted Kulites

Thirty-two Kulite, high-response pressure transducers were distributed over the pressure and suction surfaces of four blades (Figure 9) instrumented in pairs such that the instrumentation ocations on the suction surface of one blade matched those on the pressure urface of the adjacent blade across the flow channel. Kulite Model LQL5-080-15S transducers were used on the blades. Transducers specifications are shown in Table VI. The data from these transducers provided detailed mapping of he pressure fluctuations during flutter.

Signals from the rotating Kulite transducers were amplified before passing through the slipring to the recording device. An amplifier package was used which rotated with the rotor assembly.

The rotating Kulite pressure transducers were calibrated both before and after mounting on the blade surfaces. The accuracy of the calibration facility was 0.1 percent full scale over a range of zero to 345 N/cm 2 (500 lbf/in. 2).

4.3.3.3 Hot Film Anemometers

Traversing hot-film probes, located at the inlet and exit of the rotor, measured fluctuations in inlet and exit flow during stable and flutter operation. Hot-film anemometers were located in the rotor blades to characterize the flow over the blade surfaces in and out of flutter and during transition from stable flow to flutter.

Two hot-film probes were located forward of the rotor, and two behind the rotor. The sensors were oriented with their length tangent to the case and perpendicular to the rig axis.

Thermo-Systems Model 1210-60 cylindrical hot films were chosen for the probes based on their ability to operate in a high velocity gas stream. These sensors were constructed of a 0.0154 cm (0.006 in.) diameter by 0.203 cm (0.080 in.) long quartz substrate with a platinum sensor deposited on its surface. Specifications for the transducers are presented in Table VI. The hot-film probes were calibrated at ten different flow velocities.

The frequency response of the probes and the associated data acquisition system was 40 kHz with a resolution of 1.0 percent of the mean flow velocity. The dynamic accuracy of the probes was 1 dB for axial Mach numbers below 0.4. The accuracy at higher Mach numbers was less because of a loss in sensor linearity caused by flow compressibility.

Twenty hot-film sensors were installed on four blades above the shroud at positions corresponding to those of the blade-mounted Kulite pressure transducers, Figure 10. A majority of sensors were installed on the suction surfaces of two blades to provide data of flow separation. A few were also placed on the pressure surface.

The sensors were Micro-Measurements Type EGT50. The film with its polyimide backing was mounted on a 0.041 cm (0.016 in.) Kapton film substrate to minimize heat transfer to the blades. The grid was oriented in the direction of flow with the leadwires routed off the trailing edge to avoid an additional turbulence source.

The sensors were calibrated to identify strain induced errors, but their non-linear response and the difficulty in simulating the test situation in the laboratory made calibration to obtain quantitative data unrealistic. Therefore, their function was limited to qualitative characterization of the flutter. However, comparing the flutter response from one data point to another gave useful data on suction surface nonsteady flow characteristics. These sensors and associated data acquisition system provided a frequency response to 2 kHz.

SECTION 5.0

TEST AND ANALYSIS PROCEDURES

5.1 TEST PROCEDURES

The test program was conducted in two phases: an initial shakedown test phase and a performance test phase. The objectives of the shakedown test were to check rig operation, instrumentation, and data recording and reduction systems; to verify the existence of stall flutter; and to compare performance with that of the original TS22 stage. During the performance test phase, overall aerodynamic performance with the obtained over a range of flows at rotor speeds between 54 and 85 percent of cign. High response aerodynamic and structural data were obtained at all operating points, and surge points were determined at several speeds between 63 and 85 percent of design.

5.1.1 Shakedown Tests

During the shakedown test the rig was operated at speeds to 70 percent along a wide-open-discharge throttle line to make sure that the rig was free of vibration and that all steady-state and dynamic instrumentation were operating properly. A transient into flutter was made at 70 percent speed. A full data point was taken with both steady-state and dynamic instrumentation at 70 percent speed and wide open discharge. At 63 percent speed a transient into flutter was made, and two additional data points were taken: one with wide-open-discharge; the other in flutter. These shakedown tests are listed on Table VII.

The full data points consisted of:

- O A two-minute record of all dynamic instrumentation-strain gages, Hot films, and Kulites
- A two-second high-speed motion picture of optical laser/mirror data for all blade mirrors
- Still photographs of mirror data
- o TV records of all mirror images
- o A two-minute record at each spanwise location of a seven-position radial traverse made ahead of and behind the rotor with hot-film probes
- Steady-state data including rotor speed, total pressures, total temperatures, flows, static pressures, and flow angles for the rotor and stator inlets and discharges.

The aerodynamic data obtained during the shakedown tests were reduced to vall-date the instrumentation and data reduction systems and to compare performance with the performance observed during previous tests of the TS22 stage. The dynamic data were studied to validate accuracy before the performance phase of the test program.

5.1.2 Performance Tests

The performance testing phase of the program involved mapping the extent of the flutter boundary by taking data at operating conditions both in and out of flutter. The initial portion of this phase repeated some of the shakedown testing. Test data was taken over a range of speeds from 54 to 85 percent of design. The test points are listed in Table VII. For this program the flutter boundary was defined as the flow at which a vibratory stress of $\pm 2068 \text{ N/cm}^2$ ($\pm 3000 \text{ lbf/in.}^2$) was attained.

5.2 DATA REDUCTION PROCEDURES

5.2.1 Data Requirements

The following parameters were calculated for all data points:

- 1. Overall stage performance
- 2. Blade element performance
- 3. Blade untwist and uncamber
- 4. Flutter frequency
- 5. Blade stress level
- 6. Vibratory mode
- 7. Pressure contours over the blade tips
- 8. Incidence angle at seven radial stations
- 9. Reduced velocity for seven radial stations.

In addition more extensive data reduction was performed for six of the data points. This reduction provided:

- 1. Analysis of the mirror data for intrablade amplitudes and phase relations on one blade correlated with strain gage signals and other non-steady signals to define the rotor mode shape and its relationship with the instaneous aerodynamics
- Intrablade average steady pressure distribution at the wall for two passages

- 3. Intrablade unsteady pressure distribution at the wall for two passages
- 4. Amplitude and phase angles of all fluctuating signals from rotor-mounted sensors--both amplitude and phase angle were determined relative to the signals from the No. 3 blade.

5.2.2 Specific Procedures

5.2.2.1 Steady-State Aerodynamic and Blade Deflection Data

All steady-state performance data were automatically recorded in millivolts, converted to engineering units, corrected, and used to calculate overall and blade element parameters.

The measured total pressure and flow angle from the wedge probes were corrected using Mach number calibration curves for individual probes. The resulting calibrated Mach number and corrected total pressure were then used in conjunction with standard tables of air properties to calculate static pressure.

Thermocouple signals were converted to temperature measurements using wire calibrations for individual sensors. These temperature measurements were converted into total temperature using Mach number calibrations for individual sensors and the pressure-level corrections of Glawe, Simms, and Stickney (ref. 2).

Circumferential distributions of total pressure obtained at the stator exit were mass-flow averaged for each pole rake at each radial location using the corresponding measured distribution of total temperature and a constant circumferential static pressure determined by linearly interpolating static pressure data from wall static measurements. Circumferential mass-flow averages of total temperature were also calculated at each radial location, using the corresponding measured distribution of total pressure and constant circumferential value of static pressure. The three values of total pressure from the pole rakes at each radial location were arithmetically averaged to obtain a single radial distribution of stator-exit total pressure. Total temperatures were averaged similarly. The peak value of total pressure from each circumferential distribution of total pressure was taken as stator inlet pressure. The three radial distributions of stator inlet pressure were also averaged to obtain a single radial distribution. Air angles measured by the two probes at the stator exit were arithmetically averaged for each radial location.

Two separate computer programs were used to transform test measurements into the desired overall and blade-element performance parameters. The first computer program converted measurements from millivolts to engineering units and corrected, averaged, and prepared the data for input to the second computer program. The second computer program, operating off line, calculated the desired overall and blade-element performance parameters by means of a stream-line solution of the axisymmetric flow field.

The remaining input to the flow field program consisted of the geometric description of the rig and aerodynamic data. The geometric description included the shape of the flowpath walls, axial locations of blade edges, and blade inlet and exit metal angles and solidity. Blade edges were input as 24 straight-line segments that closely approximated the meridional profile of the manufactured blade edges. Metal angles at the rotor leading edge and trailing edge were input from beam calculations for the blade at design speed.

The output from the second program consisted of corrected speed and inlet flow; the spanwise profile of total pressure ratio at the stator inlet; the spanwise profiles of total pressure ratio, total temperature ratio, and flow angle at the stator exit; and blockage factors for each calculation station. Total pressures and temperatures were calculated as ratios to the assumed standard day inlet plenum values.

A flow blockage factor was used at each axial location to improve the accuracy of the static pressure velocity calculations. Blockages were applied equally to all stream tubes at each of the axial locations. The axial distribution of blockage factors was selected to give calculated wall static pressures that agreed with measured wall static pressures. A single axial distribution was found to provide reasonable agreement with measurements for all data points.

All static pressures and the flow angles between the rotor and stator were calculated by the flowfield program. The calculation was made assuming a symmetric flow and using mass-flow continuity, radial equilibrium, and energy equations. Streamline curvature and enthalpy and entropy gradient terms were included.

Overall rotor performance was calculated from mass-flow averages of tota pressure and temperature at rotor exit and average inlet conditions. Overall stage performance is not presented in this report because it is not required to support data evaluation.

Rotor blade element parameters were calculated for airfoil sections lying on a fixed set of conical surfaces defined by intersections of blade edges and streamlines calculated for a reference point at mid range at 75 percent speed. Streamlines were selected to include blade-element data at radial locations of transducers for blade surface measurements and mirrors for blade deflection measurements. For the blade element data tabulations presented in Appendix A, the incidence angles were based on measured air angle and the calculated netal angle at design speed. For the plot of reduced velocity parameter versus incidence angle (Figure 43), both air angle and metal angle were measured values.

The blade centrifugal untwist and uncamber resulting from centrifugal and gas bending loads were determined directly from the blade deflection data obtained with the optical mirror system. Images from twenty of the twenty-six blade mounted mirrors were used to determine blade movement.

Steady deflections were determined for speeds from 25 percent to 85 percent of design. Photographs taken at selected speeds in nine percent increments were used to determine steady blade movement. A coordinate system was established based on known details of the screen. The vertical position of each spot on each photograph was measured. Using the idle spot positions as a baseline, the movement of the spots for any speed was scaled. This movement on the screen was then converted to angle of twist and change in bending slope.

5.2.2.2 Unsteady Data Reduction

The reduction of the high frequency response data from the hot film probes, wall-mounted Kulites, blade mounted hot film sensors, blade mounted Kulites and blade mounted strain gages required sophisticated techniques. Signal enhancement, signal phasing from rotating instruments, and signal phasing between rotating and stationary instruments are discussed below. These discussions are followed by details of the analysis of each type of data.

5.2.2.2.1 Signal Enhancement

The signal enhancement, a time domain technique, extracted or enhanced particular frequency components from a broadband signal. The technique involved averaging numerous time segments of a broadband signal, the start of each segment being triggered by a reference signal. Each successive time segment was summed and averaged in a storage memory. The result was an enhancement or reinforcement of those components that were synchronous with the triggering signal and suppression of components that were not.

5.2.2.2 Phasing of Signals from Rotating Instrumentation

Phase information between the reference strain-gage signal on the No. 3 blade and all other strain gage and rotating Kulite and hot film signals was produced at the flutter frequency, using cross spectral density techniques, a Nicolet Scientific "Omniferous" Model 401 analyzer being used for this purpose. The analysis range for the task extended to 2 kHz. An 800-element spectural resolution was selected. To produce each final plot, 128 sweeps from the analyzer were averaged. The analysis was conducted from zero to 2000 Hz. The analyzer filter bandwidth yielded a spectral resolution of about 3.75 Hz. All resulting phase angles were corrected for errors introduced by the signal conditioning and recording systems.

5.2.2.3 Phasing of Signals Between Rotating and Stationary Instrumentation

It was necessary to determine the phasing between signals from the rotating blades and the stationary wall instrumentation. Of specific interest was the phasing of the reference signal from the strain gage on the No. 3 blade and the signals from the case-mounted Kulites. A variation or extension of the cross-spectral density technique was used.

The flutter component of the signals has different frequencies in the rotating and stationary coordinate systems. The frequencies in the stationary system are either higher or lower than those in the rotating system because they are composed of the fundamental flutter frequency plus or minus multiples of rotor rotational speed. This can be seen in the following derivation.

The vibration of the individual blades in a stage in flutter is fully defined by the sum of a finite series of circumferential harmonic waves where the number of component waves equals the number of blades, N, in the stage. The associated unsteady pressure, p, at a particular axial coordinate, x, varies with tangential coordinate, y, and time, t, is described by the sum of an infinite series of forward and backward rotating harmonic waves having all integer numbers of cycles around the circumference of the stage. This function is expressed in terms of sets of responses to individual orders, m, of blade vibration where $1 \le m \le N$.

$$P_{m}(x,y,t) = \sum_{n=-\infty}^{\infty} p_{mn}(x)e^{i(\beta_{mn}y+\omega t)}$$
(1)

Where n, the number of full waves per intrablade passage, is added to the fractional number represented by m waves around the full circumference. ω is the flutter frequency common to all phenomena in the rotating system. The unsteady periodicity condition defines the wave number

$$\beta_{mn} = \frac{\phi_m + 2 \pi n}{s} \tag{2}$$

where the interblade phase angle,
$$\phi_{\rm m} = \frac{2 \, \pi \rm m}{N}$$
 (3)

and blade spacing,
$$s = \frac{2 \pi r}{N}$$

where r is radius

hence
$$\beta_{mn} = \frac{m + Nn}{r}$$

In the stationary system, the coordinates x' and y' are related to their rotating counterparts by

$$x = x'$$

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(4)

where Ω is the rotor speed. Equation (1) then becomes

$$P_{m}(x', y', t) = \sum_{n=-\infty}^{\infty} p_{mn}(x')e^{i\beta_{mn}}(y' + (\Omega r + \omega/\beta_{mn})t)$$
 (5)

This is in the form of waves having wavelength 2 π/β_{mn} , moving at velocity ($\Omega r + \omega/\beta_{mn}$). The frequency ω_{s} neasured by a stationary probe is the product of the wave number β_{mn} and the wave velocity. Hence

$$\omega_{S} = \beta_{mn} \Omega r + \omega = \Omega m + \Omega Nn + \omega$$
 (6)

where Ω m is a multiple of shaft speed, and Ω Nn is a positive or negative multiple of blade passing speed. Therefore, the single flutter frequency, ω , in the rotating system becomes a spectrum when detected by a stationary sensor. The observed frequencies, $\omega_{\mathbb{S}}$, are spaced at multiples of shaft speed, Ω . The index m identifies the associated harmonic wave component of blade vibration and the index n identifies the added number of waves within a passage between adjacent blades.

Because flutter was seen at many frequencies by the case-mounted Kulites, phase information could not be produced directly. Instead, an aliasing technique was used. By selection of the sampling rate to equal the rotational frequency, both the rotating and stationary transducer flutter signals were transformed to a new coordinate system in which a single flutter frequency existed for both sets of signals. Phasing of the signals in question could then be performed. The one-per-revolution speed pip was used as the sampling rate command.

Two different procedures were used to produce phase information. One procedure was to allow all the flutter components in the stationary signal to be aliased. The other procedure was to isolate individual spectral components of the flutter with a narrow filter before aliasing. This latter technique extracted a single nodal diameter signal plus its harmonics at multiples of the rotor speed. In all cases, the sampling command was properly conditioned to allow the rotor to be in a selected orientation before a data sample was taken. Corrections to the final phase angle were included for influences of all signal conditioning and the aliasing process.

5.2.2.4 Strain Gages

Each of the 32 blades was instrumented with one dynamic strain gage located near the maximum thickness point above shroud at 64 percent span. The stage flutter response was obtained from the strain-gage signals consisting of amplitude, frequency, and phase. The amplitude and frequency characteristics of the individual blades were obtained from power spectral density (PSD) plots from 0 to 2 kHz. Phases relative to the gage on the No. 3 blade were obtained by using the cross spectral analysis technique described in Section 5.2.2.2.2. The strains were of the form S_{ν} e i $^{\omega t}$ where the complex number, S_{ν} , representing the strain in the No. 3 blade, defined phase as well as amplitude. The S_{ν} numbers, where $1 \leq \nu \leq N$, may be represented by the finite summation

$$S_{\nu} = \sum_{m=1}^{N} \sigma_m e^{\frac{i2 \pi m \nu}{N}}$$
 (7)

where $\sigma_{\rm m}$ is the amplitude of a series of patterns having numbers of lobes, m, where $1 \le {\rm m} \le {\rm N}$, rotating with respect to the disk at speed $\omega/{\rm m}$. From the known amplitude and phase of each strain gage, S_{ν} , the complex coefficients, $\sigma_{\rm m}$, of the series in equation (7) may be determined by mathematical inversion to give the strength of the mth modal component or spatial harmonic and its phasing with respect to all other components.

The broadband and flutter frequency amplitudes for all strain gages and rotating Kulites were plotted versus time to help establish the stability of the data during the two-minute steady-state records. The plots were also used as a cross-check with the power spectral density curves to help identify possible errors in engineering unit conversions.

5.2.2.2.5 Mirrors

Blade mode snape was determined by analysis of the laser optics mirror data. Blade deflection amplitudes were determined from the mirror data. For the blades without mirrors, the deflection amplitudes and relative phases were determined through correlation of the strain gage data and the mirror data.

Typical still photographs of the mirror data in and out of flutter are shown in Figure 11. The difference in width of the same spot in the two images is proportional to the torsional amplitude and the difference in height is proportional to the axial component of the bending slope.

The 16mm film record of the reflected laser beams was digitized using a Spatial Data Systems Scanner. The measurement accuracy was better than ± 0.00254 cm (0.001 in.). The data were stored on magnetic tape for computer processing.

A fast Fourier transform was used to convert the data from the time domain to the frequency domain. This procedure allowed the calculation of power spectral densities and cross-spectral densities to determine amplitude and phase angles for the different mirrors.

5.2.2.6 Case Mounted Kulites

The case mounted Kulites were used to obtain nodal diameter patterns present in the rotor system during flutter, contour maps of the pressure distributions over the blade tips during stable operation, contour maps of the unsteady pressures during operation with flutter, and contours of the real and imaginary components of the unsteady pressure and relative phase during flutter.

The nodal-diameter patterns in the rotor system during flutter operation were determined through Fourier analysis of the signals from the case-mounted Kulite pressure transducers.

The contour maps of pressure distributions over the blade tips were obtained from wall Kulite and wall static tap data. The technique discussed in Section 5.2.2.2.1 was used to enhance the broadband Kulite signals. The one-perrevolution speed signal was the reference signal used in this procedure. Data from 512 rotor revolutions were averaged to produce the final plots. The enhancements were timed to allow a selected group of blades to occupy a desired orientation relative to the wall Kulites. These enhancement techniques produced a signal-to-noise improvement factor of about 22.6.

Plots of pressure versus time were digitized to obtain an array of pressures representing the variation from the mean at the specific axial location. A minimum of ten samples per blade gap were digitized. The time location of each pressure sample was translated into a rotating frame, with the leading edge of the No. 2 blade used as the zero reference. The wall mean static pressure for each axial location was added to the local variation to obtain the steady-state pressures. The array of local static pressures was input into a contour plotting package, which linearly interpolates in space to find specified levels of pressure. The lines of constant pressure were normalized as percentages of the maximum local steady-state static pressure sampled, and contour maps of the constant percentages of pressure were machine plotted.

When the contour maps at the blade tips were plotted, the pressure fields with respect to the blade leading edges were observed to be shifted about three degrees tangentially in the direction of rotation, corresponding to a time delay of about 30 microseconds. However, this shift, which was nearly independent of rotor speed, did not appear in the nonsteady pressure plots obtained from the same data. The shift is therefore believed to have resulted from the data reduction procedure used to obtain the steady-state plots. Considerable time was spent trying to find the source of the shift either in circumferential relation between the time trigger and the blades or in unaccounted delays in the electronic equipment. Although the source was not found, the location of the blades was evident from the plots. Each steady pressure plot in the report has been corrected to place the blades in the proper positions. The amount of shift is presented in the Appendix D with the contour maps.

The procedures for obtaining the plots of unsteady pressures over the blade tips, the real and imaginary components of the unsteady pressures, and the phase angles for the unsteady pressures are given in Section 5.2.2.2.3

5.2.2.2.7 Blade-Mounted Kulites

Blade-mounted Kulites provided unsteady pressure amplitude and phase distribution for both the pressure and suction surfaces of the airfoil at two radial positions. Amplitudes were determined from the power spectral density for each signal over a frequency range of 0 to 2 kHz. The power spectral density data were confirmed by backup plots of amplitude against time during the two minute test period.

Cross-spectral density functions were used to determine the phasing of the pressure signals relative to the strain gage signal from No. 3 blade.

5.2.2.2.8 Hot Film Probes

The data obtained from the hot-film probes were analyzed using the same enhancement and reduction techniques used for the case-mounted Kulite data. Contour maps were not produced, however, because of the very low level of the signals at the flutter frequency.

5.2.2.2.9 Blade-Mounted Hot-Film Sensor

Blade-mounted hot-film sensors provided air velocity measurements on the blade suction and pressure surfaces at two radial positions. The flutter response from these sensors consisted of frequency, amplitude, and phase. Amplitude and frequency were obtained from the power spectral density for each signal over a frequency range of 0 to 2 kHz. The measured amplitude had a repeatability of +20 percent, making it possible to relate the data from one point to another. The strain gage on the No. 3 blade was used as the reference for determining phase angle. The resulting phase angles were compared with those from the blade-mounted Kulites and strain gages, and the accuracy of the measurements was comparable.

5.2.2.3 NASTRAN Prediction Procedure

In structural analysis of rotor blade systems, stresses and deflections are commonly calculated for both the stable and vibrating modes of operation by the NASTRAN finite element approach. To evaluate the effectiveness of this procedure, deflections of the TS22 rotor and blades were calculated and the results compared with measured values obtained during the test program.

NASTRAN calculations were made for both the stable and free-vibration mode for the TS22 rotor system. Calculations were made for speeds of 65, 73, and 75 percent of design. Calculations for vibrating conditions covered three through nine nodal diameter patterns. Because NASTRAN's cyclic symmetry analysis was used, only a one-blade wedge of the rotor was modeled. Rotor speed effects were included by adding a centrifugal prestress stiffness matrix to the conventional static stiffness matrix.

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Finite element mesh diagrams for the blade is shown in Figure 12; the shroud and disk, not shown, were also modeled. Triangular plate elements and beam elements were employed for the NASTRAN calculations. The blade, shroud, and disk models were joined using multi-point constraint equations. On the basis of previous experience with the TS22 rotor analysis, shroud-to-shroud interfaces were assumed to be pinned together at a single center node in the cyclic symmetry analysis. The disk used for the TS22 rig was very stiff, and its flexibility did not contribute to the mode shapes.

5.2.2.4 Blade-Work Interaction Calculation

The flutter characteristics of the test rotor and the types of data obtained allowed for an evaluation of a theory of energy transfer that takes place during flutter. The assumptions associated with this theory are:

- 1) Self-excited vibrations occur in a bladed rotor when the energy supplied by the air stream exceeds the energy dissipated through the structural damping associated with that mode.
- 2) The complex rotor vibration mode can be defined as a summation of simple circumferential harmonic responses (i.e., Fourier decomposition).
- 3) The net aerodynamic energy of a mode is the algebraic sum of the aerodynamic energy associated with each harmonic response.
- 4) The susceptibility of a rotor vibration mode to flutter is a function of the stability of the individual harmonic responses.

An aerodynamic damping exists for each harmonic response. This damping is defined by the log decrement parameter, which is proportional to aerodynamic work divided by kinetic energy of the harmonic

$$\delta_{\text{aero}} = \frac{W_{\text{m}}}{E_{\text{m}}}$$

For positive values of the aerodynamic damping parameter, the energy flow is from the structure to the flow stream and in the reverse direction for negative values.

The aerodynamic work per cycle done by each of the individual harmonics is computed by integration

$$W_{m} = \int_{chord} \int_{0}^{2\pi} \Delta P_{m} \frac{dh_{m}}{d(\omega t)} d(\omega t) db$$

where:

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 ΔP_m = pressure jump across the airfoil from the mth harmonic and is of the form $\Delta P_m = P_m (x,y_p,t) - P_m (x,y_s,t)$

where:

 y_{D} and y_{S} are blade surface coordinates on the pressure and suction surfaces at axial location x

 h_m = deflection normal to the airfoil surface of the mth harmonic

 (ωt) = position angle during the vibration cycle

b = chordwise location

 ω = flutter frequency

t = time

The pressure at the airfoil tip at any axial location is the summation of the distribution resulting from individual blade harmonic motions.

$$P(x,y,t) = \sum_{m=1}^{N} P_m(x,y,t)$$

The pressure of each harmonic is defined by a fourier series described in Section 5.2.2.3.

$$P_{m}(x,y,t) = \sum_{n=-\infty}^{\infty} P_{mn}(x)e^{i(\omega t + \beta_{mn}y)}$$

These pressure waves are translated into the stationary system using the relationships given in Section 5.2.2.2.3.

$$P_{m}(x',y',t) = \sum_{n=-\infty}^{\infty} P_{mn}(x')e^{i\left[\left(\omega + (m + Nn)\Omega\right)t + \beta_{mn}y'\right]}$$

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The values of P_{mn} at frequencies ($\omega_{mn}\text{=}(\text{m}+\text{Nn})\,\Omega)$ are obtained by processing the casing wall Kulite signals through a wave analyzer. The frequency band of the recorded data was 40 kHz which at the maximum rotational test speed of the rotor permitted ten harmonics (i.e., $-10 \le n \le +10$) to be determined.

Since no direct measurement was made of the mode shape at the blade tip, a NASTRAN analysis was used to predict the deflections.

The predicted mode shapes were scaled and phased in accordance with the measured strain components to define the tip motion, hm, required to calculate the energy transfer in three dominant harmonic components.

The kinetic energy per cycle of the individual harmonics was computed by integration:

$$E_{\rm m} = \frac{1}{2} \int_{\rm Chord} \int_{\rm Span}^{\mu\tau \omega^2} (f_{\rm m}^2 + g_{\rm m}^2 + h_{\rm m}^2) dl db$$

where:

 μ = airfoil material density τ = airfoil thickness spatial components of deflection in the mth harmonic

= spanwise location coordinate b = chordwise location $<math>\omega = flutter frequency$ chordwise location coordinate

The NASTRAN mode shape energy levels were scaled in proportion with the strain component amplitude squared to determine the kinetic energy level of the individual harmonic responses.

SECTION 6.0

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DISCUSSION OF PROGRAM RESULTS

6.1 OVERVIEW

The large body of time-correlated, high-quality data acquired has broadened our understanding of subsonic/transonic stall flutter. The more significant results were:

- 1. Deviations from uniform phase angle from blade-to-blade, previously attributed to insignificant anomalies in the data, are important, being indicative of a complex flutter characteristic.
- 2. Flutter alters the passage steady pressure pattern only slightly, as shown in the steady-pressure contours.
- 3. Work input is concentrated near the leading edge, as shown in the unsteady-pressure contours.
- 4. Local supersonic flow is required in order for this flutter to occur.

Details of these results and a discussion of possible causes of flutter are presented in the following sections. The bulk of the data obtained in this investigation and blade coordinate data are given in Appendices A through E:

Appendix A - Tabulations of Steady State Performance Data

Appendix B - Rotor Blade Coordinates

Appendix C - Part I, Steady Blade Structural Data Part II, Unsteady Blade Structural Data

Appendix D - Part I, Steady Pressures Part II, Unsteady Pressures

Appendix E - Hot Film Data

6.2 TEST MATRIX

Tests were run over a range of corrected speeds from 54 to 85 percent of design. A transient was run at each of several speeds from wide-open-throttle to surge, and the points of flutter initiation as well as the surge were determined. Data along the 70 percent speed line are shown in Figure 13.

The data points in Figure 13 were taken during a slow transient in which equilibrium conditions were not fully established. Furthermore, the pressure ratios were obtained from arithmetic averages of a limited number of rake readings. As noted on Figure 13, flutter was first indicated by the hot-film gages at about 67 percent of design flow, and the first indication of flutter on the strain gages appeared at about 63 percent of design flow. Surge occurred at about 56 percent of design flow.

A composite map for all test speeds is shown in Figure 14. These data were obtained at fully stabilized conditions and represent mass-weighted average performance. Flutter occurred at speeds between 63 and 75 percent of design. The flutter boundary shown on Figure 14 represents a blade vibratory stress level of $\pm 2068 \text{ N/cm}^2$ (3000 lbf/in.²) as measured on the strain gage just above the shroud. Surge was encountered before flutter at speeds below 63 or above 75 percent of design.

Additional blade-element data and other aerodynamic performance detail are tabulated in Appendix A.

6.3 STRUCTURAL DEFORMATIONS

Steady-state structural deformations of the blades were determined from data from the optical mirror system. Unsteady deformations during flutter were determined from the optical mirror system, the strain gages, and by analysis of the high response pressure data.

6.3.1 Steady-State Deformations

The mirror system provided what is believed to be the first set of high quality data describing blade deformation at normal fan operating conditions. The results showed that the deformations under combined centrifugal and gas loads were close to the predicted levels, with slightly higher uncambering. Results are given in Appendix C. Table C-1.

Local steady-state untwist at from 35 to 85 percent of the design speed are shown in Figure 15 for the 95 percent span location. Above 25 percent speed the amount of untwist varied as the square of the rotational speed, as predicted. Below this speed, the midspan shroud was not seated, and the untwist varied in an unpredictable manner.

The distribution of untwist along the span at 73 percent speed is shown in Figure 16. Approximately equal amounts of untwist occurred above and below the shroud, which was at the 62 percent blade span and constrained untwist to near zero at this location. Untwist was essentially a function of speed only. The effects of gas loading were negligible. As shown in Figure 17, the variation of untwist with flow at 75 percent speed was less than 0.1 degree for a flow change from 70 to 59 kg/sec (155 to 130 lbm/sec), corresponding to a blade tip D-factor increase of 0.1764.

Measured untwist as a function of chordal position is shown in Figure 18 for 73 percent speed. Uncambering was significant at all stations above the shroud, exceeding 0.3 degrees near the blade tip.

Figure 19 shows both the measured untwist and the untwist calculated by the NASTRAN analysis. Generally, good agreement was obtained except close to the leading and trailing edges, where predicted deformation was greater than measured. Therefore, the measured uncambering at the tip was slightly higher than predicted. However, the deformations in this region, where the airfoil was very thin, were sensitive to the actual airfoil thickness, and slight variations within specified tolerance might have been sufficient to cause the observed discrepancies.

Additional steady-state deflection data are given in Appendix C, Part 1.

6.3.2 Unsteady Deformations

Previous to this program, fan flutter had been visualized as a sinusoidal, circularly traveling wave superimposed on the rotor, forming a single multinodal pattern, each rotor blade deflecting sinusoidally in sequence as the wave traveled around the rotor (ref. 3).

Such a wave was characterized by concentric ring nodes and traveling nodal diameters or diametral lines of zero deflection. Figure 20 shows such a system with two ring nodes and three nodal diameters. This pattern is referred to as a vibration in the second mode with three nodal diameters. On a rotating stage, the radial lines travel either forward or backward, and adjacent blades experience a relative time delay or phase difference (interblade phase angle) as the wave passes. With such a concept, all blades are assumed to flutter at the same frequency and amplitude, with uniform phase angles between adjacent blades.

The results of the current program revealed a different picture: all blades fluttered at the same frequency, but not at the same amplitude and interblade phase angles were not equal. Typical amplitudes and phase angles observed during the program are shown in Figures 21 and 22, respectively. These data were obtained from the strain-gage measurements. Amplitudes in Figure 21 are expressed in terms of measured stress. The patterns shown represent a family of spatial harmonics described by the superposition of a number of rotating nodal diameter patterns, each characterized by a different number of nodal diameters with different but uniform amplitudes and different but uniform phase indexing, with each pattern rotating at a speed that results in the same flutter frequency.

The detailed definition of the amplitude and phase for each nodal diameter pattern was determined from wall Kulite data. A result of this analysis is presented in Table VIII. As shown in the table the fifth nodal diameter pattern had the strongest signal at 67 percent speed. The seventh nodal diameter pattern was strongest at 73 percent speed, and the eighth was slightly stronger than the others at 75 percent speed.

To further study the complex mode shapes of the rotor and blading, stability calculations were made for the fifth, seventh, and ninth nodal patterns at 70 percent design speed. These patterns represented two strong signals and one weaker signal. The results of these calculations are given in Table IX in terms of the logarithmic decrement which is 2π times the ratio of available damping to critical damping. Since this number represents the percentage rise or decay of the signal, a negative value of the logarithmic decrement represents an unstable or flutter condition. Complete pressures used in the stability calculations (see equation at bottom of page 21) are listed in Table IX and plotted in Figures D-40, D-41, and D-42 for the upper and lower surfaces of the airfoil. The chordwise position of the pressures is the same as for the wall mounted Kulites from which the data was obtained.

Table IX shows that the fifth harmonic was the principal source of instability at 70 percent speed. The seventh harmonic was marginally unstable; the ninth, marginally stable. The results suggest that the effect of asymmetries, or "mistuning", on the system in flutter is to couple secondary modes into the instability. This is an important result, clearly demonstrating that any future flutter analysis that is to be correlated against test data for a mistuned bladed disk system must be capable of handling several spatial harmonics.

The present analysis is not capable of explaining the mechanism that determines what patterns will occur or what their relative indexing will be. However, the mechanism probably relates to the mistuning of the stage, which results from small dimensional differences among these airfoils. These airfoils had been deliberately grouped by frequency when the rotor was assembled, see Figure 2. And it may be significant that the group of airfoils with the highest flutter amplitudes were those that individually had natural vibratory frequencies equal to the average frequency for the lade set. It may also be significant that only forward traveling waves (traveling in the same direction as the rotor) were observed.

Additional stress level and phase angle data from strain gages are given in Appendix C, Part 2, Table C-2 and Figures C-8 through C-10. Blade deflection data from the mirror system were also reduced to obtain amplitudes of bending and torsional displacements during flutter. These data are tabulated in Tables C-3 and C-4 and plotted in Figures C-11 through C-15 of Appendix C, Part 2. These additional data corroborate the results presented above.

6.4 PRESSURE DISTRIBUTIONS

The study of the steady and unsteady pressure contours obtained with the case-mounted Kulites and unsteady pressures obtained from the blade-mounted Kulites revealed several important features concerning transonic compressors in general as well as the stall flutter phenomenon.

A review of the pressure contours outside and inside the flutter boundary showed the development of the shock structure with increasing rotor speed and the shifts in position of both the peak pressure point and the shocks with increased loading. In general, increasing rotor speed on a given operating line resulted in a strengthening of the expansion waves and normal shock and a shift rearward of the shock. Moving up a speed line to higher loading and incidence shifted the shock forward towards the leading edge. Crossing the flutter boundary produced little change although the normal shock appeared to have spread, which is probably indicative of shock oscillation. Details are presented in the following paragraphs.

6.4.1 Steady-State Pressure Distributions

At 63 percent speed outside of flutter, data from the case-mounted Kulites showed that high loading occurred at the leading edge and that the flow was subsonic (Figure 23). Moving up to a high operating line into flutter is shown in Figure 24.

At 67 percent speed on the low operating line, expansion waves occurred behind the leading edge, culminating in a shock at about 15 percent chord (Figure 25). At the flutter boundary at 67 percent speed, the shock appeared to be a gradual compression, which may be indicative of an oscillating shock (Figure 26).

At 70 percent speed outside the flutter boundary, supersonic Mach number expansion at the leading edge was more clearly evident, and the normal shock moved rearward to the 20 percent chord position (Figure 27). At the flutter boundary, the shock moved forward, very close to the leading edge (Figure 28). Near surge the leading edge expansions appeared to be weaker, but the passage shock appeared stronger (Figure 29).

At 73 percent speed on a low operating line (Figure 30), the shock moved further rearward to about the 30 percent chord position. Moving into flutter (Figure 31) the principal loading remained at the leading edge with the data showing considerable smearing of the normal shock. Essentially identical trends occurred at 75 percent speed (Figures 32 and 33).

Significant changes occurred at 85 percent speed. At this speed surge occurred before flutter. On the low operating line (Figure 34) significant reacceleration occurred behind the shock and the compression process was far from optimum, with negative lift occurring on the aft portion of the blade. Moving up the operating line (Figure 35) resulted in a high Mach number with strong leading edge expansion and a strong detached bow shock. Operating near surge (Figure 36) produced little change in this pattern.

Additional plots and tabulations of steady-state pressure distribution data are given in Appendix D. Part 1.

6.4.2 Unsteady Pressure Distributions

Unsteady pressure data were reduced to contours of unsteady pressure amplitude and contours of the real and imaginary components of the unsteady pressure to provide relative phasing information. Typical plots are presented in Figures 37, 38, and 39. To interpret these plots it should be noted that the real and imaginary components represent the instantaneous unsteady pressures at two time phases separated by 90 degrees. Hence, the square root of the sum of the squares of the real and imaginary amplitudes shown in Figures 38 and 39 is equal to the amplitudes shown in Figure 37, and the relative phase angle of the unsteady pressure is equal to the arctangent of the ratio of the real and imaginary components.

The data showed high unsteady pressures near the leading edge (back to approximately the 25 percent chord position), relatively low values near the trailing edge, and minimum amplitude near midchord. Similar trends were evident in the blade unsteady surface pressures measured by the blade-mounted Kulite (see Figure 40). The arrow lengths in this plot represent unsteady amplitudes and the directions represent phase angle as referenced to the strain-gage signal from the No. 3 blade. As shown, significant unsteady pressure amplitudes were confined to the leading edge portion of the airfoils.

These results clearly indicate that the major portion of the action was concentrated in the first quarter of the airfoil, implying that future flutter research should concentrate on the aerodynamics near the leading edge.

Additional unsteady pressure data and plots are given in Appendix D, Part 2.

6.5 VELOCITY FLUCTUATIONS FROM HOT FILM SENSORS

Hot-film probes were located ahead of and behind the rotor to determine the influence of flutter on the inlet and exit flows. Hot-film gages were also located on the rotating blades to determine velocity fluctuations occurring on the blade surface during flutter.

5.5.1 Upstream and Downstream Velocity Fluctuations

Enhanced wave forms from the hot-film probes ahead of and behind the rotor are shown in Figure 41 for two test points at 75 percent speed: one at wide open discharge, the other in the flutter region. Because these signals were not calibrated for amplitude, the magnitudes of fluctuation are not known. For the open discharge condition, the inlet signal at the blade tip showed a velocity fluctuation of blade passing frequency that was caused by the passage of expansion and shock waves emanating from the blades. There was no defined pattern at the inlet near the shroud and at the blade root where the relative inlet velocity was subsonic. At the rotor exit, a well defined blade wake pattern existed for all three radial positions. The inlet probe patterns in flutter, were similar to those for the nonflutter condition. Behind the rotor at the hub, the pattern was also similar to that for wide open throttle. However, at the near shroud and tip exit position, the blade wakes were not as well defined as for the nonflutter condition. The tip pattern had some random fluctuations at other than blade passing frequency, but did not show a significant fluctuation at flutter frequency.

6.5.2 Blade Surface Unsteady Velocities

Unsteady velocities and phase angles were determined from the hot-film gages mounted on the rotor blades. Data for a flutter condition at 67 percent speed are shown on Figure 42. The arrow length in this plot represents the amplitude of the unsteady velocity relative to the maximum fluctuation observed for that test point. The direction of the arrow indicates the phase angle referenced to the strain-gage signal from the No. 3 blade. The major fluctuations of velocity occurred on the forward part of the airfoil, but some significant fluctuations also occurred at midchord and near the trailing edge.

The blade-mounted hot-film data were not analyzed from the standpoint of determining flow separation from evaluation of turbulence levels. Determination of separation point location within the gage spacing can probably be obtained from the existing data, but the spectral analysis required is beyond the scope of the present analysis.

Additional hot-film data are given in Appendix E.

6.6 REDUCED VELOCITY VERSUS INCIDENCE ANGLE

Empirical correlations of reduced velocity versus incidence angle have been used extensively as a stall flutter criteria. The range of design types over which any specific correlation will accurately predict flutter boundaries, however, is questionable. Existing correlations were based on measured air angles, but blade metal angles were usually taken as the calculated metal angle at design speed. In this program, actual metal angles were measured. Figure 43 presents a plot of reduced velocity versus measured incidence angle. Incidence angles were based on the blade leading-edge mean-line metal angle. The reduced velocity parameter, $V/b\omega$, is the ratio of the relative inlet velocity, V_1 ', to the product of the blade half-chord, b, and the rotational flutter frequency, ω , in radians per second.

Figure 43 shows that flutter occurred at high incidence angles only over a limited range of reduced velocity values, with flutter-free operation being obtained at reduced velocities both above and below those at which flutter was achieved for a given incidence. A possible explanation is that locally supersonic flow may be required for flutter and that this was not achieved at low rotor speeds and velocity ratios, even at high incidence. At very high speeds and velocity ratios, the incidence was too low even at surge to support flutter.

Conventional values of incidence based on calculated design speed metal angles and reduced velocity parameters for any selected radial position can be obtained from interpolation of the blade element data in Appendix A and the blade chord data in Appendix B.

SECTION 7.0

SUMMARY REMARKS

Certain phenomena were consistently observed when flutter occurred, and some of these may be necessary for flutter.

7.1 LOADING LEVEL

Stall flutter is initiated by an increase in aerodynamic loading level, and reducing the loading level returns the stage to stable operation. The loading level at which flutter occurs, however, is not unique because small modifications to the airfoils—or sometimes simply reassembly of the rotor using a different blade sequence—will move the flutter boundary significantly.

7.2 LOCAL SEPARATION

Local separation has been a popular candidate as a cause of flutter. The physical concept by which separation, particularly oscillating separation, might put work into the system to induce flutter is conceptually attractive. In addition, such a theory would be consistent with the observed relationship between flutter and loading. Although the data analysis procedures used in this program did not clearly reveal regions of separation on the airfoils, a more detailed analysis might reveal that such separation did occur, at least on small areas of the airfoils.

7.3 OSCILLATING SHOCKS

Oscillating shocks is another intuitively attractive cause of flutter. The pressure step across the shock is on the order of 1.4 N/cm^2 (2 $lbf/in.^2$) and small oscillation could put work into the system. In addition, stall flutter does not occur, at least in the TS22 stage, at speeds below those where local supersonic flow occurs.

An oscillating shock would also be expected to produce a region of high unsteady pressure on the unsteady pressure amplitude contour plots. Such a region was not observed.

7.4 REDUCED VELOCITY VERSUS INCIDENCE

Empirical correlations of reduced velocity versus incidence have been used to predict flutter boundaries for stall flutter. This is essentially an extension of wing flutter theory. This empirical approach, however, has not been completely successful when applied to a variety of design types. The subject program supplied data for incorporation into existing correlations.

7.5 CENTER OF PRESSURE-CENTER OF TWIST

The relative position of the aerodynamic center of pressure and the structural center of twist has been considered significant in flutter. This theory states that flutter will occur if the effective aerodynamic center of pressure moves ahead of the structural center of twist of the airfoil. The case-mounted Kulites in this program gave data on pressure distributions in the blade tip region, which might give a clue to center of pressure location, but data at all radial positions must be considered in such an analysis.

SECTION 8.0

SUMMARY OF RESULTS

Although the program objective related primarily to the acquisition of data, several important conclusions can be drawn from the review of the data completed under the contract:

- 1. The agreement between the measured steady-state blade deflections and those predicted by NASTRAN calculations was good. The small deviations noted could have been due to slight deviations in blade leading and trailing edge thickness.
- 2. Unsteady work during stall flutter occurred almost entirely in the forward section of the airfoil.
- 3. The mode structure during stall flutter was more complicated than previously supposed, apparently because the effects of mistuning result from blade-to-blade variations that previously were assumed to be insignificant.
- 4. Much work remains to define the causes of stall flutter, but a clear correlation with loading has been identified.
- 5. Local supersonic flow over at least a portion of the airfoil appears necessary for stall flut or to develop.

SECTION 9.0

RECOMMENDATIONS

The development of a design system that will preclude stall flutter requires a better understanding of the physics of the phenomenon. This program provided new data for obtaining that understanding.

The next step should be a more detailed analysis of the available data to determine the behavior of such phenomena as mistuning, localized separation, shock oscillation, and the unsteady pressure change across the blades.

Such a detailed analysis would then suggest additional test programs in which the specific parameters identified as significant could be varied to quantify their effects.

An oscillating shock would also be expected to produce a region of high unsteady pressure on the contour plots. Although such a region was not observed, additional data might be extracted from the recorded data.

SECTION 10.0

REFERENCES

- 1. Stargardter, H: "Optical Determination of Rotating Fan Blade Deflections," <u>Journal of Engineering for Power</u>, April 1977, pp. 204-209.
- 2. Glawe, G. E.; Simms, F. S.; and Stickney, T. N.: "Radiation and Recovery Corrections and Time Constants of Several Chromel-Alumel Thermocouple Probes at High Temperature in High Velocity Gas Streams," NASA TM X-2170, 1971.
- 3. Mikolajczak, A. A.; Arnoldi, R. A.; Snyder, L. E.; and Stargardter, H.: "Advances in Fan and Compressor Blade Flutter Analysis and Predictions," Journal of Aircraft, April 1975, pp. 325-332.
- 4. Stargardter, H: U.S. Patent 4080823, "Vibration Measurement."

TABLE I

TS22 FAN STAGE DESIGN PARAMETERS

<u>Aerodynamic</u>

Pressure ratio Rotor Stage	1.702 1.67
Adiabatic Efficiency Rotor Stage	0.871 0.838
Corrected Flow	95 56 kg/sec (210.67 lbm/sec)
Specific Flow (annulus at rotor inlet)	202.78 (kg/sec/m ²) (41.53 bm/sec/ft ²)
Geometric	
Rotor Tip Diameter	0.8178m (2.7 ft)
Number of Blades	32
Fub Solidity	2.60
Tip Solidity	1.315
Hub/Tip Ratio (rotor leading edge)	0.32
Partspan Shroud Location (percent span from hub)	62

TABLE II

TS22 BLADE DESCRIPTION

Corrected Design Speed Airfoil Series Aspect Ratio Taper Ratio Tip Speed	11,042 rpm Multiple Circular Arc 3.6 1.5 472.4 m/sec (1550 ft/sec)
Root Diameter Inlet	26.2 cm (10.3 in.)
Tip Diameter Inlet	81.7 cm (32.2 in.)
Exit	79.7 cm (31.4 in.)
Beta 1*(a) Root Tip	54.999 deg 27.0399 deg
Beta 1* Suction Surface(b) Root Tip	48.503 deg 25.398 deg
Chord Length Root	7.47 cm (2.94 in.)
Tip	10.42 cm (4.10 in.)

Notes:

- (a) Beta 1* is the leading-edge metal angle, β , *, the angle between the tangent to the mean camber line and the meridional direction.
- (b) Leading-edge metal angle based on suction surface.

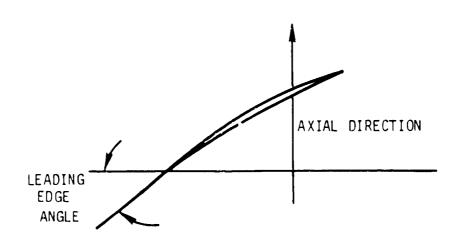
OF Fig. 1

TABLE III

LEADING EDGE ANGLE BLADE INSPECTION RESULTS

Percent(a) Span	Design	Minimum	Maximum	Average	Design Value Minus Average Value
0.08	47054 '	47040	480121	470501	0004 '
0.12	46010'	45024	4600'	450441	00261
0.22	42054 '	42016'	43012'	42042 '	0012'
0.32	40054 1	390281	390461	390371	00301
0.43	370581	370181	37040'	370291	ე029 '
0.52	36052 '	36081	3700'	360291	00231
0.55	37041	36050'	3700'	360551	0091
0.58	370101	36°10'	360281	36018'	0052'
0.62	35026 '	35001	35081	35021	00241
0.66	34036 '	330301	34054 1	34015'	0021'
0.72	32001	310481	31052 1	3105'	00551
0.82	280501	280241	28044'	300291	0014
0.92	250241	25041	250501	250291	-00051
0.99	230101	220561	23041	220581	0012'

Note: (a)Percent Span From Hub



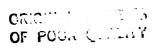


TABLE IV

TRAILING EDGE ANGLE
BLADE INSPECTION RESULTS

Percent(a)Span	Design	Minimum	<u>Maximum</u>	Average	Value Minus Average Value
0.08	96050'	950501	96021	950541	00561
0.12	870101	860141	86042 1	860281	0042 '
0.12	690561	6900'	70016	690371	00291
0.32	580281	570581	580341	580141	0014
0.42	49081	480 42 1	49001	480401	0018'
0.52	44034	43044	440401	44071	۰ 27 00
0.55	430421	430241	430301	430281	0014
0.58	43014	420221	420461	420371	0037 '
0.62	4100	40041	400281	400151	0048'
0.66	390421	49041	390521	390251	0017'
0.72	35028	350261	350381	350321	0041
0.72	300281	30014'	300481	300291	י 001
0.92	24024	24024	25001	24041 '	-0017'
0.99	21058'	210381	21056'	21044'	0014'

Note: (a) Percent span from hub

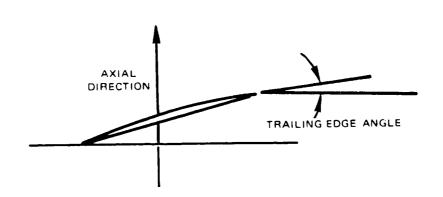


TABLE V

INSTRUMENTATION AND READOUT EQUIPMENT

Non-Steady Instruments Recorded

- 32 Strain gages
- 24 Hot films blade mounted
- 4 Stationary hot film probes
- 10 Wall Kulites
- 32 Blade mounted Kulites
- 102 Sensors

Recorders

- 1 70 channel multiplex
- 2 9 channels Sangamo
- 3 11 channels Sangamo
- 4 12 channels strain gage console
- 5 <u>4</u> channels strain gage console

106 channels

Each of the five recorders had strain gage 3 in parallel as a common signal to permit time correlations between any of the 102 sensors.

Crim Or Park

TABLE VI

HIGH RESPONSE INSTRUMENTATION SPECIFICATIONS

Kulite - Model XCOL-8V-808

Rated Pressure:

Sensitivity:

Temperature Compensation

Acceleration Sensitivity:

Traverse

Perpendicular:

Natural Frequency

Non-Linearity and Hysteresis:

 $17.24 \text{ N/cm}^2 (25 \text{ lbf/in.}^2)$

3.8 x 10^4 mV/N/m² (2.62 mV/lbf/in.²) 278K to 422K (40°F to 300°F)

0.00004% Full Scale Gage

0.0002% kHz

230 kHz

+0.75% full scale maximum

Kulite - Model LQL5-080-25S

Rated Pressure:

Sensitivity

Temperature Compensation:

Acceleration Sensitivity:

Transverse: Perpendicular:

Natural Frequency:

17.24 N/cm^2 (25 lbf/in.²) 3.8 x 10⁻⁴ $mV/N/m^2$ (2.62 $mV/lbf/in.^2$)

278K to 422K (40°F to 300°F)

0.00008% Full Scale Gage per q

0.0004% Full Scale Gage per q

125 kHz

Quartz Hot Film

Thermo-systems model 1210-60

0.0154 cm (0.006 in.) quartz rod with platinum sensor deposited 0.203 cm

(0.080 in.) between posts

Temperature coefficient of resistance = 0.0026 ohm/ohm-ok Frequency Response at 91.44 m/sec (300 ft/sec): 200 kHz

OF Four Contract

TABLE VII
TS22 NASA FLUTTER TEST
TEST MATRIX

Run Number	Speed Code	Point Number	Unsteady Record	Percent Speed	Percent Corrected Design Flow	Rotor Pressure Ratio	Remarks
					Shakedown All Mirrors		
001	70	01	20-27	70	72.8	1.228	Wide Open Discharge
		••	28	70			Closing Discharge Valve, Transient into Flutter
001	70	05	43	70	66.9	1.2722	Check Point Wide Open Discharge
			64T		••		Transient
003	63	01	71	63	65.8	1.1776	Wide Open Discharge
003	63	03	76-84	63	53.4	1.2374	Stress Level Fluctuating, Shakedown Complete
					Performance All Mirrors		
003	73	01	86-94	73	74.7	1.2587	Wide Open Discharge
003	73	02	100-108	73	60.0	1.3 .7	Maximum Flutter
				4 Rows	3 Watt Lase Mirrors (Abov	er ve Shro d)	
004	70	03	128-135	70	59.8	1.3004	70% Low Flutter Point
004	67	01	136-143	67	68.5	1.1890	Wide Open Discharge
004	75	01	176-183	75	75.3	1.2840	Wide Open Discharge
004 005	75 73	04 08	195-202 220		60.3 56.5	1.3369 1.2978	Maximum Flutter
					All Mirror 3 Watt Las		
007	66	01	239	66	54.5	1.26	Maximum Flutter
007	60	01	242-249	55	52.0	1.1530	Near Surge (Rotating Stall)
007	85	02	279-286	85	85.8	1.3792	Wide Open Discharge
	••		287	**			Transient To Surge
007	85	05	288-295	85	75.1	1.4862	Near Surge

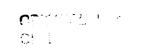
TABLE VIII

UNSTEADY WALL PRESSURE AMPLITUDES FOR INDIVIDUAL NODAL DIAMETER PATTERNS FUNDAMENTAL MODES ONLY (NO HARMONICS)

•• • •			Rel	ative	Power	Spectr	al Den	sity		
Nodal <u>Diameters</u>	-55 4	-15.1	-3.6	9.4	Percer	it Chor	d		^^ ^	111 7
D raince cer 3	-33.4	-13.1	-3.0	9.4	22.2	34.6	47.5	<u>73.4</u>	99.3	141.4
67 Percent	t Speed	<u> </u>								
2										
2 3 4 5 6 7 8 9				30						
4			40	45		24	25	33	34	
5			. •	65	58	50	100	140	220	
6				65	60	60	50	75	70	
7				65	70	75	70	85	80	
8				100	140	80	80	85	60	
9				85	100	45	35	28	20	
10							30			
73 Percent	Speed	-								
2										
2 3 4 5 6 7								26	24	25
4						40	36	26 24	24 57	25 41
5	9	25			96	54	78	100	140	170
6	10	32			92	59	86	74	150	125
7	24	84	96	68	165	240	180	340	270	280
8	35	77		130	165	150	140	160	150	120
9	0.0			110		88	75	44	35	38
10 75 Percent	26 Speed			125			80	34	31	24
75 Fercent	Speed									
2										
3								18	17	
4								25	20	
5				50	100	55	39	45	60	
2 3 4 5 6 7				50	80	78	70	70	100	
7					120	70	50	45	45	
8 9					140	110	78	55	75	
9 10					120	85		45	35	
10										

TABLE IX

COMPUTED DAMPING IN DOMINANT HARMONICS
AT 70 PERCENT SPEED



Harmonic	Log <u>Decrement</u>
5	-0.012
7	-0.001
٥	+0.002

Complex pressures used in damping calculation normalized to 1600 $\mbox{N/m}^2$ (0.232 lbf/in.2).

Percent Chord	Upper <u>Real</u>	Upper Imaginary	Lower Real	Lower <u>Imaginarý</u>	
-3.4 9.4 22.2 34.6 47.5 73.4 99.3	0.039 0.573 0.504 0.095 0.030 0.138 0.198	-0.091 -0.681 -1.000 -0.125 -0.246 -0.089 -0.026	0.022 0.056 -0.254 -0.069 -0.086 -0.108 -0.228	-0.022 -0.134 -0.060 -0.050 -0.142 -0.086 -0.039	5 Nodal Diameters
-3.4 9.4 22.2 34.6 47.5 73.4 99.3	-0.065 -0.250 -0.177 -0.091 -0.095 -0.129	0.01 0.190 0.384 0.056 0.060 -0.004 -0.052	0 0.039 -0.091 -0.121 -0.129 -0.112 -0.147	0.043 0.026 0.241 0.052 0.052 0.004 -0.043	7 Nodal Diameters
-3.4 9.4 22.2 34.6 47.5 73.4 99.3	-0.112 -0.030 -0.181 0.017 -0.030 -0.043 0.043	-0.099 -0.259 -0.134 -0.03+ -0.172 0.056 -0.194	0.009 -0.069 -0.129 -0.043 -0.052 -0.017 0.022	-0.009 -0.134 -0.091 -0.043 -0.164 0.060 -0.233	9 Nodal Diameters

1)20 MIRRORS LOCATED AT 7 RADIAL POSITIONS

20 STRAIN GAGES LOCATED ON 10 C:FFERENT BLADES 16 BLADE MOUNTED HOT FILMS

1 STRAIN GAGE PER BLADE

32 HIGH RESPONSE PRESSURE TRANSDUCERS ON & DIFFERENT BLADES LOCATED TO OBTAIN MEASUREMENTS AT 7 RADIAL POSITIONS

2) 2 HOT FILM PROBES TRAVERSED TO 7 RADIAL POSITIONS

TOTAL AND STATIC PRESSURE. TOTAL TEMPERATURE, FLOW ANGLE ON ONE COMBINATION PROBE TRAVERSED TO 7 RADIA', POSITIONS

2 WEDGE PROBES TRAVERSED TO 7 RADIAL POSITIONS

- (3)4 INNER WALL STATIC PRESSURE TAPS
- 4 TOTAL PRESSURE, STATIC PRESSURE AND FLOW ANGLE 2 WEDGE PROBES TRAVERSED TO 7 RADIAL POSITIONS
- (5)2 COMBINATION PROBES TRAVERSED TO 7 RADIAL POSITIONS

3 DUAL TOTAL TEMPERATURE AND TOTAL PRESSURE PROBES WITH KIEL HEADED SENSORS LOCATED AT 9 RADIAL POSITIONS. THESE ARE LOCATED APPROXIMATELY 1200 APART IN A CIRCUMFERENTIALLY. ROTATABLE TRAVERSE RING THAT CAN BE POSITIONED TO PROVIDE AT LEAST 11 TOTAL PRESSURE AND TOTAL TEMPERATURE READINGS ACROSS A ONE ID STATOR VANE GAP AND TWO OD STATOR VANE GARS

- 6 STATIC PRESSURE 4 ID AND OD WALL STATIC PRESSUE PRESSURE TAPS
- (7) TIME VARIATION IN LOCAL MASS FLOE FLOW (Vz)

BY 2 HOT FILM PROBES TRAVERSED TO 7 RADIAL POSITIONS

- (8)2 WEDGE PROBES TRAVERSED TO 7 RADIAL POSITIONS
- 9 10 KULITE SENSORS

10 STATIC PRESSURE TAPS

(10)4 OUTER WALL STATIC PRESSURE TAPS

ADDITIONAL INSTRUMENTATION

GEARBOX

BOTOR ROTATIVE SPEED (RPM)

2 IMPULSE TYPE PICKUPS

INLET DUCT

FLOW RATE

CALIBRATED ORIFICE

ROTOR INLET

TOTAL PRESSURE

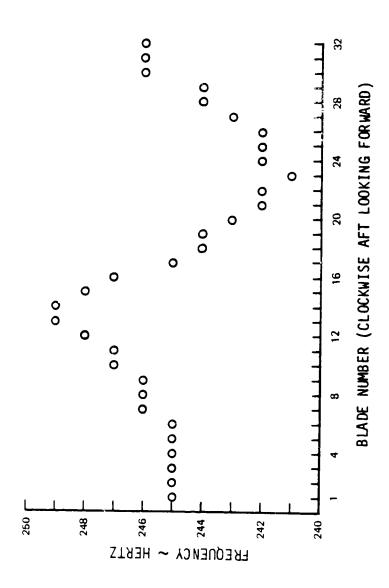
6 WALL STATIC PRESSURE TAPS LOCATED IN THE PLENUM CHAMBER

TOTAL TEMPERATURE

6 BASE WIRE CHROMEL ALUMEL THERMOCOUPLES LOCATED IN THE

PLENUM CHAMBER

Figure 1 Schematic Diagram of TS22 Rig



Distribution of Natural Second Mode Vibration Frequencies of Blades in Assembled Rotor Figure 2

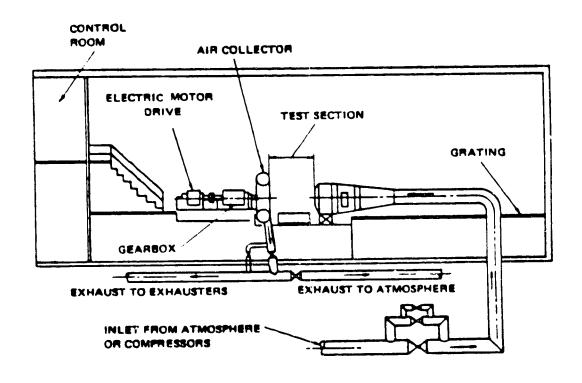
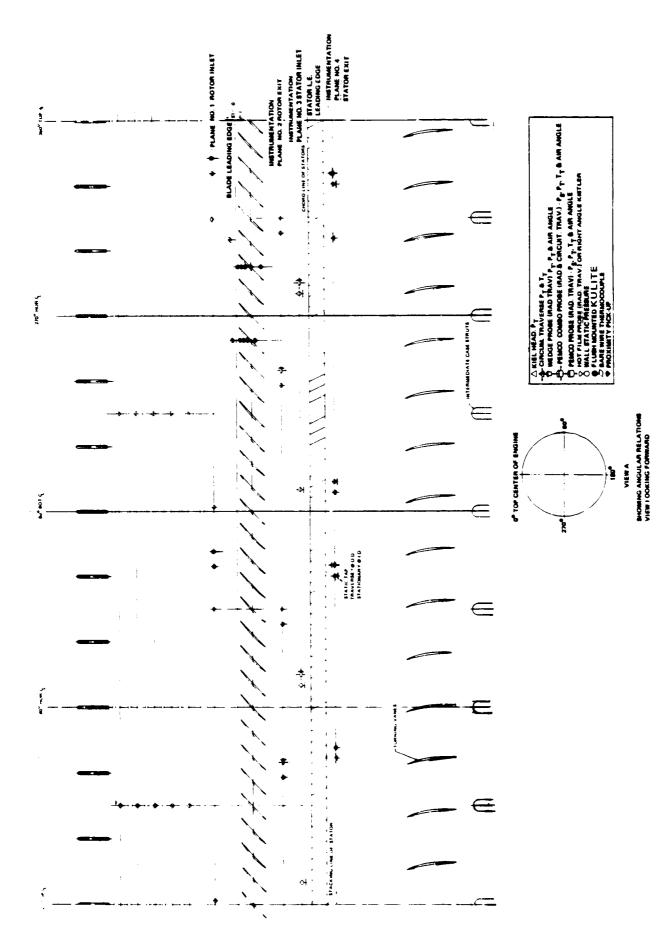
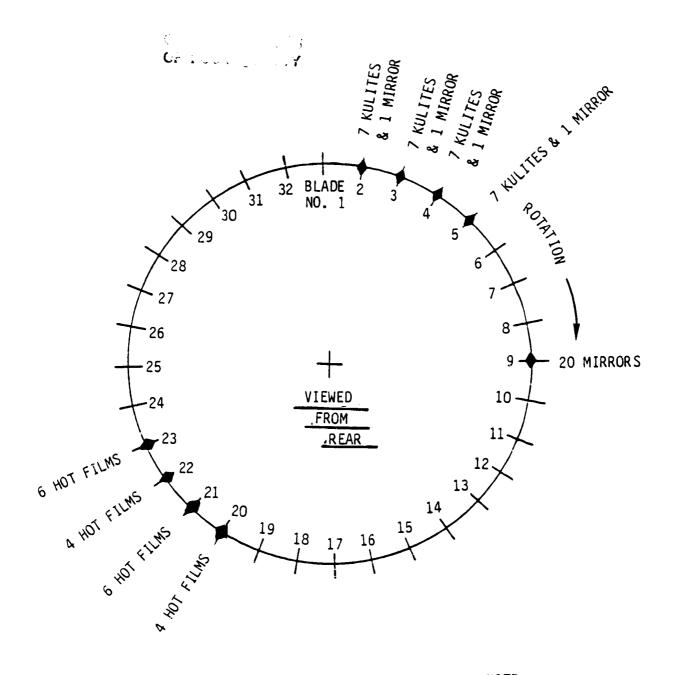


Figure 3 Schematic of X-204 Test Stand



Circumferential Schematic View of TS22 Compressor Instrumentation



NOTE
ALL BLADES HAD ONE
ASMT STRAIN GAGES

Figure 5 Circumferential Location of Blade Instrumentation

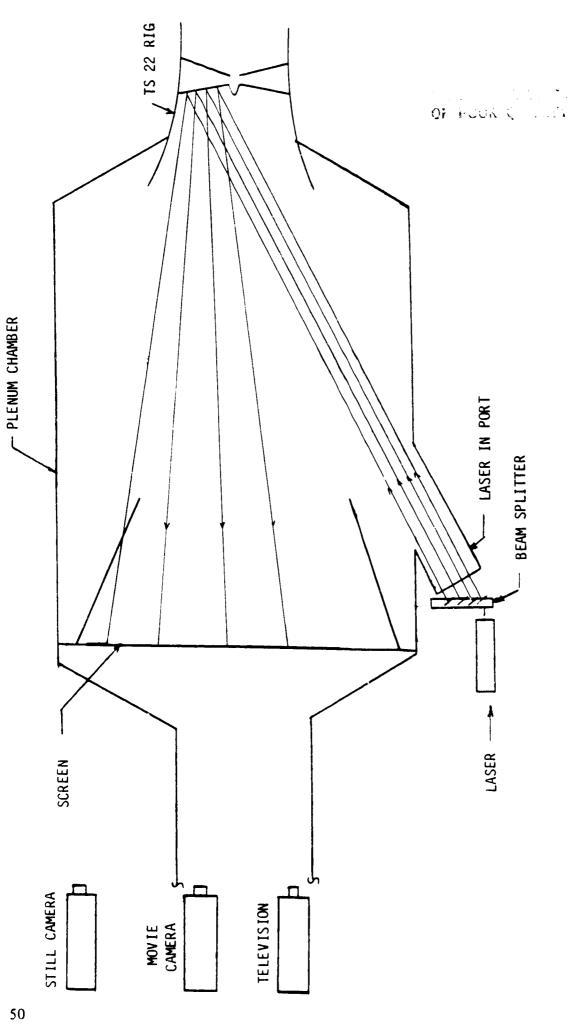


Figure 6 Schematic of TS22-X204 Laser Configuration

C			
C	6 - W.	 	7

BLADE NUMBER	PERCENT SPAN (a)	PERCENT CHORD (b)
2 3 4 5 9	86.3 86.3 66.0 66.0 95.2 86.3 76.4 66.0 55.0 47.0 38.0 20.0	50 50 50 50 50 5 5 5 25 50 70 5 25 50 70 5 25 50 5 25 50 5 25 50 5 25 50 5 25 50

Note: (a) Percent Span From Hub



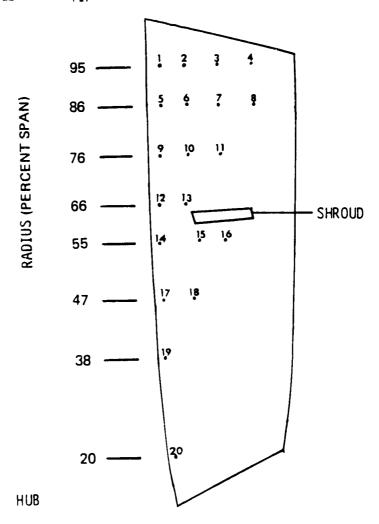
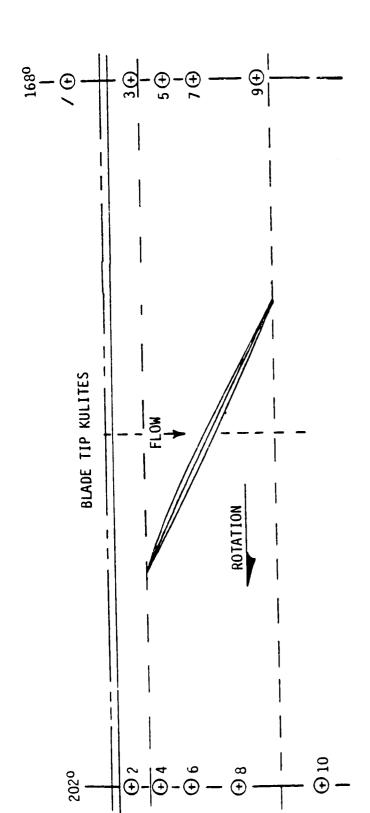


Figure 7 Mirror Installation Locations



PERCENT CHORD FROM LEADING EDGE	-55.4 -15.1 -3.6 9.4 22.2 34.6 47.5 73.4 99.3
ά	1680 2020 1680 2020 1680 2020 1680 2020
REF.	1 2 3 4 4 5 6 7 7 7 9

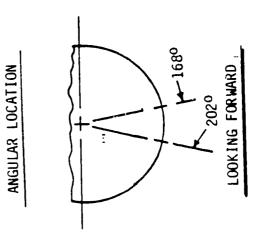


Figure 8 Installation Locations For Case-Mounted Kulite Pressure Transducers

LOCATION OF KULITE TRANSDUCERS ON BLADE SURFACE

Blade No.	Percent Span(a)		Pre		obe e Su		tion e	(Per	cent Suct	Cho ion	rd)(Surf	b) ace_	
2 3 4 5	76.4 76.4 86.3 86.3 86.3	5 5 5 5	15 15	25 25 25 25	40 40	65 65		5 5 5 5	15 15	25 25 25 25		65 65	

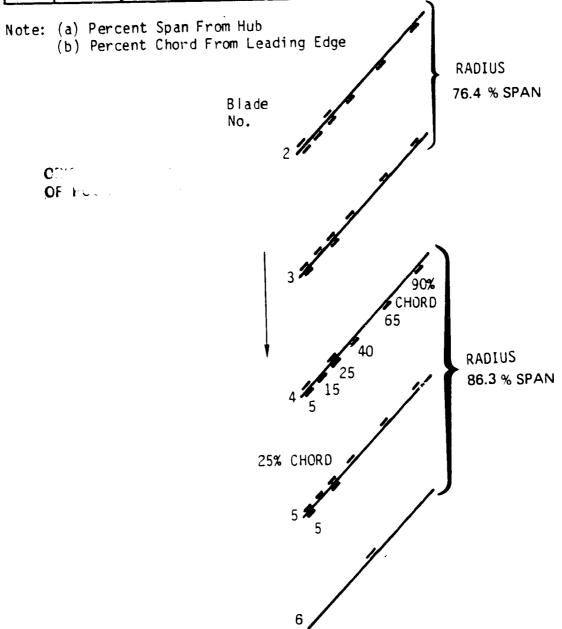


Figure 9 Installation Locations For Blade-Mounted Kulite Pressure Transducers

Location at Hot-Films On Blade Surface

Blade No.	Percent Span ^(a)		Probe Location (Percent Chord)(b)						
			Pressure Surface	Suction Surface					
20 21 22 23	76.4 76.4 86.3 86.3	5	40 40	5 5 5 5	15 15	25 25	40 40 40 40	65 65	

Note: (a) % Span From Hub

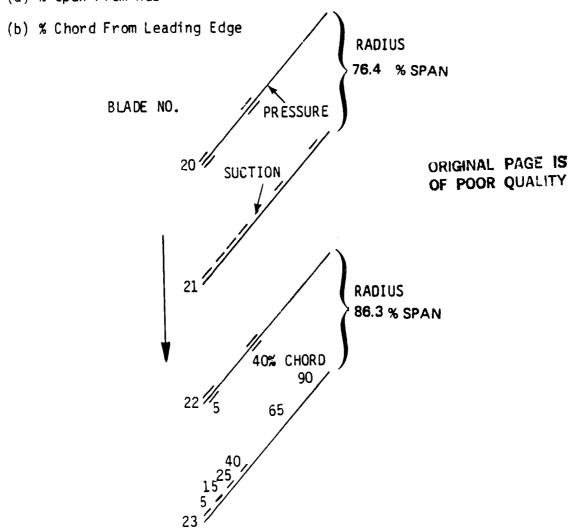
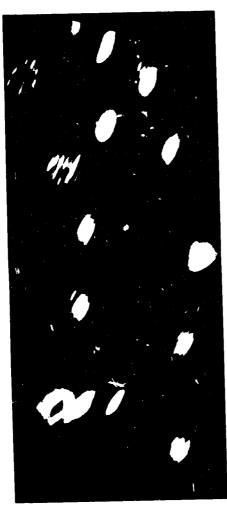


Figure 10 Installation Locations For Blade-Mounted Hot-Film Sensors

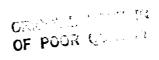


NO FLUTTER

FLUTTER

Figure 11 Typical Laser Mirror Results for Operation at 67 Percent Speed In and Out of Flutter

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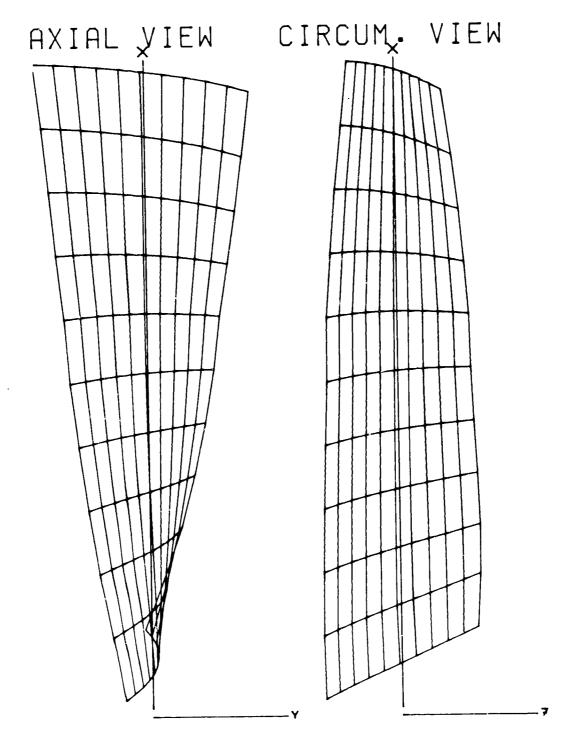
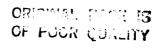


Figure 12 Finite Element Diagrams Used for NASTRAN Analysis



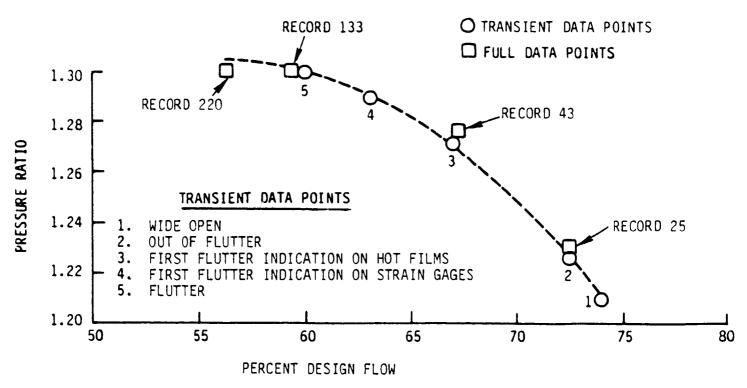


Figure 13 Identification of Data Points at 70 Percent Speed, Including Transient From Open Discharge Into Surge

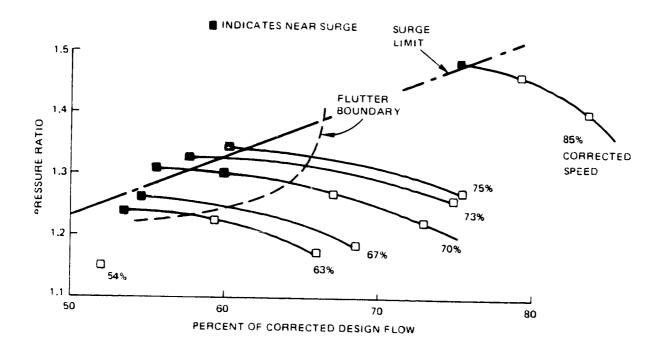


Figure 14 TS22 Performance Map Showing Test Points In Relationship To Flutter Boundary

Chiamines and

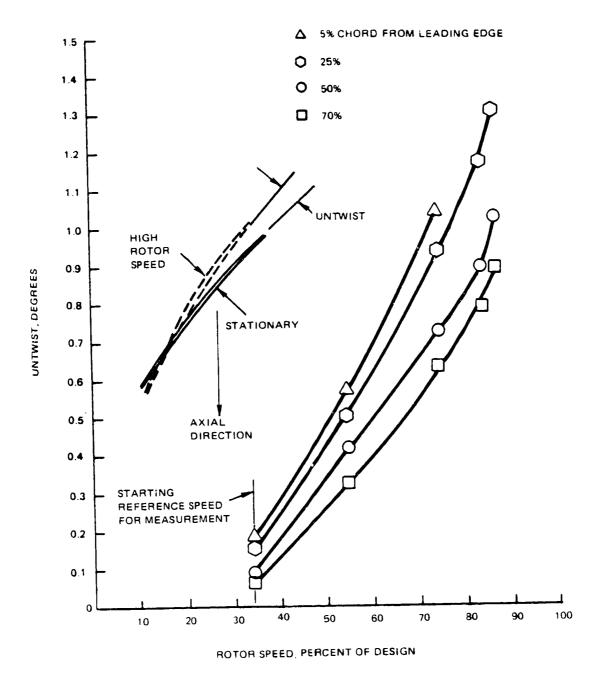


Figure 15 Measured Untwist for TS22 Fan Blade as a Function of Rotor Speed at 95 Percent Span



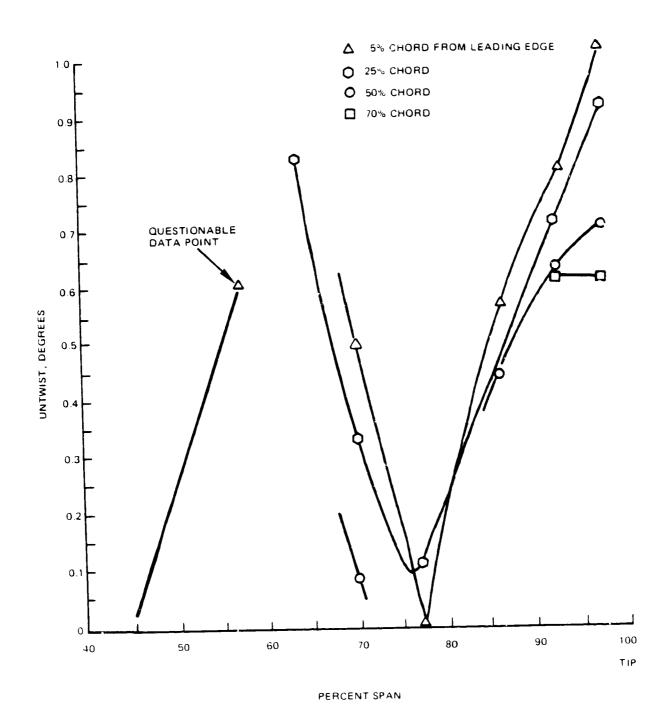
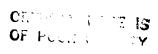


Figure 16 Measured Untwist for TS22 Fan Blade at 73 Percent Speed Relative to Untwist at 25.4 Percent Speed



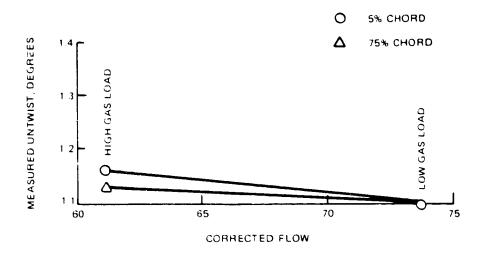


Figure 17 Measured Untwist for T322 Fan Blade as a Function of Flow Rate at 75 Percent Speed

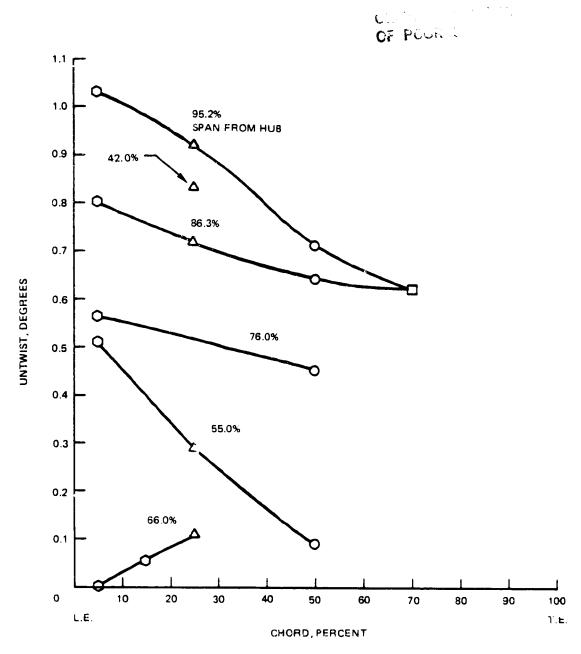
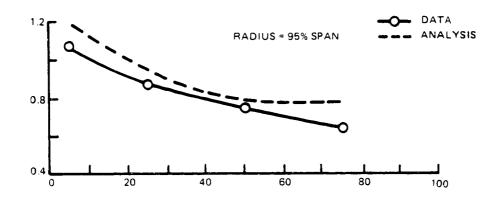
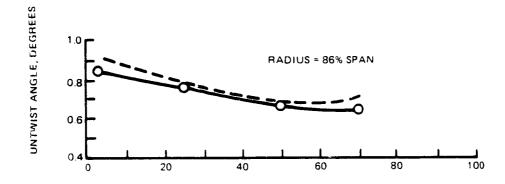


Figure 18 Measured Untwist for TS22 Fan Blade as a Function of Chord at 73 Percent Speed







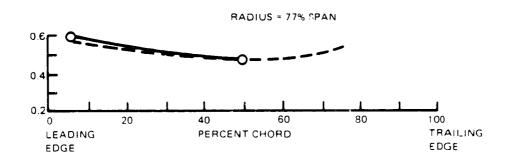


Figure 19 Measured Untwist for TS22 and Predicted by NASTRAN Analysis for Rotor Speed at 75 Percent Speed

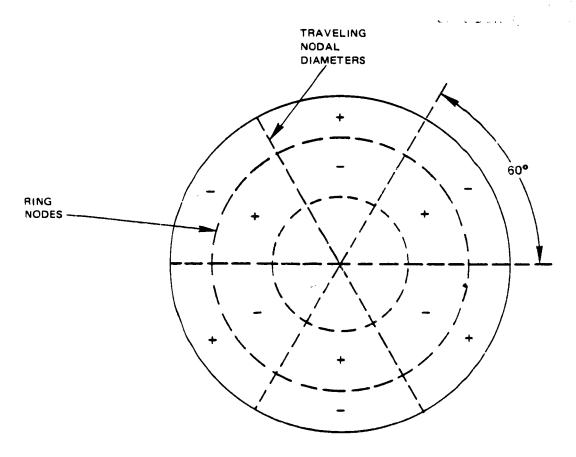


Figure 20 Three Nodal Diameter Pattern Second Mode - Previous theory predicted the presence of only one nodal diameter pattern at any time

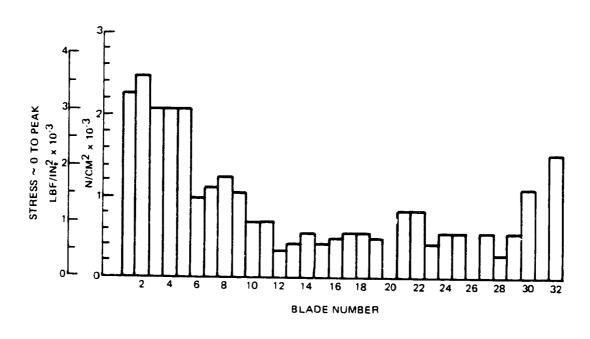
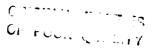


Figure 21 Blade Flutter Amplitude for TS22 Rotor at 67 Percent Speed From Strain-Gage Measurements

PHASE TO STRAIN GAGE NO. 3 ~ DEGREES BLADE NUMBER

Figure 22 Blade Flutter Phase Angles for TS22 Rotor at 67 Percent Speed From Strain-Gage Measurements



% MAXIMUM PRESSURE
CURVE CURVE
LRBEL VALUE
2 0.930000E+02
3 0.8 0000E+02
4 0.790000E+02
5 0.720000E+02
6 0.850000E+02
7 0.580000E+02
8 0.510000E+02
MAXIMUM STATIC PRESSURE
9.63 N/cm² (13.96 lbf/in.²)

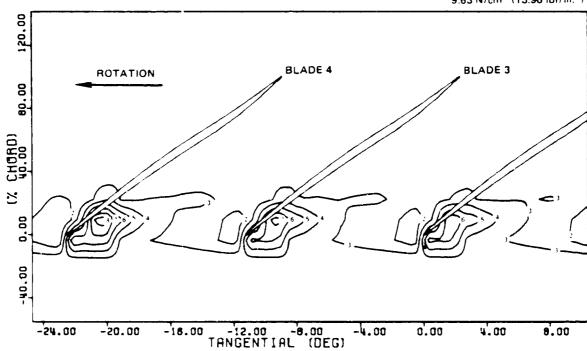


Figure 23 Steady-State Pressure Contours at Blade Tip at 63 Percent Speed Outside of Flutter on a Low Operating Line



% MAXIMUM PRESSURE

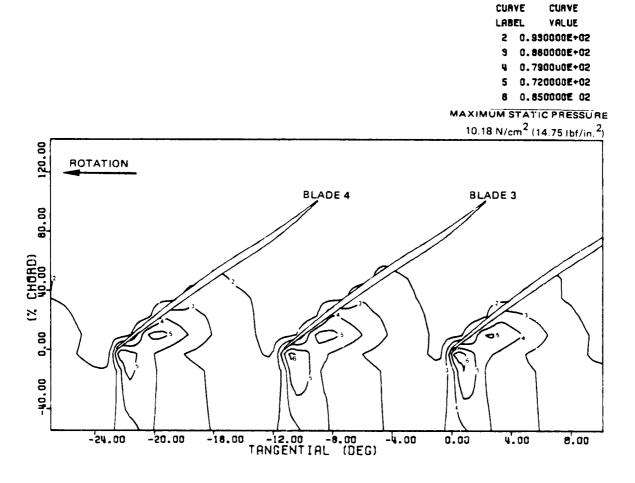
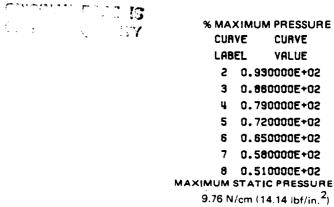


Figure 24 Steady-State Pressure Contours at Blade Tip at 63 Percent Speed Inside of Flutter on a High Operating Line



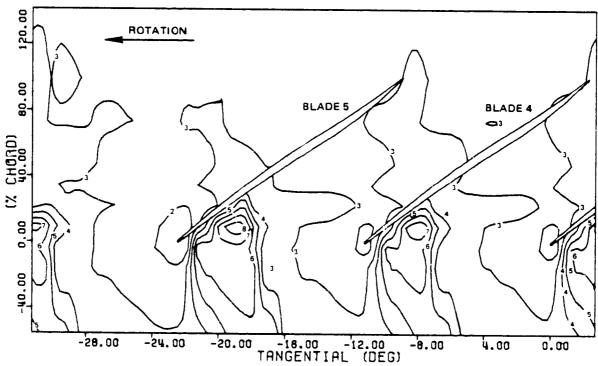


Figure 25 Steady-State Pressure Contours at Blade Tip at 67 Percent Speed Outside of Flutter on a Low Operating Line

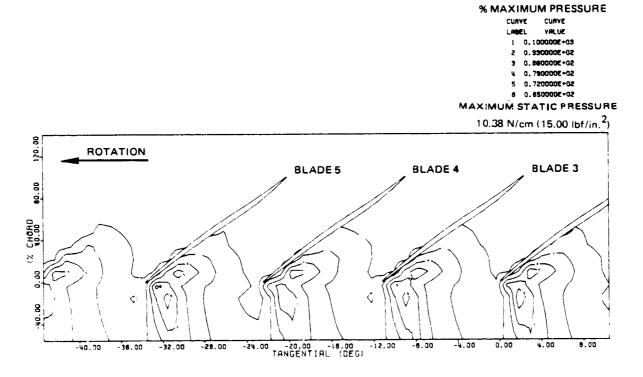


Figure 26 Steady-State Pressure Contours at Blade Tip at 67 Percent Speed Inside of Flutter on a High Operating Line



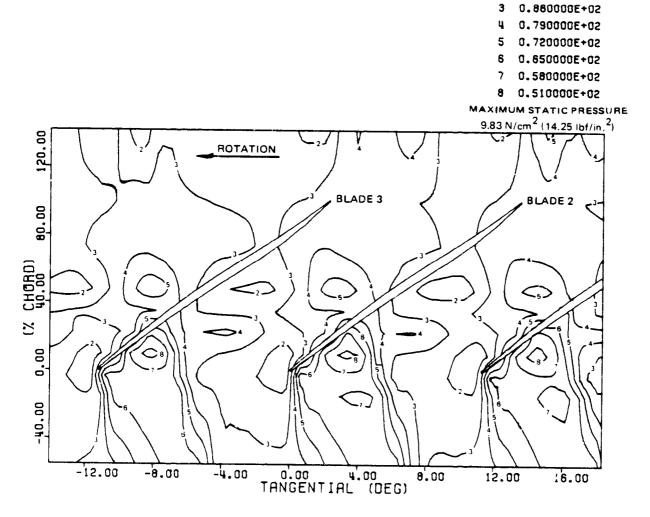


Figure 27 Steady-State Pressure Contours at Blade Tip at 70 Percent Speed Outside of Flutter on a Low Operating Line

% MAXIMUM PRESSURE

CURVE

VALUE 2 0.930000E+02

CURVE

LABEL

% MAXIMUM PRESSURE CURVE CURVE VALUE LABEL 2 0.3300000€+02 3 0.860000E+02 4 0.790000E+02 5 9.720000E+02 8 0.850000E+02 0.580000E+02 8 0.5100002+02 9 0.440000E+02 10 0.370000E+02 11 0.300000000 12 C.230000E+02 MAXIMUM STATIC PRESSURE 11.87 N/cm² (17.20 lbf/in.²)

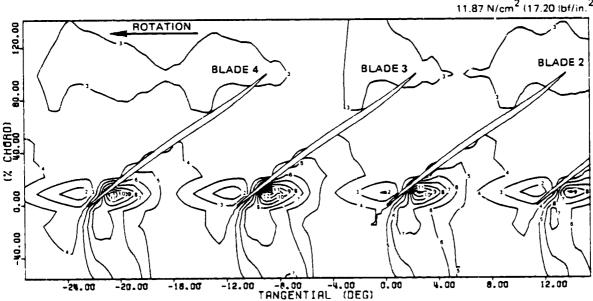


Figure 28 Steady-State Pressure Contours at Blade Tip at 70 Percent Speed Inside of Flutter on a High Operating Line

ONIOMATER LIGHTS ON MOUSE (COLOMY

% MAXIMUM PRESSURE
CURVE CURVE
LRBEL VALUE
2 0.9300000E+02
3 0.880000E+02
4 0.790000E+02
5 0.7200000E+02
7 0.5800000E+02
7 0.5800000E+02
MAXIMUM STATIC PRESSURE
10.43 N/cm² (15.11 lbf/in.²)

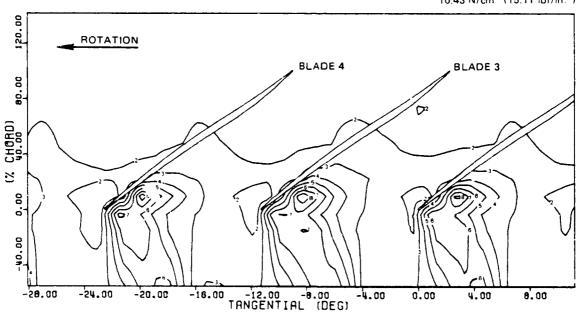


Figure 29 Steady-State Pressure Contours at Blade Tip at 70 Percent Speed Near Surge

% MAXIMUM PRESSURE CURVE CURVE LRBEL VALUE 2 0.930000E+02 3 0.980000E+02 4 0.790000E+02 5 0.720000E+02 8 0.850000E+02 7 0.580000E+02 6 0.510000E+02 MAXIMUM STATIC PRESSURE 10.25 N/cm² (14.85 lbf/in.²)

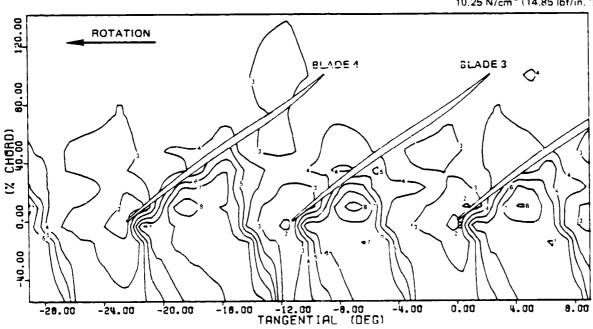


Figure 30 Steady-State Pressure Contours at Blade Tip at 73 Percent Speed Outside of Flutter on a Low Operating Line

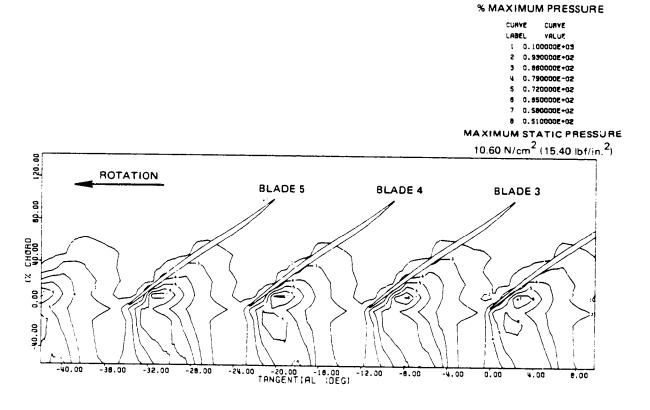


Figure 31 Steady-State Pressure Contours at Blade Tip at 73 Percent Speed Inside of Flutter on a High Operating Line



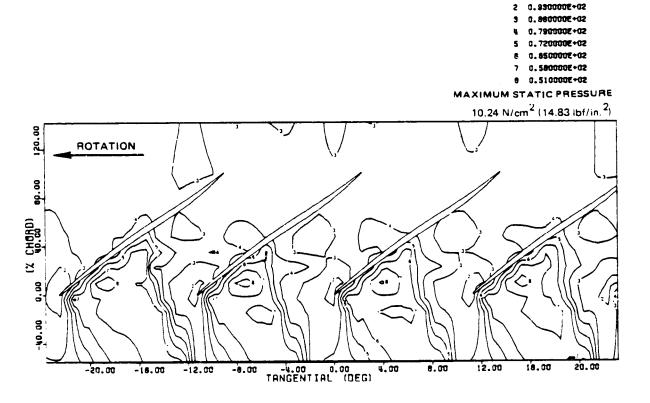


Figure 32 Steady-State Pressure Contours at Blade Tip at 75 Percent Speed Outside of Flutter on a Low Operating Line

% MAXIMUM PRESSURE CURVE CURVE LABEL

VALUE

C()

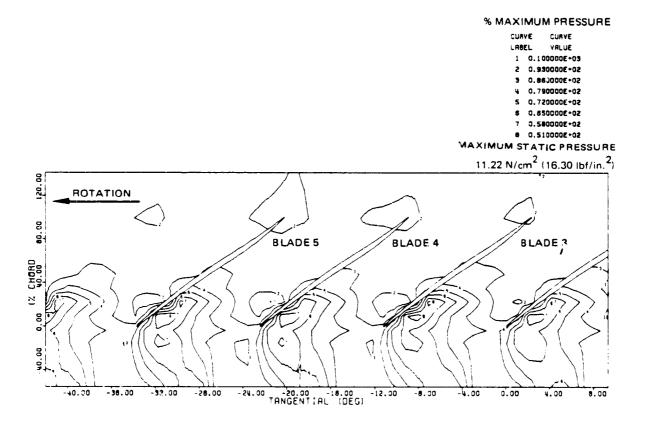


Figure 33 Steady-State Pressure Contours at Blade Tip at 75 Percent Speed Outside of Flutter on a High Operating Line

% MAXIMUM PRESSURE CURVE CURVE LABEL VALUE 0.930000E+02 0.860000E+02 0.790000E+02 0.720000E+02 0.850000E+02 0.5800000E+02 0.510000E+02 0.440000E+02 10 0.370000E+02 MAXIMUM STATIC PRESSURE 11.65 N/cm² (16.88 lbf/in.²)

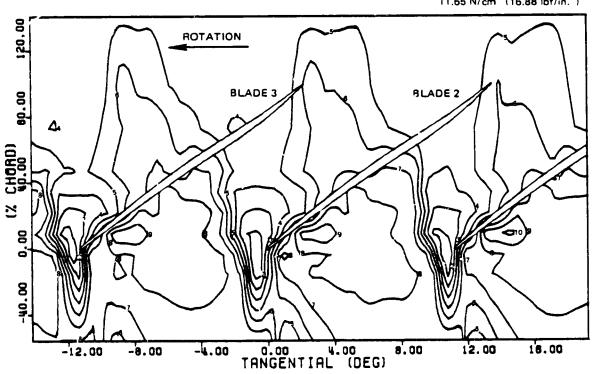


Figure 34 Steady-State Pressure Contours at Blade Tip at 85 Percent Speed Outside of Flutter on a Low Operating Line

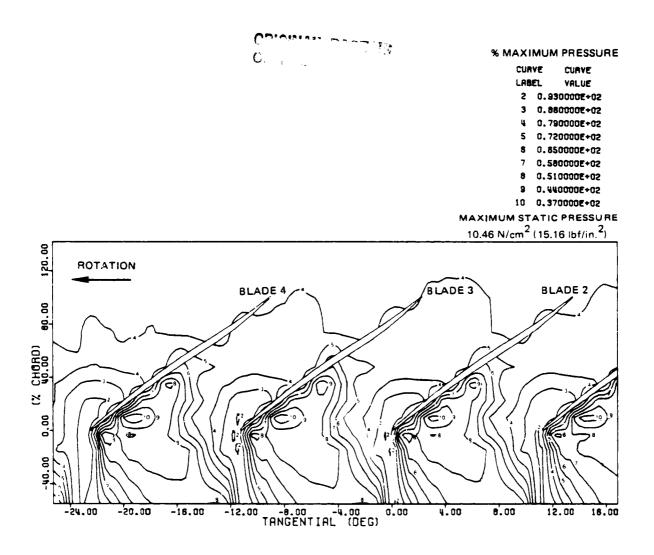


Figure 35 Steady-State Pressure Contours at Blade Tip at 85 Percent Speed on a High Operating Line

Objects of the second

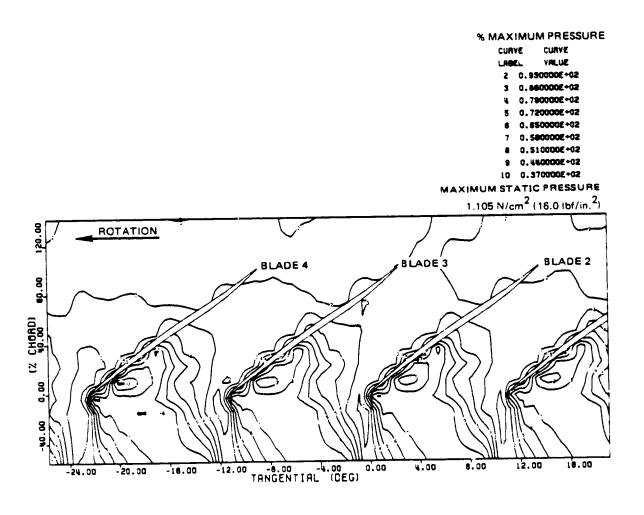


Figure 36 Steady-State Pressure Contours at Blade Tip at 85 Percent Speed Near Surge

ORIGINAL PLANTS OF POOR GULLITY

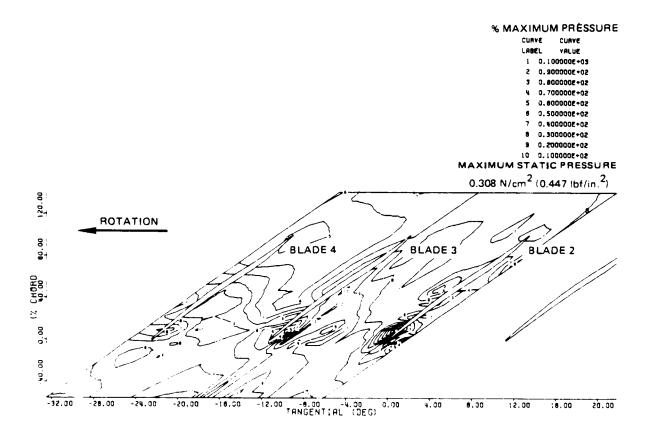


Figure 37 Unsteady Pressure Amplitude Contours for TS22 Rotor in Flutter at 73 Percent Speed



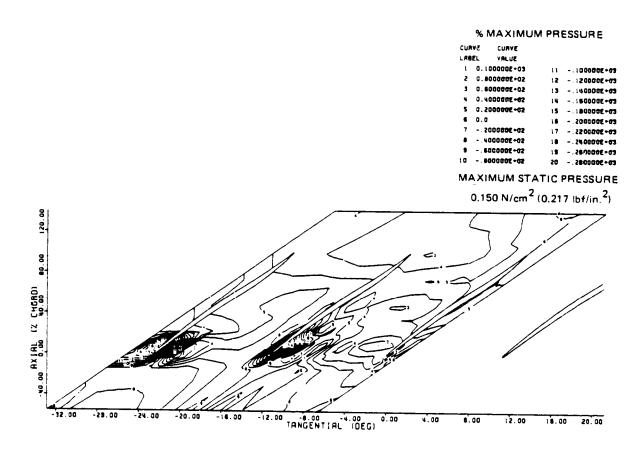


Figure 38 Real Component of Unsteady Pressure in Flutter at 73 Percent Speed



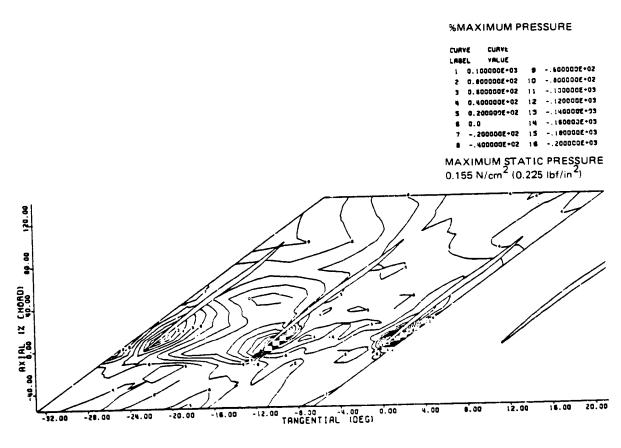


Figure 39 Imaginary Component of Unsteady Pressure in Flutter at 73 Percent Speed

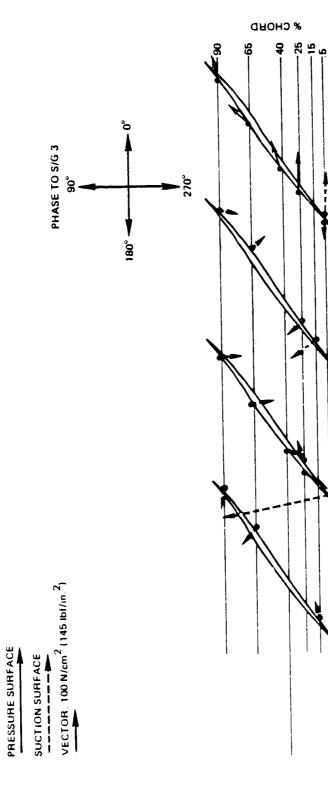


Figure 40 Blade Mounted Kulite Unsteady Pressure Amplitude and Phase Obtained in Flutter at 67 Percent Speed

and the little of

BLADE 2

BLADE 3

ALADE 4

BLADE 5

ORIGINAL FAGE IS OF POOR QUALITY

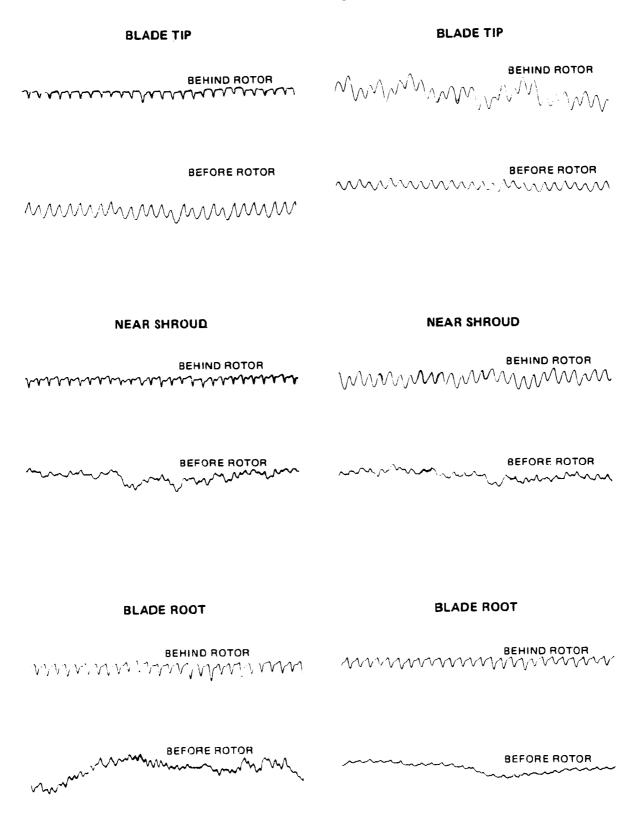


Figure 41 Signal Enhanced Wave Forms of Hot Film Probes at 73 Percent Speed (Noncalibrated Amplitudes)



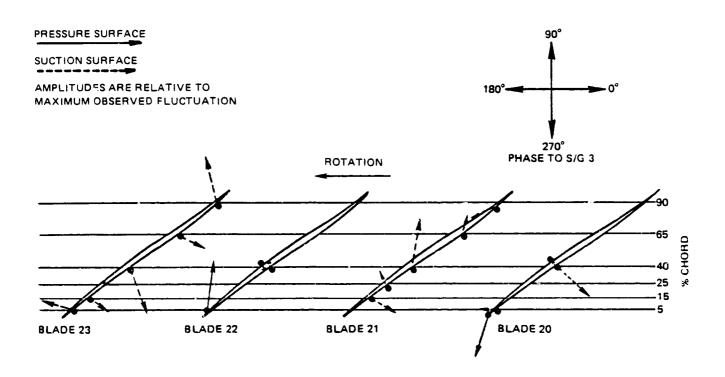
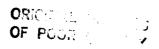


Figure 42 Blade Mounted Hot Film Unsteady Velocity Amplitude and Phase Obtained in Flutter at 67 Percent Speed



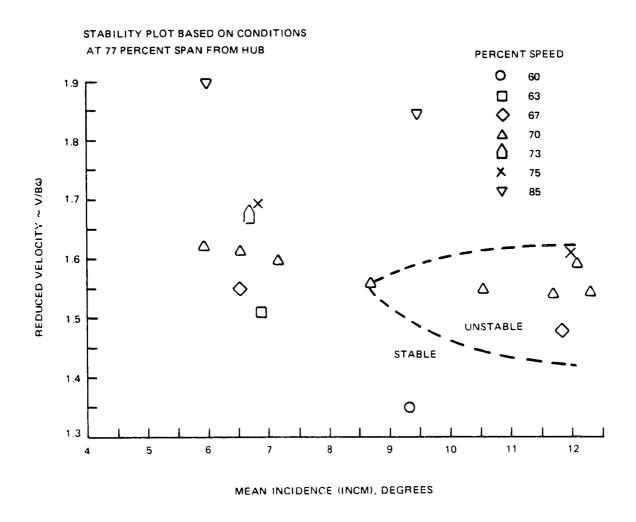


Figure 43 Observed TS22 Flutter Boundary Correlation of Reduced Velocity as a Function of Incidence

APPENDIX A OVERALL PERFORMANCE FOR TEST MATRIX (See Table A-1)

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TABLE A-1 1822 NASA FLUTTER TEST TEST MATRIX

Run Number	Speed Code	Point Number	Unsteady <u>Record</u>	Percent Speed	Percent Corrected Design Flow	Rotor Pressure Ratio	<u>Remarks</u>
					Shakeduwn All Hirrors	i	
001	72	01	20-27	70	72.8	1.228	Wide Open Discharge
		13 69	28	70	* *		Closing Discharge Maive, Transient into Flutter
001	70	05	43	70	66.9	1.2722	Check Point Wide Open Discharge
~~	7-0	••	64T	***	•-		Transient
003	63	31	71	63	65.8	1.1776	Wide Open Oischarge
003	63	03	26-84	63	53.4	1.2374	Stress Level Fluctuating, Shakedown Complete
					Performance All Mirrors		
003	73	01	86-94	73	74.7	1.2687	Wide Open Discharge
003	73	02	100-108	73	60.0	1.3317	Maximum Flutter
				4 Rows	3 Wait Lase Mirrors (Abov		
904	70	03	128-135	70	59.8	1.3004	70% Low Flutter Point
004	67	01	136-143	67	68.5	1.1890	Wide Open Discharge
004	75	31	176-183	75	75.3	1.2840	Wide Open Discharge
0 04 0 05	75 73	04 08	195-202 220	7 5 70	60.3 5 6. 5	1.3369 1.2978	Maximum Flutter
					All Mirrors 3 Watt Lase		
007	6 6	01	239	6 6	54.5	1.26	Maximum Flutter
007	60	01	242-249	55	52.0	1.1530	Near Surge (Rotating Stall)
007	85	02	279-286	85	85.8	1.3/92	wide Open Discharge
		••	287	~-	92. 64		Transient To Surge
007	85	05	288-295	85	75.1	1.4862	Near Surg e

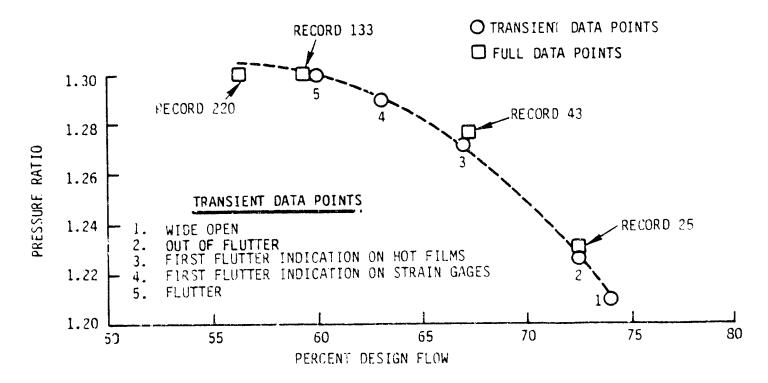


Figure A-1 Identification of Data Points at 70 Percent Speed, Including Transient From Open Discharge Into Surge

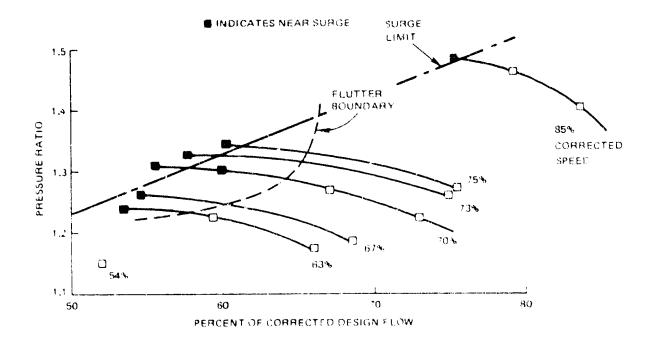


Figure A-2 Compressor Map Showing Test Points In Relationship To Flutter Boundary

AERODYNAMIC SUMMARY NOMENCLATURE

v-1	v_1	Air velocity at station into rotor
V-2	v_2	Air velocity at station out of rotor
VM-1	$v_{m,1}$	Air velocity at station into rotor in meridional direction
VM- 2	v _{m,2}	Air velocity at station out of rotor in meridional direction
V <i>θ</i> −1	\mathbf{v}_{θ} , 1	Air velocity of station into rotor in circumferential direction
V <i>θ</i> −2	$v_{\theta,2}$	Air velocity at station out of rotor in circumferential direction
U-1	\mathbf{u}_1	Rotor tangential speed into rotor
U-2	u ₂	Rotor tangential speed out of rotor
V'-1	v' ₁	Air velocity relative to rotor at station into rotor
V'-2	v ' 2	Air velocity relative to rotor at station out of rotor
Vθ'-1	ν' _θ ,1	Air velocity relative to rotor at station into rotor in circumferential direction
Vθ'-2	ν' _θ ,2	Air velocity relative to rotor at station out of rotor in circumferential direction
RHOVM-1	$\rho_1 v_{m,1}$	Product of air density and air velocity in meridional direction at station into rotor
RHO VM−2	ρ ₂ Ψ _{m,2}	Product of air density and air velocity in meridional direction, at station out of rotor
EPS I-1	ϵ 1	Angle between tangent to streamline projected on meridional plane and axial direction at station into rotor
EPS I-2	$^\epsilon$ 2	Angle between tangent to streamline projected on meriodional plane and axial direction at station out of rotor

(, , , , , , , , , , , , , , , , , , ,	 •	•	
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PO/PO	P ₂ /P _{in}	Ratio of total pressure leaving rotor and entering rig
B-1	β_1	Absolute air angle at station into rotor
B-2	β_2	Absolute air angle at station out of rotor
B'-1	β'1	Air angle relative to rotor at station into rotor
B'-2	战 ' 2	Air angle relative to rotor at station out of rotor
M-1	M_1	Absolute Mach No. at rotor entrance
M-2	M_2	Absolute Mach No. at rotor exit
M'-1	M' ₁	Relative Mach No. at rotor entrance
M'-2	M' ₂	Relative Mach No. at rotor exit
INCS	i _{ss}	Incidence angle between inlet air direction and line tangent to blade suction surface at leading edge based on calculated metal angle for design speed
ICM	i _m	Incidence angle between inlet air direction and line tangent to blade mean camber line at leading edge based on calculated metal angle for design speed
DEV	δ°	Deviation angle
TURN	ρ'1-β2	Change in relative air angle entering and leaving rotor
D FAC	D	Diffusion factor
OMEGA-B	ವ	Total pressure loss coefficient
LOSS-P	ῶcos μ' 2/2 σ	Loss parameter
EFF-P	" p	Polvtropic efficiency
EFF-A	ⁿ ad	Adiabatic efficiency
WC 1/A1	$W_1 \sqrt{\theta_1} / S_1 A_1$	Corrected flow
ΓΟ/ ΤΟ	r_2/r_{in}	Ratio of temperatures leaving rotor and entering rig

TABLE A-2

AIRFUIL AERUDYNAMIC SUMMAKY PRINT

							AIKFULL	AIKFUIL AEKUDINAAIC		14400							
55 %	55 Percent Speed	peed									X S	KUN NU 7		SPEED CUDE 60 PUINT	٦ ت		
					- 1	1	<u> </u>	1-1		>-• A	1-191	781	AHUVH-1	KHUVM-2			Pu/P0
7	- ·	7-5	- K	1 / 1 / 1 / 1 / 1 / 1 / 1 / 1 / 1 / 1 /	7 0		14/14	ا ا	M/SEC	יונ	水水の	M/SEC	KU/MZ SEC	KU/HZ SEC			וארבו
	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	7/36/6) / 	3,511		102.2	7		151.2		- 102.3	-13.4	106.08	15.4.31	0.3666	2,52,72	1.1458
• •			,)	***	416.5	125.7	144.4	110.5 -	-110.5	-34.B	71.111	130.16	0077-0	21117	1.51.1
•	2	7 - 7 - 1	1 0	10.0	3	20.0	1,11.4	136.4	103.1		-131.9	-54.0	112.75	126.70	1961-0	244	7111
٠,	,	1 1 7 1		104.5)	4-00	1.74.5	1+1-0	7.71		1.7.1-	× 19-	113.40	120.53	45410	4/100	1010
• •		124.7	3	10.17	3	75.4	157.5	101.7	100.3			- aa-	115.63	130.4		1	1561-1
٠ ٥	, 60%	0.0	10.1	101.0	,	14.0	175.5	110.0	200.4			B-101-	113.14	27.001		2750-01-	1.1674
~	7.5	136.	10.1	104.4))	11-1	175.4	47.5	4.612	٠ . د د د		4. CII-	113.14	30.00		126040-	1.1640
- 49	9	1.521	£ . t	1.5.1))	70,7	71017	8.207	731.0	0.1	- 1017-	7.101-	110.67	127.36		1101.0-	1.1614
•	4 - F	1.221	7	101.7		9.99	7117	213.5	7000			4 4 4 1	108.64	125.45		-6,1471	1.1554
2	71.	117.0	71.4	10.0	3	4	4,55.5	771	9.00			-167.7	167.18	123.59		-0.1574	1.1555
11	•	110.4	;	711.5))	3.0	4.51.5	731.4	2010		. ~	-115.1	164.45	114.30		-0.1527	1-1104
:	90	411.5		9.7.) :) .	* 1 0 /		7.04	707.07			-140.4	105.34	106.65	-0.1440-	-0.1782	1.1419
1.5	7.10	100.3	./:	1.03	•	•		•								,	
:	1	í	1	7-17	1-6	7-W	7 4	7W			DEV	TURN	U FAC OM	OMEGA-B LUSS-P	7794 4-	\$EPF-A	TOTAL
	4 - O			DICKE								DECKE.		c	-		
		_			0.1.10		1.4002	0.3104	2.1	4.53	70.61	90.		2000-0 KECO-0	-		
• `	3		51.15		7617		7 6664.0	4.3430	4.54	7.78	۲٥°٠	32.63			• -	,	
. ~	3		77.5) 160*.7	0.3×0b	4.86	7.51	12.40	77.97	0114				
•	3	4-64	55.91			. soul		0.3584	2.50	6.4	97.14		7514-0		•		
• •	3	16.1	56.70				4.5516	6696.0	5. VC	71.6	0.0				-	6	
ه ۱	3	4.61	41.12	42.40		21 06.		9674.0	2.5		9.4	15.66	0.3020	2020	• -	86.1	
•	3		15.00	+1 -1+				55.4.0	0.03	3.			4	477			
			11.50	23.40	K097.0			C874.0	6.00	2	•	00.				9	
, ,	3		10.00	24.44	U. 2105	2000.0		7616.0	2.0	¥. 54	,	11.03		3 4			
0	2		25.00	20.05	101200	71.6.0		0.55.0		14.0	71.6	2 :	7076				
: =	3	1 1	33.00	24.70	6002-0	400000		0.5020	6.13	6.00	1.0	77.6	76.26) =	-		73.9
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?	•	•							•	•	1 9 47 77	C = 0 = 0	T WATER A	RHUVM-2	£P51-1	EPS1-2	FC 18
ż	7-7		7-47	7-WA	1-01	7-01			1 - 1	7 7	1 2 2 3	145/14	AMAZET ZSEC	7		UEGREE	SPAN
	F1/3r	r1/560	+1/3EC	r1/ sec.	rl/sec	+1/3tl					2 4 4 4 1	2 4	22.14	20.4	_	14.650	0.0710
4	3.006		2.0.6				355.6	* * * * * * * * * * * * * * * * * * * *	1 2		4,744	-114.2	22.76	56.66	12.949	4.8cb	6.1592
7	30.4.3	,	2000	3.4.0			707	0.144			D + 7 C +	-114.1	23.13	20.30	115-8	5.001	L.2424
•	514.7	,	7.44.7		2 1		7 7 7 7	7,141	3,436		-460.2	-421.5	23.52	20.32	0.5.0	3.15%	0.0055
•	712.7		910	7.055		7	4 4		77119		-526.0	4-647-	23.27	20.07	3.406	1.1%	21050
^	310.			2,44		2	5.25.4	577.5	657.5		-575.9	-340.6	23.30	26.65	199.0	563-0	7007-0
•	211.		•			•	*	411.5	768.5	511.7	-634.4	-376.5	73.17	77.77	194.1-	094-7-	60000
-	010) : ; ;			671.1	0.200	150.0		-691.1	4>00-1	90-27	46.00	497 · 104	75.510	2000
.	⊸ .	7-712			, ,	225.2	112.2	200.	1.011	560.0	- 114.2	1.475-1	11.77	54.07	15.151	7/1.0	00.73
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2 :	3 7	767.		1 7 6))	7007	110.0	7.651	433.5		-710.0	£.04¢-	54-17	15-67	10.514	10.46	6.5275
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12.17.1	•		5.1682	_	3.3	6-5123				7	6.1.13	5:1:5	6.101.9	0-1650	24.6.1.0		4.5 6 6	•				****			3.16			5 65.8V						2-1543			4.6.53	7.00		***	471-1-	2000	20.00	3	370		2/3 - 27 -		1	1 5	5	•	2.36
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TABLE A-4

AIRFOIL AFRODYNAMIC SUMMARY PRINT

4/5EC 4/5EC 4/5EC 6/5EC	U-1 W / V-1	V-7 V/SEC M/SEC M/SEC M/SEC M/SEC M/SEC M/SEC M/SEC M/SEC	7 / 2 / 2 / 2 / 2 / 2 / 2 / 2 / 2 / 2 /		¥	RHDVM-7 RG/H2 SEC 129-65 130-74 131-47	RADIAN 0.3116 0.2322	RADIAN 1 0.2467 1 0.1529 1	1.2054 1.2054 1.2067
103.103.3 103.3 103.3 103.3 103.3 103.3 103.3 103.3 103.3 103.3 103.4 102.4 102.4 102.9 103.3 103.9 10	MYSEC 1119.1 1152.4 1152.4 1152.4 1164.8 1164.8 1164.8 1164.8 1164.8 1164.8 1164.8 1164.8 1164.8 1164.8 1166.9 116	7 X SEC M X 3 3 3 5 5 6 7 5 6 7 5 7 6 7 6 7 7 6 7 6 7 7 6 7 7 7 7	M/SEC 109W-0-1 1106.24 123W-6-1 136.64 148.66 1161.34 193.54		112.23	129.65	0.311	67	2054
103.3	114.1 114.6 1154.8 1154.8 1154.8 1163.9 200.7 20	33.6 156 166 167 167 167 167 167 167 167 167 16	103.9 108.2 116.4 123.4 136.6 148.6 161.3 175.9		114.9	130.74	: 22	53	2047
107.7	134.6 1152.3 11614.8 11614.8 222.3 222.3 222.3 202.4 202.4 202.4 202.4 202.4 202.4 202.4 202.4 202.4 203.4 2	445.2 16 59.9 18 19.7.6 20 19.7.6 20 10.4.0 22 10.4.6 22 10.2 28 10.2 28 10.2 28 10.3 30 10.3	107.7 117.7		• • • • • • • • • • • • • • • • • • •	131.47	ž		1000
107.7 0.0 10. 11. 107.7 0.0 10. 11. 107.4 0.0 0.0 11. 107.9 0.0 0.0 11. 107.9 0.0 0.0 12. 107.9 0.0 0.0 13. 107.9 0.0 0.0 14. 107.9 0.0 0.0 15. 107.9 0.0 0.0 16. 107.9 0.0 0.0 17. 107.9 0.0 0.0 18. 107.9 0.0 0.0 19. 107.9 0.0 19. 107.9 0.0	152.3 1154.8 1203.9 1203.9 1203.3 120	100 100 100 100 100 100 100 100 100 100	116.4 173.4 143.6 161.3 175.9			131.47		,	
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105.9 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	202.7 202.3 202.3 200.4	7004.0 77 72 23 24.6 20 29 29 29 29 29 29 29 29 29 29 29 29 29	148.6 161.3 175.9 182.4 193.5		110	10000	? 2	5	2294
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11	269.4 224.0 225.0 225.0 205.1 41 41 6.64.9 6.64.9 6.64.9 6.64.9 6.64.9 6.64.9 6.64.9 6.70.0 6.71	766.5 20 766.5 20 796.6 7.2 29 796.7 20 796.7 20 79	182.4	_	114.	140-23	Я.	7 6	17071
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(FF () SYFE	0.5495 0 0.5306 0 0.5306 0 0.5306 0 0.5170 0 0.720 0 0.720 0 0.720 0 0.720 0	2		>	0 540	A-8 LOS	S-P P02/	TEFF	ų.
77	0.495 0 0.5326 0 0.5326 0 0.53702 0 0.53702 0 0.54702 0 0.7260 0 0.7260 0 0.7260 0	2000 2000 2000 2000 2000 2000 2000 200				OTAL TO	٨٤ 8	_	TOTAL
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94 72.5P 0.2544 0.4 151 40.75 0.2946 0.4 194 40.07 0.2937 0.4 17	0.3707 0 0.5136 0 0.7260 0 0.7760 0 0.7760 0 0.7760 0	4 7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	77.77	76 98	, 4	0524 0.	1.2	76	46
.61	0.6697 0 0.7247 0 0.7267 0 0.7769 0 0.7769 0 0.7769 0 0.7769 0	3960	1 7 - 7 1			0 7770	-	6	93
.94	0.6697 0 0.7240 0 0.7769 0 0.7769 0 0.7769 0 0.7760 0	8 797 8 8797	11.98	3		7700	-		6
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V 1-67 V-17		U-2 (1-1	۸۰-2	01	RHOVA	AH.	EPS1-1	EPSI-2	PCT TE
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1 773.3 6.0 36		4.9	355.1	7	23.5	26.18	٠, ,	101.0	
3 237.0 0.0 34		4.3	381.9	7	23.8	76.93		3.275	
9 336.7 0.0 33		٥.2	404.9	ï	73.6	20.17		0.0	
1 339.3 0.0 32		613.5 686.0	449.3	-603.5 -293.6		27 26	0.00	44.0	5005
.6 335.5 0.0 31		9.3		ï			- 2	71d C-	
7 347.0 0.0 3		6.3	\$29.3	Ü	23.8		76	7 7 7	
7 2.0.8 0.0 3.		7.5	5,00,5	7	23.5	7, 00		414 4-	
.7 347.4 0.7 27		8.8	4.60%	ī	2.5	26. 26		9.040	
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18 0.0 P. 213. F.			640-1	1	55.6	25.69		10.61	֓֞֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֓֓֓֜֜֜֜֜֜֜֜֜֜֜֜֜
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1 6770 1-2	174 93.97	•4.35			1.0749	1.23/4	23.62	4.33	

TABLE A-5

AIRFOIL AERODYNAMIC SUMMARY PRINI

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TABLE A-6

AIRFOIL AERUDYNAMIC SUMMARY PRINT

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					1001.0			1617.0-					-4.1662	-0.1653	-6.1495	21 F F - A	1717	43.64	44.68	43.77	44.13	44.54	50.73	84.77	64.09	86.65	1.77	26-96	0 //	61.38		THE CALL	14.775	9.0.6	5.646	471.7	5.0°0	45001-	467.6-	7.5.4	3000	141.6-	-10.613	-11-43		<u> </u>	keluR •	a 3	00.00	
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	2				0.7235	15.1.3	4547	6107"	-0.0384	-0.6663	-6.1044	-4-1511	-0.1626	-1.1875	-0.1964	٩	٠.	-	_		_	-	-	_	_		~	_	-4	1 227				12.	20	ف	1	ذ	~	į.	ñ #	ן כ	10	=	•	EF F- AU	KG CK	. •c	66.33	
	POINT	VM-2	KG/M2 SEC	173.68	1738	171.99	17:21	77071	17,25	172.57	170047	64.93	62.18	50.05	40-75	,	101	-												70.0		KHUVM-2	76 1235	35.71	35.22	35.04	35.27	35.11	35.54	35.34	34.71	9000	22.00	2 2 2				į	1.1690	
	DE 67				ź	7			-			<u> </u>	10	-	14	4	CHECALD	101AL	77.0		2447	774	1 2 3	36.63.11	1997	2000	C. 6761	6.0843	6.1156	c.1391																1 PO27PC1	•			
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	, K		7-, 44	7 25 / 4	-134.6	-156.0								-284.9			UEV	Dr.GASE	14.08	13.09	11.19	10.02	46.7		50.0	000	, ,	77.7	2.4	5.92		ve1	FT/St C	-402.1	-456.1	-516.5	100-		-760.1	-628.1	-653-3	-417.1	4.766	-470-0	-464-					
SUMMER			7	#/>EC 7											2 .5	•	INCH	ı.	5.66	5-39	5.38	5.50	5.61	5.74	6.33	6.55	90.0	14.0	000	6.23	•	V 2			492.3	215.0	5.46.V	7 . 6 . 7	4644	73H.5	159.9	814.2	826.3	\$	863.9					
							_											E 0E						7.5.	.36	19.	4	- :	12.	75.	•	7	•			675.3				7.10	1010	1003.6	1010.7	1047.3	÷					
N N N N				M/SEC	-	٠,				7	~				319.2		INCS	50	3	٥	_	_	_	~	M	~	m.	4 .	•	* ·		>	_												69.7 166		LFF-F	- J	96.98	
LAERC			0-2	M/SEC	136.0	20.04	176.8	3.44	211.6	230.6	0.6+2	255.7	272.8	211.2	268.1	C*C67	M 0 - 2	:	0.428	0.4-08	0.460	0.4905						0.7212		0	0791-0	2-11	+		494.3					1,000				5	•					
AIRFOIL AERUDYNAMIC			<u>-</u> 1	H/SEC	122.6	137.0	171	8 0 0 1	210.3	231.1	252.4	260.1	219.5	284.3	295.6	30 3.1	1	•	6.5225	4.96.3	0.4141	0.6452	0.6424	0.7410	0.7940	6.6453	4.6646	0.5111	0.9227	6676.0	0.9679		1775	402-1	458.1	518.5	561.0	1.979	0.0	1.00	652.3	617	23.75	970.0	5.466		F F F	- L L	er .C	
•			7-2	1/SEC					73.2	61.5	0.17	.8.3	62.6	4-1-4	57.1	7.8	•	į	18.5	190		54.6	417	019	46.46	4512	4436	1474	170		3696		744	- 1	9.13.5	312.9	2.43.3	268.6		267.3	2000		4-1-2	3	9,	•	Pt./PG	11:11		2561-1
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			1	M / SE C	125.5	127.5	131.9	132.4	32.3	136.1	1.161	1.4.1	7.5	12.2	120.4	115.4		_	4	7 1	7.	٠, ٠	"	7 7		ניט	7	, ,		67.74	٠:		1-H^	F175t	. 1 .	* 7 4	436.	,	433.	430.	423	42C.	4.04	404	7.5.6	9	MC1/	X6/3	20 S	134.6
		Speed	, ,					2	•		7	^			34.40	٠.٠		2-6	CB LE	34.9	36.5	34.0	32.6	30.4	5.6	2	24.7	26.3	25.0	26.0	26.4		7-1	2.8/1	622.1	79 h	276.4		518.2	5.9.5	506.1	3-4:4	4.7E.B	4/1.0	441-0	0.61.	(1/41	IM/SEC	1.400	24-42
		9000	;	`	, ₍	1.5	٠	4-3	5.3		31.1	-		:	7 4			7-	4	0.0	0.0	0.5		်	၁ ၁	٠ •)	ء د د	و د د	2		•	_	ر		<u>ت</u> ا	•		1 5 5	0.00	23.7		o.		0.5	4-881	3	. <u> </u>		-
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TABLE A-7

AIRFOIL AERUDYNAMIC SUMMARY PRINT

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	PO/PO INLET 1.2416 1.2546 1.2265 1.2263 1.2263 1.2432 1.2432 1.2251 1.2134 1.1977		PC1 1E SPAN 0.0916 0.1592 0.2439 0.5002 0.5003 0.5003 0.8462 0.8663 0.8663 0.8663 0.8663
	EPS1-2 KAD1AN (6.261A 0-1726 0-0926 0-0517 0-0164 -0-0164 -0-1847 -0-1847	#FFFF # 111- # 111-	CSI - 455 -
M OM	EPSI-1 6.504N 6.504N 6.504N 6.1560 6.1151 6.0155 6.0155 6.0156 6.1562 6.1562 6.1562 6.1562	P027 P01 11.2316 11.2326 11.2224 11.2226 11.2425 11.2435 11.2435 11.2231 11.2231 11.2231 11.2231 11.2231	2.25 - 2.55 - 2.
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		000 CA-B 101AL 0.0340 0.0350 0.0550 0.0570 0.0570 0.0705 0.0705 0.0705 0.0705	
1 SPEED CODE	KG/HC/SEC 151.66 155.60 158.27 158.27 158.64 154.86 157.70 157.70 155.46 155.46 157.10	6 A C C C C C C C C C C C C C C C C C C	КНЦ V М-1 1.05 31.05 31.05 31.05 32.55 32.56 32.56 32.56 32.56 32.96 31.72 30.73 30.73 30.73 1.070
RUN NO	V62 M/StC -14.6 -14.6 -13.2 -117.5 -117.5 -117.5 -141.3 -156.1 -167.4 -221.9 -221.9	108 N DECREE 58.46 30.67 22.78 20.67 10.36 10.66 10.66 10.66 10.66 10.66 10.66 10.66 10.66 10.66	700 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -
ર્સ	VBC-1 M/SE-1 1131.3 1131.3 1144.0 1164.0 1164.0 1266.3 127	DE DE CENTRE DE	17 SE C C C C C C C C C C C C C C C C C C
	V2 M/SEC 150.7 150.7 163.2 110.0 183.2 183.2 183.3 245.0 245.0 265.1 275.3	DE D	F1/5 FC F F F F F F F F F F F F F F F F F F
	V1 H/SEC 181.5 231.6 231.6 246.8 246.8 265.2 310.3 327.9 342.2 342.2	0.22 0.02 0.03 0.03 0.03 0.03 0.03 0.03	F1/SEC 605-3 605-3 605-3 723-0 723-0 723-0 723-0 873-0 945-0 1007
	U-2 M/SEC 148.5 101.4 107.7 107.7 107.7 200.8 247.1 297.1 297.1 297.1 297.1	M2 0.4432 0.44716 0.44776 0.5681 0.5681 0.6184 0.7107 0.7107 0.7123	0.12
	141.3 141.3	0.5547 0.5547 0.65688 0.67688 0.7458 0.7458 0.7458 0.7458 0.7458 0.7458 0.7458 0.7458 0.7458 0.7458	FI/SEC F 430.9 490.9 555.7 6011.0 734.4 671.0 734.4 6814.6 8814.6 8814.6 881.5 914.4 999.8 11039.5 11039.5 11039.5 11039.5 12040.3 120400.3 12040.3 12040.3 12040.3 12040.3 12040.3 12040.3 12040.3 12
	748 778 778 778 778 778 778 778 778 778	######################################	1.2264 1.2264 1.2264 1.2264 1.2264 1.2264 1.2264 1.2264 1.2264 1.2264 1.2264 1.2264 1.2264 1.2264
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TABLE A-8

AIRFOIL AFRODYNAMIC SUMMARY PRINT

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	POZPO INCET 1.2503	1.7468	1.259	1.295	1.293	1.290	1.792	~	1.264	TOT!	97	6	96	, 2,	63	88	0 4	3 8	8	75	7	PCT TE	5 K C C	•	۲.	ı,	0.401	•	• -	. ~	0-842	8	0 (•		
	PSI-2 ADIAN -2511	0722	7110	92,000	0880	1042	1441	1620	.1975	EFF-A Trial	97.09	97.50	96-30	95.09	93.70		0 V	87.52	_	•	0	51-2		000	-139	976.	.668	189	420	9	23	.92	•	•31		_
	m E O		0	9 9	9	9			9	2 /2	502	453	9 9	965	703	958	100	851	829	111	049	EP	א נו		4	3 1	0	۲' •		. T	۰, ۰	2 -8	72 e	<u>ا</u> ا	EFF-P ROTOR	87.88
2	EPSI-1 RADIAN 0.3022	22.00	0.065	90	820.0	80.0		. ~	~	28	1-2	1.2	7		7.	2.	7	7.7	~	1.2	7.	EPSI-	# 5	7 K	×	8	2	81	2:	4 74	′ κ	3.91	-10-42	3		4.5
INT NO								9	9	0.55-P	0063	00.63	97.00.	0088	.0101	0204	0193	020	0213	.0770	0020	~	ָ ער											1	FFF-AD ROTOR	£7.
TO POINT	RHOV4-2 (6/M2 SE(00-69	65.68	70.5	1689	ب	64.3	•	44.9	~	_	_	o (• 6		<u>ن</u> د ده	-	9 10	0	٠ -	٠,	RHOV	17512	33.38	33.0	33.0	33.9	m (40	34.0	33.6	33.2	31.07		P02/P01	2723
CODE 7	د ن				_			_	-	OMEGA-	0.03	0.026	0.0340		0.047	0.094	ç	0.108	17	.15	-17		نڌ				٠.									5 1.2
SPEED C	RHOVM-1 (6/M2 SE 138.63	142.51	5.44	ر ا ا ا ا	3.84	2.85		35.61	3+84	FAC	275	423	505	201	053	202	910	5861	553	1617	209	RHOVM-1	~ .	200	9.6	1.0	۲.	တ္၊	` `	20.26		9.3	27.81	Ļ.	T02/T01	1.0915
S S	¥									٥	4.0	4.0	0	. 4	0	••	0		0	0	0.3					~									¥ .	
ON	VB1-2 H/SEC -16.4	-42.6 -68.0	-100.2	-130.5	-171-2	-180.5	-203-4	219.5	227.9	TURN	40.45	32-29	25.73	17.09	15.03	14.03	12.02	95.9	9.15	7.56	6.47	7-101	TZSEC	130.0	-223-2	276.4	-355.1	4 29 • 3	7.4	501.0	667	-685.0	-720-2	747.		
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	\$ 2 7	.4 -149.		m a		0	-29		5 -3	90	' –	_		-		_	۰.		. ~			>	ш.		7	109- 5	19- 6	£ -73	6 -e1		- 1	-10	0-10	1-10		
	V1-2 M/SEC 132-1	143	. 73	63.	. 7	7	39	, 8 7	253.	TACH	် ဗေ					•	•	9 6			•	V - 2	FT /SE	423.5	471	407	550.	109	6.39	735	783.	796.	815.	60		
		111.6	41.1	59-2	69.5	05.5	73.4	30.2	45.1	NCS	, r	3.61	4.13	10-4	2.00	5.63	5.95	20-9	40.07	6.15	6.19	۷۰-1	/SEC	585.7	94.2	12.0	0116	9.05	16.0	4 60	7.70	15.6	109.6	•		
	> 7 ~ .					(-)	ر در د	. 6	σ.	-2 I	, V		76	65.0	305	13	63	35.7	9	160	4		•	5 6 6					5 5 6	-	9 4	ָריי פיייייייייייייייייייייייייייייייייי	.5.	-	<u>u</u> 2	7.83
		177.8					3, 8	ริ ลิ		¥	10	0.39	3.	\$ 4	. 5	0.5	9.0	0 C			~	_	=	4 4		? ?	69	7	= :	- 6	0 40	. 6	_	103	E F	46 9
	11-1 4/55C 131.4	69.5	204.6	2,52.5	270.6	618.9	1.000	317.0	325.0	H 1	v.	573	-6305	0 0	777	. 9321	. 8992	0.0101	9766	0058	0.250	1-n	TISEC	431.7	556.0	601.5	671.4	739.9	1, 11,	O. 44 4	7 6 30	000	1040.1	9.990	EFF-AD INLET	87.4
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	4/5E	12.7		7 7		7	7.5	5.7	. 22	1 c	~		•				•	A. 4.	•			1 2 >	Υ.	306		``	3	្ន	80	\sim	7 6	9 9	٠٠	Č.	WC1/A1	135.
Sneed	V-7	75.0	, 5 , 5 , 5 , 5 , 5	0 C 7	60.5	55.3	43.7	, , ,	42.7		- - J	٠,	ċ	o r	٠.		ç	-C 4	, , 4		· e)	۷- ۲	75.	10.6	• - 0	0	6)	77.	Ş	5.	• •		-	69	1/A1 4/5°C	.76
	ب و ن	٠.٠. د د د	- "	 • •	. •.	0:	٠.	~ ~	- •	, , ,	1. 	0	c.	د. د	9 0	· ·	۲.	٠, د	÷ c	` C	· •	_	נו פּד	٠,٠	, a			• 4.		۰۰۰	٠ •	c r	. 4	٠.	7.5°	\$C
20 Pe		125	٠,	,		2	F (<u></u>	or i	7	. r	د	C (i c		C	c c	: c	. с	. (-	Ţ	F1/5	¥ 0 0	7	7 7		61º	٠.	(13	? c	. 0	356	300		
		r .			_		-		_	-1	_	٠,	•														_	. ^	•	_	•	٠. ـ		-		

TABLE A-9
AIRFOIL ACRUDYNAMIC SUMMARY PRIMI

											RUN	RUN NO 4	SPEED CODE	JE 7L POINT	1 NO 3		,	
	70 Perce	ent Speed	_						•	,	9	2-450	1-MAIJH0	V-MV.HR	. FPS1-1		-2 PU/P	3
7	K-7	V-2	I	VM-2	-97	~	N-1				1	71.00	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	CHY VAV.	KAU		AN IRLLI	-
,	~	H/SEC	-4	M/stC	?	Šŧ	M/SEC				17.5EC	7/2/5/5/5/5/5/5/5/5/5/5/5/5/5/5/5/5/5/5/	124-44 124-44	345.36			-	21:25
-	107.1	178.5	.;	115.3	ب	9	131.6			1 1011	151.0	4 4 4	128.39	144.80			~	4.47.
7	110.5	104.0	ċ	113.4	o ·	125.3	0.041	e - 1 - 1	7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		3 4 5 4 1	-00-7	136.34	143.28			-	.2061
M	112.4	161.4	;	110.8	· .	116.4	20.63	100	0 · 0 · 0		-163.7	76.0	130.76	143.23			~	.2653
4	117.8	128.5	5	770	, د	0-517	1.501	4 . K . C . C . C . C . C . C . C . C . C	7.44.1			F-16-	131.19	144.36			-	24720
Ŷ	11:20	157.9	÷.	115.6	٠ د	6	2000	F . C . C	252.8			-114.3	151-44	151.66			_	3
•	113.5	157.6	<u>.</u>	111	. د	0.01	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		273.3			-134.5	130.91	127.17			٠.	1.5234
7	113.0		; ;	118.5	، د	7-611	1.047		707		271.1 -	154.7	125.19	157.69				7
æ	111.3	163.7	: :	116.6	9	9-711	1.17	C 71.2	300.3		-274.3 -	-162.7	128.08	155.70	1.0-			750
٠	116.2		;	11/11	٠ ر	116.0	6.67	204.0	318.6			-182.6	124.28	143.23	7:5-		٠.	. 3 4
·)	16.0		3	0.801	.	* *	7 4 7 7	6,770	323.1	14.7		-187.1	123.18	139.39	1.1-			.
7	105-6	152.8	å,	100.	. ر	? ^	4 6 6 6	36.0	333.E	20.5		-197.1	120-40	129.35	: د	: د	: .	V-1-0
<u> </u>	163.0	1 - 4 - 1	0.50	1.54	ور د د د	112.0	325.6	_	341-0	0.0		+-507-	115.60	1.5.59	*041-1-	•	T-11 0177	ì
7	7. 10.		•						;		2	10.00	HC 543 1	OMS GA-R LG	1085-P		34	4-113
5	F1	1	-	74	¥-	F-2	TI	H2	ر در در د			4 8 3 1 6			TUTAL PUL			101AL
;	DEGREE	IFGRIE	4	ULGREE			•		יני ניי ניי			77 77	1 4887	•	٦.	7	76.55 7	99.0
-		•	?	1.51	၁	0.5265		C. 3386	200	27-71		20 45			-4			50.17
~	0.0	~		1.13	3	C. ~914	5533	0.3464	3 c	* D • T *	12 20	23.67		1000	7			71
٦	0.0	•	3	1.53	•	0.4080		2995.0	2 .	11-17	13.66	24.00	,	47.79	_			43.60
*	0	~	•	4.45	•	6864.0	1079-0	0.88.0		77.11	94.0	20.16		1690.	4			47.63
•	0°0	•	:	76.7	•	6.44.59		0.4333	,		0 0	17.70			_	× 7767.	``	41.55
د.	2.3		3	77.0	3	1.4537	6.7512	991.	0 1	07-11		60.4	~		7		43	1
_	٠. ن	4.3.7		1.04	;	0.4.0		011010	7.0	11.40) F	15.12			-			20.00
· or	0.1	~~		15.7	3	0. 2676	4.4.5	70000	0 f	11455	7	14.19	516	1. 1535 G.	~			4.45
•	9- 0	43.8	84.89	24.30	0.3274	0023	9168	4174.0	60.0	11.67	4	11.68		0	7		74.38	15.51
01	o. J	٠,١	4.0	7.34	•	•		0.00.0		76.75		10.33		1.21th C.	~			13.61
1	0.7	•	3.0	65.0	•	_		0.00.0	70.0		44.4	8 1 1 1		به	_			69.61
15	0.0	æ	٠.	03.42	•	•		270.0	0 4		4	7.13) 47 64.3	534 0	-		2.91	61.10
13	0.0	v	7:7	26.43	•	_	1. CIO	U. 6344	2		١.	•						
			:	:	3	. !	1	\ <u>-</u> 1	1-•7	××	1-,91	7-,41	KHUVM-1	KnUVR-Z	EV 21		7	וני הנו היי
ž	- 1	>	1-57		1100	7-04	1.0	٠	SE C	SEC		F1/5+C	LEM/F125tl	. LBM/F125	י כא	، د		77.47
	£1/S	?	7	-		•	731 0				-431.9	-41.7	25.57	ď		◄		0167.0
-	351	ري م	351.		٠.	•	1077	530.0	6111-3			-119.9	56.29	29.67	-			76.7.0
~	36.	554	366		ء د	•	55.4	5,144	£68.C			-189.1	60.02	47. °	٠.	₽ :		
~	3.5	575	366.			٠.	4004	523.2	76.7.6			-2.6.2-	26.13	29.13		٠.		0000
.*	37.	7 .	9 6		.	7	672.5	683.7	768.2			-354.5	26.45			-	7 -	1
^	3	976	37.		5 0		7.1.1	745.5	829.4	543.2		-361.6	26.92	20.00	776			
n •	7		376		d	. ~	816.5	812.8	696.7			-441.2	26.81	25.19			, ,	2000
•		,	4		ð	3.70	889.5	1.118	961.6			-507.5	24.07	05.26				7.00
79 7	30	200	4 4 4		Ö		916.5		965.5			8.664-	50.43	64.00				27.7
•	700		,		Š	æ	1.065		1045.4	646.2	٠,	7.66-	25.45	44 87	45.1.35		_	1,000
2 -	7	3	, M		0	363	1005.0	٥.٢	1006.2	704-4-1002	.	V . 61.5-	62067	20.02	,			< 1.56.
: :	, (A	84	337		o	368.4	1041.9	15.2	1095.3	٠,	•	20,00	٠,	25.7	-11.2	50 -11.	815	0.9635
7	332.	463.3	332.	313.8	Š	367	1068.3		1116.7	743.5-	5-1004-3	1.4.0	4 7 7		!			
1	•				•	000	0 4 11 9 7	3144	Ą			,	102/101	PC2/PC1	EFF-AU	FFF-P		
		(1/4)	MC I/A	 .	2 ())	14 17 1	د							KC1CK	KI CY		
		LBM/SEC	3/2E	ر	<u>د</u> د	1 (4 1 .	1			:	,) : جر :	: ئ	`	
		7. F.	22.5		6690-1	1.3004	83.62	83	*				1.6939	1-3004	83.02	#3.04		
		74.84	1:1	•	1000	•)))	,										

ORIGINAL PUBLIS OF POOR QUALITY

TABLE A-10

AINFUIL AEXUUYNAMIC SUMMAKY FRINT

RUN NC 3 SPEED CODE 13 PUTNI NG 1	CANALL MAILS KHUVM-1 KHUVM-1 EPSI-1 EPSI-2	CH-1 VH-2 VO-1 VO-2 U-1 U-2 VI-1 VI-2 MACH KIC/MS SEC KIC/MS SEC KADIAN KADIAN	HAVE HAVE HAVE ANDER MANEL MAN	185.1 155.4 6.0 158.2 157.5 155.5 175.4 156.5 158.10 186.24 0.2278 0.1750	140.E 191 0.0 122.2 150.4 168.8 ZIU.5 150.4 172.1 -75.5 160 184.22 0.1600	141.0 1.0.0 110.4 1/7.1 185.8 228.1 10.0.0 1	12.7 1.2.1 0.0 104.0 191.0 195.1 240.1 1/3:1 1.31.0 1.51.1 157.78 185.96 6.0644 0.02.27	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	145.4 110.1 0.0 92.6 235.6 237.1 277.1 205.1 -235.5 -144.5 102.0 16.56 -0.0292 -0.0464 1	145.6 145.0 146.04 254.6 256.4 277.5 216.4 1554.6 159.4 166.6 1	10701 11701	143.6 141.9 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	142.1 140.5 0.0 0.0 0.1 0.1 0.05.7 0.05.7 0.00.7 0.0	136.9 http://out.org/18.5 410.5 347.0 210.6 -318.5 -231.7 155.19 101.20	00.5 157.7 159.5 10.0 10.0 5.1.2 5.2.7 357.5 270.4 -331.2 -244.1 152.2 -0.1966 -0.1994 1	1.6 1.5 1.2 6.0 17.0 334.0 331.1 304.3 280.1 -334.0 -252.1 1.0	THE DEAL DESCRIPTION OF FAC ONEGA-6 LOSS-P POZZ ZETT-A	M-1 M-2 M-1 M-2 JND	UNDER DEUNEE DEUNEE	41.7 43.43 6.48 0.4060 0.6060 0.3040 0.3040 0.28 13.41 31.13 0.3046 0.0465 0.010 1.446 94.95	48-13 17-01 6-4210 0-5700 0-6254 0-10-4 0-18 11-61 24-04 0-3565 0-04-7 0-0504 1-2564 94-14	50.46 20.42 0.4303 0.5303 0.6012 0.501 2.13 0.22 10.42 20.59 0.3350 0.0416 0.5019 94.14	54.45 54.45 u.4550 u.4550 u.4560 u.5518 2.55 0.15 1.98 lu.52 U.5150 U.5150 u.454 u.52643 92-b8	55.77 39.20 64351 64314 643245 64355 2480 643 6441 13441 64303 6431 64310 142887 85-53	58.54 44.41 0.45.01 0.00.00 0.00.00 0.6253 3.55 6.54 3.70 15.10 0.53.70 0.00.57 0.0135 1.2649 89.20	60.77 4/15/ 0.4370 0.2370 0.244) 0.6588 3.93 6.68 3.86 10.14 0.311 0.0131 0.0138 1.2864 68.37	65.05 52.41 0.4574 0.4574 0.4170 0.1174 4.04 6.66 3.78 9.76 0.460 0.0823 0.0157 1.2750 84-70	2 03.40 03.10 0.00 0.00 0.00 0.00 0.00 0.00 0.	3.5 00-01 21 17 0-413 0-4025 1-0307 0-1796 4-27 0-40 4-13 1-1 0-3012 0-1347 0-0235 1-2464 74-13	3 52 73 74 1479 6-4016 6-4052 1-0672 0-7935 4-44 6-54 4-57 2-31 1-1066	11. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	CAS DOLLD CALLY KHOWN-1 KHOWN-2 EPSI-E EPSI-Z	UN-1 VN-2 V6-1 V6-2 U-1 U-2 VI-1 VI-2 VI-1 VI-2 V6-1 V8-1 VN-1 V8-2 V6-1 V6-2 U6-1 V6-	177-C F175EL F175EL F175EL F175EL F175EC F17	077.5 440.7 503.2 0.0 453.4 450.5 504.4 513.8 513.8 1545.9 32.38 35.14 1340.3 10.00.0	461.7 470.0 0.6 400.8 31.0 4 346.0 544.0 -580.9 -247.6 32.94 31.13 4.125 7.224	471.6 48**4 C.U 361.7 18.4 18.4 18.4 18.4 18.5 18.6 18.8 18.6 18.8 18.8 18.8 18.8 18.8	414.1 480.1 0.0 110.0 110.5 110.1 848.0 0.22.1 -101.5 -344.1 03.23 3.6.10 0.933 -0.442	411. 421. 1.2. 1.2. 1.2. 1.3. 1.3. 1.3. 1.3. 1	410-4 410-4 6-4 6-4 6-4 6-4 6-4 6-4 6-4 6-4 6-4 6	10.0 281.9 427.8 915.4 10.0.8 793.2 792.8 7.2.1.0 36.14 5.564 5.564 5.564	10.25 1.55 1.50 1.50 1.50 1.50 1.50 1.50 1.5	50.5 400.2 4.14. 10.7 51.4 10.7 1.5 1002.0 1124.0 615.0-1027.5 170.7 31.38 36.91 -9.200 -0.945	21.01- 05.62 HILLS 1.014-1.1134-0-887-7-001-1-4-01-1-33-9-0-1-4-0-1-2-3-3-9-9-1-4-1-1-1-3-3-9-9-1-1-4-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	0 431.1 424.2 0.0 258.0 1080.7 1058.9 1172.9 900.8-1080.7 -800.7 31.77 -11.265 -11.424	2. 4.4 4.0 259.4 1114.2 1080.4 1195.8 918.9.1114.2 04.0	107/101 P02/P01 EFF-AD	ALIVAL 10/10 PU/PU ETT-P	KONSEL INLET INLET INCE	1,0404 1,2647 87-60 uc.u.	_
		-	,	-							47.4	43.0		30.0	37.1	7.50			ш	*	7	4	ر د د	5.13	*7.0	-	63.05	つ ₁	0 4	27.00	2 2 2 4	2	- H	1/251	440.7		4.11.6	414.1	0 - 1	1.0.7	· ·	7 .	7.007	0.004	1.15		,	461/A1	XC/SEC	KOS.	151.06
	Transfer Speed	To retreat 67	7 7 7	3 2 2 3 3 5 W	4.001	7 44 9 7 7	5 - 20 T 9 - 5 - 7	7	D-074 - 4-677	145.6 112.0	1-5-3 1/5-7 1	143.4 1/1.9 1	142.7 109.6	436-y 102-U 1	1 4.001 1.161	1 0.161 6.961 51		7-12	ת ברוקא הרות	1.14 0.0	7-85 0.0	3.36.0.0	4.46 0.0	0.0 33.5	0.0 32.5	4.26	20.1	2-05 0-0	6.62 0.0	0.0	3 - 1 C	35	1	1-A	440.7 077.3	20124 038.3	71.8 004.0	474.7 590.1	4.17.6 577.4	4.18.4	170.0	1111	108.2	455.6	21.7	2 - 2 - 2 - 3 - 3 - 3 - 3 - 3 - 3 - 3 -	434.0	14/137		1444	30.95

TABLE A-11

AIRFOIL AERODYNAMIC SUMMARY PRINT

RUN ND 3 SPEED CODE 73 POINT NO 2

0000		INCE	1.2786	Z	.282	.287	1.3052	۳.	1.3554	•	•	٦,		. "	•	•	*										78.98		7.		44	,	PCT TE	SPAN	0.0916	0.1592	0.2439	0.3055	0.4015	2005-0	0.6063	0.7093	0.7468	0.8422	0.0669	0.9275	0.9693							
		3 3	0.2507	0-1599						-0-1017			-0-1690	1801	5000		XEFF-A	TOTAL		94.25					83	2	3 78.02	7	Ş	65	1	•	EPS1-2	DEGREE	14.366	9.053		410	126		-3.204	.824	.833	179	5	2	1.489		EFF-P	ROTOR	\ W	.47		
	1-15-1	KADIAN	0.3091				0.0653	0.0144	0.0381 -	0.0944	0-1163	-0.1671	-0.1170		100	1001			_	1.2779	_	_		_		_	1.3723	_	-		•	1	EPSI-1	DEGREE	17.709	13.118	9.325	7.050	3.743	0.823	-2.185	-5.411	-6-663	513	-10.14		-11-462	,		2		0.70		
:	KHUV F-2		.78	.58						58.60						•	LOSS-P	TOTAL									0.0376				•	•	RHOVM-2	FTZSEC	29.86	9-82	29.60									E .	2	:	/PO1 EFF			•		
		لا	_								_		-			71	OMEGA-B	TOTAL	0.0776	0.0764	0.0854	0.0948	0.0947	0.1130	6.145.0	272	77810	2222	0.6230	6720		1797.0	-1 RH	<u>۔</u> پ))														01 P02/P			7186.1 78		
:	I-WADHA	KG/HZ S	125.99	129.24	130.89	131.21	131.56	131.77	130.96	128.88	127 63	C 9 C C L	20-071	277		11.	D FAC		0.5235	0.5431	0.5461	0.5418	1115.0	1105.0	7	1000	1000	016	6064.0	51440	70440	O.48 85	RHOVE	1 RW/E 12	č	26.4	26.81	26.8	26.9	26.9	26.8	26.4	26.14	25.3(7.4	34.40	7		T02/7	:		1.1057		
	7-,00	MISEC	-10.5	-34.				- 119.0	- 1	. 1	Ī	7	ī	ı	ī	-202-	1.00 K	Ç	•								00.01					30	V				- 36			300	•	200	8	5	74.0		1							
	>	E/S	-136		175.0	. 190	-212	1.45-		7000						-337.4	. <u>.</u>	DECREE	12.97	13.27	12.80	12-12			7		0.00		2 · 0 · 0	07-0	ċ	99.9					-577-1					7	679	- 0000	0.0201-10200	- 04 VI - 6	1017							
	~	X.	_		•	_	•		•	•		661	209	212	218.	22	E 2	` 2	5				• •		-							•	· · · ·		11/25		414																	
		C M.'SEC						4000		0.162								2	5	- F	•	•	•	9		-		•	•	.	_	•	2	٠	•		C-170 7					2 453.0	•		10073			_	9	NET		1-47		
	n-2			••	•					1.007 4							7		•		•	• •				Ö	0	ŏ	0	ò	o ~	ö			_		3000				٠ ڊ	٠,	- 1	- (•	1012	. 7 1052-0	•	u	.	•	0.70		
	1-0) X	7							.1 257.9							1		•	n 1) (ю (o ·	0 0	70 0.8971	8	0 ~	-	9	_			<u>ب</u>	۸.	1. 507.7		•	,		9	176		•• 1020	1038	1079	.2 1107		FO CFFFFE				
	>	K,		2 :	× .	٠.	121 0	1	2	0 122	0 133	123	ฎ	0 123	太1 0	0 133	1	Ě		50 · 0	7 · · ·	£ 0 95	26 0.47	15 0-41	95 0 28	58 0.48	94 0 16	61 0.48	\$ 0.7	24.0 60	31 0.4	79 0.43	;	>	EC FT	•		• •	٠ د	9 1	9	•	•	4	•	4	• • • • • • • • • • • • • • • • • • •	•	•	3 2	•	-	•	
	>	× /×	•	> •	o	Э (9	۰ ۵	0	0	0	0				95.1 0	1	£	•	25.0	0	0.33	0.33	0.33	0.33	60.33	26.0 1	0.32	0.31	10.3	7 0.3	0.2	:	•	.c F1/	-	9	•	•	m 1	Ŋ.	-	٠,	m,	cų.	-	¢.	•	•	101	Ľ	1,047	•	
	>	3	· ·	7	-	-	£ .	9	- -	3.0 118	= •	~	•	9	~	8.			E CEG	٠ د	~ :	7	400	40	9 4 9	9	7 52	6 54	9 59	9 60	8 63	6.3		÷ K	SEC FT/S	5.1 378	5.4 372	0.6	1.6 364	2.7 37	3.4 376	0.9 38	4.2 386	0.3 38	7.4 34	3.9 331	5.4 310	9.8 31	;	1/41	1 7 1 1	Ţ.	, (, 1,	
peed	>	. 1		2.4		1.1	4.2 11	3.8	3.6 11	3.2 11	1.2 11	9.9 10	2.3 10	0.7 10	7.6 10	9.1 10		60 (990	. 51	9.2 54	57	7.5 59	5.7 61	5.4 64	5.9 66	6.3 69	69 9-9	9.2 71	17 0.0	2.1 72	2.3 73		2 YH	EC FT/	.4 35	96	2.	.7 37	.5		.5 37	.8 36	96 9.	* 34	.3 34	.9 33	.1 32		3 ,	•	:	4	
Percent S ₁	>		<u> </u>	.2	- 1	ş Ş	3 16	,6 16	. 16	.0	. 0	91 8	91 6.	16	2 15	00.5 15		-	REE DEG	o.	•	•	٠ د	•	•	•	•	•	•	٥.	\$	0.0		>	EC FT/	09 1	365.4 573	٠ ۲	3	.7 53	.4	.9 55	.2	.3 55	.4 53	.9 52	.4 51	16 8.	,	WC1/A1	100	57	*7	
13	>	ì	È	2	=	=	=	Ξ	~	=	7	10	2			2		€0	3																7	m	ň	~	~	~	~	m	ň	ñ	ň	À	•	M						

TABLE A-12

AIRFUIL AERODYNAMIC SUMMARY PRINT

•		_			•	-	-	•	_	-	•	•	7	9		•		4	74.	.81	34	43	53	19.	19.	55.	11.11 85.	3	.91	-2 PCT 16	SPA	30 0.0916	337 0.1592	02 0.2:39	70 0.3055					9 (7	20 0 0345	65 0.9693				
60						10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	,		-0-	-			-0-1	7.7-	POS YEEF.			2508 96	6	6	3	9	8	8	52	7.5	.3222 70	3213 65	ક જ		LEE DEGREE		<i>.</i>	÷	~	-	٠ ا	ri I	ŕ.	, e		, , , , , , , , , , , , , , , , , , ,	25 -11.6		EFF	80108	95.56
0	~	SEC	2 0.3040		٠.	٠.	. ~		٠		4241-0- E	. ~		•	d-220	TOTAL	0081	7600	.0132	.0166	. 7210.	1 1610.	6970	.0314 1	.6334	.0392 1	.0409	1 8740	. 4240				2 12.712	~			۰,	•	165.6-	→ 6	٠.	1011 W	2 -11.4	,	EFF-AD	2	82.00
ODE 73 POINT		¥	138.4		2 4 5 5	7 1 71	143.4	149.8	150.6	7.4.4	6	129.6	119.0	116.3	OMEGA-B	זער	Ç	0.0435 0	0	0	0	0	0	0.1539 0	0	9	-2337 0	\$-2750 O	. 2883		C LBM/FT2 SEC		28.1	27.7	27.6	29.0	64.5	0.05	900	30°4		3	23.8		P02/P01		1.2978
S SPEED CODE	KHU VM-1	KG/H2 SE	118.32	121.02	125.50	4 4 4 4	124.08	124-46	121.60	120-43	116.45	115.33	112.60	110.79	D FAC 0	•		.5393	.5434	.5373	.5031	.4917	6164.	.4835	**825	+284.	714	2030	9.4.4.F	RHUVA-1	LBH/F12SE	24.23	24.91	25.25	25.31	25-30	14.62	62.63	74.40	24.00	23.65	23.05	22.69		102/101		1.0%4
KUN NO	1 V62	: د			(-71- (9 -115-6	· 1		Ĩ		-177	-185	7	TURN	DEGR	'	m	_									8. % (S)	ລ້	70A	FT/S	-42	-117	-195		-310	4.70					-608	-632.7				
	90	2	-129.		-181	-707-	-227	-245	.207.	-275.	296.	301.	-313.	-3210	+ DEV	DECKE	7	-	1.4.1	13.4	10.5	8.5	2.5	7.5	4.0	6-1	6.43	9	0	0 \	F1/5	126.		7.7.	-56-	-003	177	ָ ֓֞֝֞֜֝֞֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֓֡֓֓֡֓֓֡֓֡֓֓֓֡֓֡֓֡֓֡֓֡֓		-972	9 70	-1028.	-105				
		M/SEC M/SEC	6.5 109.9 80 a 113.4	•	•		7.0 158.5	*	0	٧	*	2	937 9	-	CS INCM	EE OF	0	8.22 13.10	- 99	- 53	- 3	· •	7 9 7	~ ·	7 59	70	.66 11.79	7		_	4		3.5 369.9						7-024		4	9	.2 6%				
	~ ;	، د	-	- •	. ~	۰ ~	224.3 24				289.1 312.	3.8	5.3	7	N2 IN		*3207	.3217	97.							2708	574	6186	2000				523.8 593.5								٠-	-	027.6 1098		EFF-P	- X - X	87.66
	1-0		1.69.9	167.5	181-2	202.2	222.9	245.5	267.5	275.0	296.2	301	313.3	321.2			0.4877 0	0.5366 0	0.5875	6.6228	0.6777	U- 7328	C. 233	6.8513	0.0725	4524		0.9702 0		7	_		465.5			!		177.0			4	9			EFF-AD	- X	82.00
	3	: <u>د</u>	133.0	: =	1	7	2	11	7	7	7	=	11		M-2		0.5	0	•		0	٠	5	٠ د	, ,	* · · ·	0.430	5 6	5	9	F1/5	434		7 P F	110	35.5	7			377	381	0 392.7	35		PO/PC		1.2978
	A 2	È									0.0				~	ie.	*				2			35-3 3-3 3-3		47.0 c	2 2	22.0	9.7.0	1-91	C F1/SE	•	.	• •	• •	• •				; ;	ی د	` .	· 0		10/10 14 24		1.0944
	-WA 1- /A		2-401 0-10	104	15.9 10.	101 2.00	16.4 Lug	15.8 112	. 11 11.0	2.5 111	101 7.61	18.2 98	15.6 90	3.5.	2	DEC	٥	9	7	9	;	3	ĵ.	2	, ,	ζ.	11.73 01.	3 4	ò	>	÷	٠ بر	m à	1	<u>, </u>	, ,		~			٤	113.8 296.	₹,		C1/A1	203	114.34
Percent Speed							155.5 10					0	_	,		ONE E	^		۲.		•	.	٠.,	, i	20 1) 0		Ξ	., ,	·	•		, ~			. ~	۰,	4.6		7		MCL/AL MC		•
73 Perce	1-1			105.1	105.9	100.2	166.4	105.8	104-1	102.4	94.5	7-25	42.6	, 4	6-1	DEGKEE DE	၁ ၁))) ())	ء د د	0.0)) ;) :) :) ;	3 6) (?	~	, r.	۲۰.	•		, ,] [7.7	*	20.		7.7	313.8	2.5	•	7 1	35	23
	3	-	4 ~	~	*	•	٥	~	20	•	0	=	77	?	オ		-	. 🗸	.	•	Λ.	0 6	• ;	• 0	>	3 :	1 ?	7 -	:	7	•	٠ ٠	٠.	٠ ،	, 4	ه ۱	~	20	•			77					

TABLE A-13
AIRFOIL AERODYNAHIC SUMMARY PRINT

	04/04	INLET	2831	2869	2924	3006.	.3270	.3603	.3758	.3706	.3671	365	.3631	~	g-3534	101	; ~	11 75	270	92.39	91. RB	40.04	84.97	00	70.28	73.05	3.17	67.81	66.41		PCY TE	SPAN	0.0916	7651.0	245	70000	2005	6063	7007	76AB	6477	866	.927	0.9693					
		NY :	1 9157-0	• -	2.	99	.0141	1 7550	1015 1	1190 1	1601	7	189	20	Ų	TOTAL	07.10	05.97	0.40	92.10	01.56	50	84.20	200	78 33	71.84	•	•	0.		EPS1-2			4.140	4.534	114-7			710	70.4	173	682	0.846	00571		4	e	7	, •
4	<u> </u>	N I	۰ م د ک		9	245	139 6	374 -0	24	140 A	634	732 -0	916	٩ 3	,	28	2 8 6 3	7697	0986	7007	7002	333	26.04.	2000	27.5	00,50	4400	9	1.3632)	EPSI-1 E		254	0	9 9	2 5	0 4	0 6	2 9	2 5	2,45	3 5	: 5	7	•		ROTOR	8	5
ON L		C RAD						٠	•	•		Ŷ	9	9		1	000			286			170	7,70	0340	0.0364		0140	9840		~	ũ	17.	_		•							1	1		FFF-AC	ROTOR	81,30	•
75 POINT		KG/M2 SEC	151.11	14.4.51	146.11	152.15	153.27	158.34	157-89	155.40	140.46	136.58	٠,	8.4		2, 8	- 6		- 0	9 6	9 6	2	1 1	5 1 2	404	9 9	2 0	, ,	200		Ϋ́	BM/F12	30.95	30.62	30.17	29 93	31.15		75		100	207	2 4 0		ů	P02/P01		9766-1	•
SPEED CODE	H-1	ر	77.	- :	ט מ		9			: 2	. K	٠.٣	00	0	1	à'	ICIAL POLICE	- ·	- C		- 6	• • • • • • • • • • • • • • • • • • •	 	0		9.	· ·	• •	n c		H-1	2 SEC L	69	41	.81	-92	.03	= 1	66.	ó,	99	ن د د	35.		D .	102/101 P		1043	
4 SPEE	RHOV	KG/H2	125	128.	121				2	1.0	766	123	120	119.		D FAC		2 (•	0 (0 (0000	0	00.0	0	64.0	5 6	7.4.0	0.478	•	RHO	LBM/F	52	, 56	56	55	~ :	2	92	\$ 7	92	25	; ;	5 ?	*2	102		•	;
0	VB*-2	M/SEC	-13.3	-37.2	10/0-	2017	7101-	121.7	156.0	2 671		107.7	-198.7	-207.0		108 N	DEGREE	42.69	37-15	78.83	24.64	9	17.56	17.17	15.3	14.42	11-02	52.01	20 1		V8*-2	•		-122-1	-204.6	-255.4	-332-1	-398.4	9.844-	-512.0			-615-1						
A NO	V6 - 1	H/SFC	-137.5	1 -156.6	-171-	9.17.6		, 0				ç	•	-340.0		DEV	EGRE	1.4.1	14.0	13.3	12.7	0.01	8.2	5.2	4.0	4	4.9	0	Ξ,	:	183	FT/SEC	-451.0	-513.9	-511.6	-629.3	-702.3	0.774-0	-852.7	-928.9	-957.1	92.0-1028-8	950	9901-	=		,		
	۲. · ·	M/SEC	-	25.	129.1	20.05	÷,	7.191	105		4.00		20.0			INC	DE GAEE	13.25	17.89	17.74	12.67	12-33	15.00	12.16	. 12.07	11.98	11.58	11.45	11.17	10.95	٠	FT / SEC	393.3	400.7	457.4	446.2	502.6	548.0	593.1	7	657.7	692.0	٥.	7 - 7 7	745.7				
		•	174.6	192.0	210.2	6.222	747.0	20202	783.	504.5	317.1	331.3	1.020	9.4		INCS	()	7.70	10.8	8.40	8.64	8.70	8.6e	9.13	9 .32	9.36	9.35	9.31	9.26	9.20	•	£1/5£ C	573.0	630.0	6.9.7	731.2	795.7	860.2	630.9	0.000	1023-9	1087.1	1107.7	1139.7	1164.4	٩	ET		-14
	5-1-	M/SEC	155.4	169.0	186.0	7.801	71 /.6	•	759.7	,	Ŷ	306.0	- 1	331.5		H2		0.3403	0.3547	0.3735	٠,	0.4412	4	٠,	s.	0.5698	Š	9	7.113.0	0.636P	11.2	E 7.	7	. %	9		714	778	878	910	94.1	5	~	1060.2	1087.7	4	T INCET	,	9 82.
	-	7.57	137.5	156.6	177.3	191.8	214.1	735.9	259.9	283-1	291.7	313.6	317.9	351.0	•	I-1		514	2.5	9.74	562	0.7207	20110	0.8431	0.9045	٥,	٠,	Ġ.	.03	•	- 1	1-0	7777	513.0	501.6	629.3	702.3	174.0	852.7	928.9	957.1	1028.8	1046.4	•	•	C C C - A	r.	1;	81.3
		7-4X	142.1	131.8	123.6	120.5	116-4	116.0	122.0	123.3	123.2	123.1	173.5	124.5		H-7						0.4711	9845.0	16450	0.4543	0.4796	0.4565	0.4.17	6 0.4416 1	0.436.9	9	7-01	7	٠,	٠.	345.4	8	5	~	•	~	0	~	6.604	4.)8.5	0	INLET		1.3369
	(30											0		- X		1915.	3,00	3357	.3372	.3389	3401	3383	3327	0.3293	.317	.314	306.	.301		, ,	<u> </u>			0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		INLET		1.1063
		1 4	? 0	9		_	5	5	13	_	.5	5	2	95.6	•	1	DICAFE	5.30	1.59	04.4	76	1.31	5.56	91.0	3000	0	01.0	1.33	. 13	5.51	1	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	200		1.0	7 6	377	377	36.7	395	179	344	-	313	307		- ()		
		1 L L L L L L L L L L L L L L L L L L L	(C		_	_	7	۲,	2	_	2	107.0	č	103.4	101	-	ن ان و ان ا	55.		٠,		_				69.22	_	_	ď.	'n.	•	> 1			,		7 1	1	, ,	¥	· •		34	33	333.5	•	KG/SE	So	122.(
	2	ر - ۲ د ر م		75.										157.3		•	ال والله والوا	7	•	` ~				v	٧.	0.44	, ,	•		L.4		>	ς:		٠.			٠.	٠.			Ÿ	526.0	_	511.5		FC 1 / A 1		25.00
	75 Percent	;	7246	· =	113.0	-	114.0	ž	-	_	110.9	Ċ	è	103.4	0	1					2 0			; ·		9 0	0	0.0	C	0.0		^ - 1	2	ζ.	ž	370.1 6.16.6		ľ	٦,	2	7	161	. 7	5	333.5				
		ş	•	۸ ۲	. r	1	٠	9	٢	Œ	•	10		21	2	į	ָ ער		٠,	. ~	٠ ٦	•	` •	0 F	•	E 0	٠.	<u>.</u> =	: :	: :		۲,		_	٠,	- 、	s v	` •	۰ ۱	- •	. 6		. =		12				

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TABLE A-14

AINFUIL AENUUYNAMIL SUMMAKY PHINT

TABLE A-15 AIRFOIL AERODYNAMIC SUMMANY PRINT

85 Perc	ent Speed					٠			:		2 9			Z		
-	>	1-HA	7	1-01	7-97	1-0 1-1	7-7	77	7-17	40.7 7.7 7.7	70A	KILAM2 SEC	KG/HZ SEC	KADIAN		
345	3		4/ St (∞	Str.	M/5EC	77.52.6	327 6		٠,	-20.5	177.22	. •			~
9.	431.6	4	١)	7,44	0.451	7 701	247 2		-181-1	-53.7	181.60	206.90	0.2386		_
4.5	219.	Ďă.	101.3	ء ئ	1-1-	10101	1100	7 6 7 6		-205-0	-46.2	184-17	207.41	9071.0	_	_
,	408.	Ξ.	9	3 .	1.8.4	9. 60.7	1.612	7.107		. 4	-106.6	185.61	207.91	0.1305		1.3546
2.0	403.		7	၁ ၁	1777	0.122					-1 10 ak	1 56.38	213.60	6.0731		-
7	.401	ż	105.5	0	114.0	241.5	451.6		٠,	٠.	-164-1	186.44	216-12	0.0223		1.3617
	Lyc.	Ė	•	o-0	7. A. B	217-8	214.5		1		-	186.15	215.21	-0.0261	0.0	_
-	. 707		•	0.0	117.5	300.5	•		•	٠,	2 4 4 7	184.481	221.69	-0.0753	0.0	_
	2 7	7	101.5	٥ . د	106.1	327.4	320	۰	213.6	77.1.2	4 666	07.69.0	220.05	-0-0955	-0.1	_
	7		ು	0.0	104.1	337.3	~	.	•	331.0	00 177	7000	212.43	-0.1475		_
7	00	Ġ	Þ	٠ د	78.1	305.6	355.9	•	•	307.0	3		208.99	-0.1660	1.5	_
	7 4 7	3	150.3	0.0	*.5*	366.8	357.6	M			1. 010		16 141	7	-0.18	_
3	12.		J	0.0	45.5	363.5	~	415-5	314.4	•	1-005	172.13	140.50	-0-1963	-0.19	_
2 1 2	107.8	157.3	130.8	J.J	93	343.2	363.4	423.5	25075		1.607			1		
	,					•	•		1	740	2	D FAC OME	GA-B	٩	1 XEFF	A REFF-
1-9	7-9	n 1	~	1-K	7-W	7 1	7K	1000	u - 4		3	•	141		7	101A
×	×	CKE	ULGREE					ָּבְּיבְּיבְּיבְּיבְּיבְּיבְּיבְּיבְיבְיבְיבְיבְיבְיבְיבְיבְיבְיבְיבְיבְי			37.15	0.4129 0	0.0768 0.0171	~	.3630 43.	.57 93.83
5	4	•	٩	0.4840			6964-0	***	200		3	4024	1514	•,		95.2
3	5	Ţ	17-62	4.5069			\$515°0	3		10.0	22. 51	45.84	15.38	~	2	94.3
3	36.	7	٥.	0.14.0	7909-0	2 5	79FC-0	5.	4.5	7.71	97	4.233	0 4150	30	ė	43.4
3	36	24.10	40.66	0.524.0	2165.0		0.5648		9	8.29	5.5	3983	0	~	.3642 53.87	87 94-13
5	34.	7	?	1626.0	0.5820	0.9136	****	1		4	12.47	.3824	0 1050	~		93.
3	.64	~	7	0.5210	1715-0		75.3.0	, ,	7.70	9	12.11	40.32	1120 0	_		85.5
;	45	٧٠,٨	0	0.5242	0.5775		?;	6. 10		•	30.01	. 35 76	0 2 5 9 0	~	8	1 68.1
5	32	62.3	7	0.51 15	Š	8 - 1 1 - 1	•	35.6	2	2	4.33		0 1100	~	9	2
3	36	63.2	53.89	0.5130	0.5614	1.1390	100.0	9.7	4		7.04	1626.	0 7501	1.0202 1.3	~	55 83.35
;	7	4.00	`.	31440	0.5376	1.1775	400	7	5. E.2	7	7.15	.3256	1138 0	_	5	Э 1 20 (
3	7.	4.00	r)	6764-0	9575-0	7-17-1	•	3	5. BO	5.12	5.19	3173	1551 0	_	.3540 /3-	3
3		•	40.70	1084.0	4464 1	1.27		3	2.5	5.86	3.60	.3254	1771	~	SAS CAS	0.01
;	ŕ	0.84	7	77,4-0									1			2
•	;	1		4	V 6-2	1-0	7-N	1 7	7	101	791	RHOVH-1	KHOVA	EPSI-1		FE SPAN
! :	3	1777	F 1	F1/5	F17stC	FT/SEC	F1/5	/SEC		. ر	11/2/11	36 30	107.14	۔ ۔	14.9	ö
١:	7.5			Э	4-775			1.01	\$ 2 2 2 e	• •	20102	27.25	7.7	13.66		
557	177	••	2000	Э				811.1			4 6 7 6	7	7	9.19	0 5.544	ċ
	100	•	557.	0				5 · · ·		•	940	7	2.5	7.47		ö
~	400	•••	534	3			152.6	4.224			E 4771		3.7	4.19		o
2	7	•	547	2				1.246	•	4 6	5.016-	č	4.2	1.276		ö
~	3	•	545	•	306.	8 75.0		9-7901		•		ĕ	44.08	-1.446		ö
5	9	•	5.74	.	365.	786.0		1136.7	١.	,	£ 002	-	4.4	-4.31		Ö
7	2.0	•		•	350		_	1212.0	27. 5-1104.	4 04	-144	19	S	-5.46	î	ò
3	3	•	ž	0	7.5	1100.0	C-9901	1639.	10 177	•	-639.2	36	3.5	54.8	9-	o
7	13		75	Ο,			٠.	1.1001	1006.2-1210.		-861.9	36	42.80	-9-169	-8-	o
7	ž	•	21.5	,	~	1000	11179	1 - 1 - 2 - 1	1971	-1258.2	. ~	•	39.31	-10.6	-10-	o (
٠,	ž		104	•	213		1220.0	•	•	; ?	4.846-	Ġ	36.99		196-11- 50	o .
-	^		155	•	4-807 (1250.1	1757.6	1387.4		•		,				
	#C 17 A 1	461/4	-	10/10	FU/P0	EFF-AU		4.				102/101	P02/P01	EFF-AD RUTOR	REFE DE	
	LON/sec	•	ı	ů.	INLET		Ė	-						~	×	
	1 13.5	エフハ	_			₩						1,1112	1.3792	16.52	87.12	
	35.54	173.44		1.1112	1.3792	86.5	2 87.1	7.7				i i i				

TABLE A-16

AIRFOIL AERODYNAMIC SUMMARY PRINT

	ć	2 5	.3861	.3879	.3598	6607	1.4343	1.5.31	1.5437	1.5469	.5~78	54.75	2454		TEFF-P	וארוסן פיניים	70°07	67.67	01.70	55.0%	67.40	85.81	85.32	83-79	80.61	77.11	13.95	0	31 1	SPAN	0.0916	2651.0	3055	0.4015	0.5002	0.6663	0.7693	0.7468	0.8422	V6000	6676	7 63 6				
	•	-2 P0/P0	-	_	~			٠.			~	_	٠.	•				00.00				_				31	2.32	10.20	-				0 057.6	1.585 0.					_) ^				
	1	FPS			0.0914		22.00	- 1	-0.0721				1421-0-		•													7446		_	_					١		ĩ	7			7	E F F -P	RU1CR	84.29	
.	, ,	FPS1-1	0.3C68	0.2362	0.1695	0.1331	0.0838	7140.0	-0.0557	-0-0175	-0-1312	-0-1439	-0-1724	888	P02/			- 1	100	- ۲	-	•	1.5437	_	_	_	٠,	=	EPS1-1	DEGREE	17.690	13.192		4.303	2.391	-0.158	-3.19	-4.438	-7.518	-8.246	119.6-	19*01-		RCTOR	83,39	
OM TATE	:		ږ										·		L055-P	TUIAL	0.C138	0.0145	210.0	0170-0	8461	FOE 0 - 0	0, 20, 0	0.0308	0.0361	0.0375	0.0414	0.0421	H-2	2SEC	60	96		¥ 7	62	27	41.13	40.74	36.93	38.34		1	4			
TATO SE		KHOVM-2	K6/M2 SEC	175.59	173.66	177.	176	1 78	200.81	193.94	190.06	187.20	19.771	173.73	DMEGA-B	TOTAL	C. 06 3B			0.0944		1 4 24	0000	005	1877	1999	0.230R	.2468	KHOVM-2	LBM/F 12SE	36.09	35.96	35.57	35.57	36.62	39	41.	40,	36,	38	36.45	Š	P02/P01		1.4862	
200 (00)		H-1	SEC	2 7	5.	80	10	* :	10	7 6	90-6	8.05	155.30	8														0	RHOVM-1	LBM/F 12 SEC	.37	32.28	.83	44.26	37		.37	.21	.58	.37	.91	-37	102/101		1 14 38	
100		RHOVH	KC/H2 SEC	14.751	160-29	161.08	162.01	162.94	163.41	162	159	158	155.	153	D FAC		0.5130	0.53	0.5508		47770						٥	0.4734	EHO.	LBM/F	31	32	32								31		102		-	i
	2	764	E/SEC	1,01	4.01-	-87.5	113.6	-136.9	-156.7	2 661-	-214.7	-220.5	232.4	241.8	1 CR N	FCREE	43.27	34.92	27.08	23.09	18-77	15.52	10.40	13.40	10.96	10.43	9.05	8.23	702	F1/SEC	-51.5	-140.5	-231.0	- 287 - 1	0.216	-516-2	-602.0	-631.4	-704.5	-722.3	-762.4	-793.4				
i	5	101	M/SEC	7.101	-205.3	-222.1				- 4.126-		_		393.8 -) i	DEGREE D	14.24	16.61	12.79	11.97	24.6	90.6	¥0.4		7000	•	4.13	4.28	V8 1	ú					0.000											
		-5		1.48.8							. 1.467 . 0 E36			•	HUNE			10.56		10.36		9.76	68.6		9.0	8.87		95.8	~	SEC				511.6				784-4-1108-4	H33.2-1191.4	844.9-1211.8	969.6-1	892.0-1292.0				
		-1 V*	-								٠,	• ^	. ~	~											48.4		.77	.81	>		•					0 4.0101			١.		_	:1				
		>	X '		E-677 1									•	7 7 7 7	0		-			•	•	•				•	•	7	4	•				•					9	8	_	9-1	ξź		94.29
1		0-2	M/SIC			229.7				323.5		P - 040		363.9			0.4034	0	0	0			-		4.74.0			0	2-11	-				7 753.7			•	1001	٠.	1181	1227	1259	٠	-		
2		U-1	M/SEC	159.2	191.4	222.1	247.9	273.2	301.0	327.9	337.8	363.	384.1	393.8		Ti.	0.6247	0-6854	3.1488	0.7921	0.8597	0.9275	1.0024	1.0746	1.1007	1.1027	1-2190	1.2435		1-0	522.3	20.5	673.6	729.7	813.	896.3	767.	10/2-1	110011	1211.8	1260.1	1292.0	į	INLET	H	13.39
•		V 6-2	3384	1 64.3	152.0	0.641	3.4.5	138.0	142.9	1.0.0	元		2 4	142.1	;	ì	45 64	1 3					•	•	0.5602	15 4.0	5266	0.5226	•	, de .	7 20 4	501.A	475.7	4.66.6	. X . 3	4.52.9	100	4.50	200	3	465.3	466.3		INET		1.4862
		0-1	SE	0.0	0-0	ن د د د		0	0.0	0-0	0.0		200] K	440		4243	4310	4342	374	4340		4347	7474		1047	•	- 3	ָ מַלְ	•	0	0.0	0.0	0	0	0	0 0		0	0.0		0/10 NLET		1439
			4/SEC M	6-1	6.4	2.0	7 -	5	4.8	3.3	41.8	vn 1	۵, ۱	24-3		2	ָ בַּרָבָּ	204	110	000	0.71 0	6.35 0	A.56 0	1.99	3.57		200	. ~	;	~ · ·	725.	٥٠٧١	7.60	453.4	32.3	28.5	454.2	70.3	465.4	6 957	618.2	7.70	1			-
		_	_	<u>~</u>	_	۸.	-			_	~			35.5	1	9 0 1	ي د	,	. 0	60	707	7	7 70-	3 96.	\$ 69.	ر. د ر	10.	9 24.		^ ;	٠,	6 -		72.6 4	_	. •	_	•	^		•	4		C 1/A1 6/SEC	SOR	152.09
	Speed	>	Ì	=	-	~ ·		1 -		7	Ä	7.		-		3	20 C 20 C 20 C	•	` `		5	6	4	5	9	3	4	9.		> '	<u>۔</u> ن	2 G	. 0		4	4	, ,	4	4	•	•	. 4		¥ ¥ س		-
	Percent	, 1			203.9								661	199	1	E.	DEGR.	7 .	,	1	,	1	7,	,	1	*	4	1 1	:	>	175	က္က (၁)		3	527	£23	652	657	53	9	c .	0		HC1/A1	SCFT	31.17
	85 P		M/StC	3,	C	3	;	1-/51	9 40	3	1.5.2	141.8	146.7	137.5		8	a (0	3 0) C		0	0.0	2	0-0	0.0	0		1	1-	£ 1/5 °C	444	7.00	472-4	47c.	*-0.2	4.81.1	47.	97.	46544		1.75.				
		į	1	-	~	~	4 ,	^ •	م د	· Œ	•	10	- 1	3 :	:	25		- (٠,	n 4	r w	٠.	, ~	• •	•	10	-	71	}	SL		-	٠,	١ ١	ď	٥	~	œ	•	2	= :	13	:			

APPENDIX B BLADE COORDINATES

MANUFACTURING COORDINATES FOR BLADE SECTIONS NORMAL TO STACKING LINE

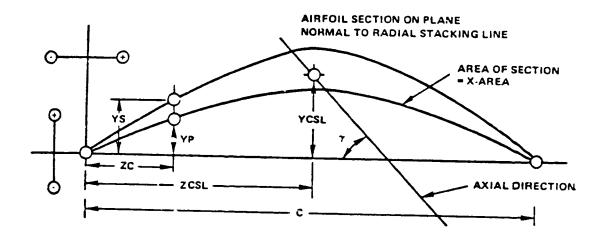


Figure B-1 Airfoil Designations for Manufacturing Coordinates

	METERS			INCHES	
ZC	YP	YS	zc	YP	Y \$
0.0	-0.0003	0.0004	0.0	-0.0117	0.0140
0.0003	-0.0002	0.0005		-0.0077	0.0216
0.0021	0.0004	0.0017	0.0827	0.0166	0.0686
0.0042	0.0011	0.0031	0.1654	0.0448	0.1220
0.0063	0.0018	0.0044	0.2481	0.0711	0.1726
0.0084	0.0024	0.0056	0.3309	0.0957	0.2206
0.0105	0.0030	0.0068	0.4136	0.1187	0.2663
0.0126	0.0036	0.0079	0.4963	0.1402	0.3101
0.0147	0.0041	0.0089	0.5790	0.1603	0.3508
0.0168	0.0045	0.0099	0.6617	0.1788	0.3879
0.0189	0.0050	0.0107	0.7444	0.1955	0.4210
0.0210	0.0053	0.0114	0.8272	0.2104	0.4502
0.0231	0.0057	0.0121	0.9099	0.2233	0.4754
0.0252	0.0060	0.0126	0.9926	0.2343	0.4969
0.0273		0.0131	1.0753	0.2433	0.5144
0.0294		0.0134	1.1580	0.2502	0.5282
0.0315	_	0.0137	1.2407	0.2551	0.5382
0.0336		0.0138	1.3235	0.2578	0.5443
0.0357		0.0139	1.4062	0.2583	0.5464
0.0378		0.0138	1.4889		0.5445
0.0399		0.0137	1.5716	0.2524	0.5384
0.0420		0.0134	1.6543	0.2459	0.5279
0.0441		0.0130	1.7370	0.2368	0.5129 0.4931
0.0462		0.0125	1.8197	0.2251	0.4683
0.0483		0.0119	1.9025	0.2107	0.4380
0.0504		0.0111	1.9852		0.4018
0.0525		0.0102	2.0679		0.3593
0.0546		0.0091	2.1506 2.2333		0.3099
0.0567		0.0079	2.3160		0.2528
0.0588		0.0064	2.3988		0.1873
0.0609		0.0048 0.0028	2.4815	0.0227	0.1122
0.0630			2.5477		0.0429
0.0647	-0.0003	0.0007			
0.0051	-0.0007	0.0001			
RADIUS (METERS)	= 0.1307			5) = 5.1440
CHORD (METERS)	= 0.0651	CHORD		= 2.5643
7051 1	METERCI	= 0.0344			= 1.3535
vesi i	METERSI	= 0.0080	YCSL		5) = 0.3139
RLE (METERSI	20.000330			s) = 0.0130
RTE (METERS)	=0.000531			s) = 0.0209
X-AREA(S	Q.METERS)=0.000342) = 0.5299
GAMMA-CH	HORD (RAD.)= 0.0890	GAMMA-	CHORD (DE	(3.) = 5.10

OR POOR QUARY

	METERS			INCHES	
zc	YP	Y S	zc	YP	YS
0.0	-0.0003	0.0003	0.0	-0.0100	0.0115
	-0.0001	0.0005		-0.0059	0.0182
0.0022	0.0008	0.0020	0.0856	0.0312	0.0778
0.0043	0.0018	0.0036	0.1711	0.0698	0.1398
0.0065	0.0027	0.0050	0.2567	0.1059	0.1981
0.0087	0.0035	0.0064	0.3423	0.1397	0.2528
0.0109	0.0043	0.0077	0.4279	0.1710	0.3039
0.0130	0.0051	0.0089	0.5134	0.1997	0.3516
0.0152	0.0057	0.0101	0.5990	0.2258	0.3957
0.0174	0.0063	0.0111	0.6846	0.2492	0.4360
0.0196	0.0068	0.0120	0.7701	0.2695	0.4716
0.0217	0.0073	0.0127	0.8557	0.2866	0.5019
0.0239	0.0076	0.0134	0.9413	0.3003	0.5273
0.0261	0.0079	0.0139	1.0269	0.3107	0.5478
0.0283	0.0081	0.0143	1.1124	0.3175	0.5634
0.0304	0.0081	0.0146	1.1980	0.3198	0.5735
0.0326	0.0081	0.0147	1.2836	0.3195	0.5790
0.0348	0.0081	0.0147	1.3691	0.3170	0.5806
0.0369	0.0079	0.0147	1.4547	0.3128	0.5787
0.0391	0.0078	0.0146	1.5403	0.3065	0.5731
0.0413	0.0076	0.0143	1.6259	0.2981	0.5635
0.0435	0.0073	0.0140	1.7114	0-2874	0.5499
0.0456	0.0070	0.0135	1.7970	0.2744	0.5319
0.0478	0.0066	0.0129	1.8826	0.2590	0.5093
0.0500	0.0061	0.0122	1.9681	0.2409	0.4819
0.0522	0.0056	0.0114	2.0537		0.4491
0.0543	0.0050	0.0104	2.1393	0.1966	0.4106
0.0565	0.0043	0.0093	2.2249		0.3658
0.0587	0.0036	0.0080	2.3104		0.3141
0.0609	0.0027	0.0065	2.3960		0.2548
0.0630	0.0018	0.0047	2.4816		0.1866
0.0652	0.0008	0.0028	2.5671		0.1084
0.0671		0.0008	2.6408	-0.0077	0.0311
0.0674	-0.0004	0.0005	2.6527	-0.0139	0.0188
RADIUS (METERS)	= 0.1459			1) = 5.7445
CHORD (METERS)	= 0.0674	CHORD		1 = 2.6539
ZCSL (METERS)	= 0.0358	ZCSL	(INCHES	1.4089
YCSL (METERS)	= 0.0090	YCSL	(INCHES	3) = 0.3530
RLE (METERS)	=0.000257	RLE		0.0101
RTE (METERS)	=0.000384	RTE	(INCHES	0.0151
X-AREA(S	Q.METERS	=0.000324	X-AREA	ISQ. IN.	0.5021
GAMMA-CH	ORD (RAD.)= 0.1424	GAMMA-	CHORDIDE	(a) = 8.16

TABLE B-3

MET	ERS		INCHES	
ZC Y	P YS	zc	YP	YS
0.0 -0.0	002 0.0003	0.0	-0.0097	0.0111
0.0002 -0.0	0.0004	0.0083	-0.0057	0.0173
0.0022 0.0		0.0864	0.0312	0.0759
0.0044 0.0		0.1727	0.0704	0.1378
0.0066 0.00		0.2591	0.1076	0.1964
0.0088 0.0		0.3454	0.1426	0.2518
0.0110 0.00		0.4316	0.1755	0.2040
0.0132 0.00		0.5182	0.2060	0.3531
0.0154 0.00		0.6045	0.2336	0.3983
0.0175 0.00		0.6909	0.2584	
0.0197 0.00		0.7773	0.2803	0.4398
0.0219 0.00		0.8636		0.4768
0.0241 0.00		0.9500	0.2994 0.3152	0.5090
0.0263 0.00		1.0364		0.5363
0.0285 0.00			0.3278	0.5588
0.0307 0.00		1.1227	0.3371	0.5766
0.0329 0.00		1.2091	0.3430	0.5895
0.0351 0.00		1.2954	0.3455	0.5976
0.0373 0.00		1.3818	0.3444	0.6008
0.0395 0.00		1.4682	0.3395	0.5988
0.0417 0.00	_	1.5545	0.3307	0.5914
0.0439 0.00	_	1.6409	0.3198	0.5790
	_	1.7273	0.3069	0.5634
		1.8136	0.2922	0.5438
		1.9000	0.2750	0.5201
		1.9864	0.2551	0.4912
		2.0727	0.2326	0.4571
		2.1591	0.2073	0.4173
		2.2454	0.1791	0.3713
		2.3318	0.1477	0.3183
	· -	2.4182	0.1130	0.2576
0.0636 0.00		2.5045	0.0748	0.1881
0.0658 0.00	<u> </u>	2.5909	0.0329	0.1084
0.0677 -0.00		2.6664	-0.0071	0.0285
0.0680 -0.00	0.0004	2.6772	-0.0128	0.0171
RADIUS (METERS	= 0.1509	RADIUS	LINCHES) = 5.9420
CHORD (METERS	0.0680	CHORD) = 2.6790
ZCSL (METERS	= 0.0362			= 1.4252
YCSL (METERS	= 0.0092	YCSL	INCHES) = 0.3617
RLE (METERS	=0.000249	RLE	ITNCHES) = 0.0098
RTE (METERS	=0.000348		ITNCHES	0.0098 0.0137
X-AREAISQ.METE			ISO TH) = 0.0137) = 0.4939
GAMMA-CHORD (RA			134. TM.	·)= 0.4939 ·)= 9.59
J.		JENTINE .	107 D (050	・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・・

TABLE B-4

MET	TER S		INCHES	
ZC Y	P YS	ΣC	YP	YS
0.0 -0.0	0002 0.0003	0.0	-0.0094	0.0107
0.0002 -0.0		0.0082	-0.0057	0.0166
	0.0019	0.0872	0.0305	0.0736
	0.0034	0.1744	0.0690	0.1339
	0.0049	0.2616	0.1056	0.1912
	0.0062	0.3488	0.1403	0.2455
	0.0075	0.4360	0.1731	0.2968
	052 0.0088	0.5232	0.2033	0.3453
	0.0099	0.6104	0.2325	0.3909
	066 0.0110	0.6976	0.2590	0.4338
	0.0120	0.7848	0.2832	0.4728
	0.0129	0.8720	0.3048	0.5075
	082 0.0137	0.9592	0.3234	0.5375
	086 0.0143	1.0464	0.3389	0.5630
	089 0.0148	1.1336	0.3507	0.5835
	091 0.0152 093 0.0155	1.2208	0.3591	0.5987
		1.3080	0.3643	0.6093
		1.3952	0.3661	0.6152
	093 0.0156 091 0.0155	1.4824	0.3643	0.6161
=	0.0153	1.5696	0.3589	0.6119
	085 0.0149	1.6568 1.7440	0.3496	0.6025
	081 0.0144	1.8312	0.3364	0.5874
	075 0.0137	1.9184	0.3188 0.2968	0.5664
	069 0.0128	2.0056		0.5390
	062 0.0118	2.0928	0.2698 0.2434	0.5043
	055 0.0107	2.1800	0.2162	0.4641
	048 0.0095	2.2672	0.1873	0.4220 0.3752
	039 0.0082	2.3544	0.1545	0.3219
0.0620 0.0		2.4416	0.1183	0.2601
0.0642 0.0		2.5288	0.0786	0.1894
0.0664 0.0		2.6160	0.0351	0.1084
0.0684 -0.0	002 0.0007		-0.0055	0.0264
0.0687 -0.0	003 0.0004		-0.0119	
0.07.4				
RADIUS (METER		RADIUS		= 6.1420
CHORD (METER		CHORD		= 2.7037
ZCSL (METER: YCSL (METER:		ZCSL		= 1.4440
· - · - · ·		YCSL		= 0.3708
	S) =0.000244 S) =0.000244	RLE		= 0.0096
	S) =0.000323	RTE		= 0.0127
CAMMA CHUDU LD	ERS)=0.000313 AD.)= 0.1915	-	(5Q. IN.)	= 0.4855
GANDATCHUKU (K)	AU . J= U. 1915	GAMMA-CH	HORD (DEG.)= 10.97

TABLE B-5

METERS		INCHES	
ZC YP	YS ZC	YP	YS
	0.0003 0.0	-0.0093	0.0104
	0.0004 0.0082		0.0161
	0.0018 0.0881		0.0713
	0.0033 0.1762		1298
	0.2643		1856
	0.0061 0.3524		.2387
	0.0073 0.4405		2892
	0.0086 0.5286		3370
	0.0097 0.6166		3822
	0.0108 0.7047		-4250
	0.0118 0.7928		.4665
	0.0127 0.8809 0.0135 0.9690		5001
			5313
	0.0142 1.0571 0.0147 1.1452		0.5580 0.5803
	0.0152 1.2333).5982
	0.0155 1.3214		0.5762
	0.0158 1.4095		0.6208
	0.0159 1.4976		0.6253
	0.0159 1.5857		0.6251
	0.0157 1.6737		0.6196
	0.0155 1.7618		0.6083
	0.0150 1.8499		0.5914
	0.0144 1.9380		5684
0.0515 0.0079	2.0261		5390
0.0537 0.0073	0.0128 2.1142	0.2861 (-5026
	0.0116 2.2023	0.2542	.4582
	2.2904	0.2169	0.4051
	2.3795		.3419
	2.4666		0.2663
	0.0048 2.5547		1888
	0.0027 2.6428		1065
0.0691 -0.0002		-0.0062	
0.0694 -0.0003	2.7309	-0.0113	0.0149
RADIUS (METERS) =	0.1612 RADIUS	(INCHES)	= 6.3470
CHORD (METERS) =	0.0694 CHORD	(INCHES)	= 2.7324
CCSL (METERS) =			
CSL (METERS) =		(INCHES)	= 0.3783
tle (METERS) =		(INCHES)	= 0.0094
RTE (METERS) =			= 0.0120
(-AREA(SQ.METERS)=			
SAMMA-CHORD(RAD.)=	0.2150 GAMMA-	CHORDIDEG.1	= 12.32

TABLE B-6

	METERS			INCHES	
zc	YP	YS	zc	YP	YS
0.0	-0.0002	0.0003	0.0	-0.0092	0.0102
0.0002		0.0004		-0.0057	0.0156
0.0023		0.0017	0.0892	0.0281	0.0686
0.0045		0.0032	0.1783	0.0641	0.1248
0.0068		0.0045	0.2675	0.0987	0.1784
0.0091		0.0058	0.3567	0.1316	0.2296
0.0113		0.0071	0.4459	0.1629	0.2782
0.0136		C •0082	0.5351	0.1927	0.3244
0.0159		0.0094	0.6242	0.2208	0.3682
0.0181		0.0104	0.7134	0.2473	0.4099
0.0204		0.0114	0.8026	0.2721	0.4487
0.0227		0.0123	0.8918	0.2949	0.4842
0.0249		0.0131	0.9809	0.3151	0.5157
0.0272		0.0138	1.0701	0.3328	0.5428
0.0294	0.0088	0.0144	1.1593	0.3478	0.5656
0.0317	0.0091	0.0148	1.2485	0.3600	0.5843
0.0340	0.0094	0.0152	1.3376	0.3694	0.5987
0.0362	0.0095	0.0155	1.4268	0.3759	0.6089
0.038	0.0096	0.0156	1.5160	0.3793	0.6146
0.0408		0.0156	1. 052	0.3796	0.6158
0.0430		0.0156	1.,944		0.6123
0.0453		0.0153	1.7835		0.6040
0.047		0.0150	1.8727	0.3603	0.5904
0.049		0.0145	1.9619		0.5714
0.052		0.0139	2.0511		0.5464
0.054		0.0131	2.1402		0.5149
0.056		0.0121	2.2294		0.4754
0.0589		0.0109	2.3186		0.4276 0.3706
0.061		0.0094	2.4078		0.3029
0.063		0.0077	2.4969 2.5861		0.2229
0.065		0.0057	2.6753		0.1278
0.068	0.0014	0.0032 0.0006	2.7569		0.0244
		0.0004			
0.070	2 -0.0003	0.0004	2.043	-0.0113	0.0140
		= 0.1661	RADIUS		5) = 6.5400
CHORD	(METERS)	= 0.0703	CHORD		5) = 2.7666
ZCSL	(METERS)	= 0.0377			1.4856
YCSL	(METERS)	= 0.0095			3) = 0.3749
		=0.000236			5) = 0.0093
		=0.000267			s) = 0.0105
					0.4670
GAMMA-C	HORD(RAD.) = 0.2488	GAMMA-	CHORD (DE	3.) = 14.26

TABLE B-7

	METERS			INCHES	
ZC	YP	YS	zc	YP	YS
0.0	-0.0002	0.0002	0.0	-0.0089	0.0096
	-0.0002	0.0004	0.0085		0.0142
0.0024	0.0006	0.0015	0.0926	0.0220	0.0595
0.0047	0.0013	0.0027	0.1852		0.1077
0.0071	0.0020	0.0039	0.2779		0.1537
0.0094	0.0027	0.0050	0.3705		0.1976
0.0118	0.0034	0.0061	0.4631		0.2394
0.0141	0.0040	C.0071	0.5558	0.1580	0.2790
0.0165	0.0046	0.0080	0.6484	0.1812	0.3166
0.0188	0.0052	0.0089	0.7410	0.2028	0.3523
0.0212		0.0098	0.8336	0.2232	0.3857
0.0235		0.0106	0.9263	0.2419	0.4172
0.0259		0.0113	1.0189	0.2590	0.4454
0.0282		0.0119	1.1115	9.2740	0.4700
0.0306		0.0125	1.2042		0.4907
0.0329		0.0129	1.2968	0.2973	0.5077
0.0353		0.0132	1.3894	0.3055	0.5207
0.0376		0.0135	1.4820	0.3113	0.5300
0.0400		0.0136	1.5746	_	0.5352
0.0423		0.0136	1.6673	0.3151	0.5364
0.0447		0.0135	1.7599		0.5334
0.0471		0.0134	1.8525		0.5259
0.0494		0.0131	1-9452		0.5138
0.0518		0.0126	2.0378	0.2886	0.4968
0.0541		0.0121	2.1304	0.2739	0.4744
0.0565		0.0113	2.2230	0.2552	0.4463
0.0588		0.0105	2.3157	0.2323	0.4118
0.0612		0.0094	2.4083	0.2051	0.3700
0.0635		0.0081	2.5009	0.1732	0.3204
0.0659 0.0682		0.0066	2.5935	0.1363	0.2616
0.0706		0.0049 0.0028	2.6862 2.7788		0.1922
	-0.0001	0.0005	2.8635	0.0451 -0.0054	0.1101
		0.0003		-0.0054	0.0211
0.0129	-0.0003	0.0003	2.5/14	-0.0101	0.0128
RADIUS (METERS)	= 0.1775	RADIUS	(TNCHES) = 6.9882
	METERS)	= 0.0730	CHORD) = 2.8730
	METERS)	= 0.0391	ZCSL) = 1.5387
	METERS)	= 0.0079	YCSL) = 0.3116
	METERS)	=0.000236	RLE) = 0.0093
		=0.000257) = 0.0101
		=0.000289) = 0.4483
)= 0.3535			.)= 20.25

TABLE B-8

METERS			INCHES	
ZC YP	YS	zc	YP	YS
0.0 -0.0002	0.0002	0.0	-0.0088	0.0093
0.0002 -0.0002		0.0090	-0.0069	0.0126
0.0025 0.0003		0-1000	0.0118	0.0463
0.0051 0.0008	0.0021	C • 2000	0.0316	0.0819
0.0076 0.0013	0.0029	0.3001	0.0504	0.1160
0.0102 0.0017		0-4001	0.0683	0.1484
0.0127 0.0022		0.5001	0.0852	0.1791
0.0152 0.0026		0.6001	0.1010	0.2082
0.0178 0.0029		0.7001	0.1158	0.2356
0.0203 0.0033		0.8002	0.1295	0.2613
0.0229 0.0036		0.9002	0.1421	0.2854
0.0254 0.0039		1.0002	0.1536	0.3079
0.0279 0.0042		1.1002	0.1641	0.3286
0.0305 0.0044 0.0330 0.0046		1.2002	0.1733	0.3474
0.0356 0.0048		1.3003	0.1811	0.3632
0.0381 0.0049		1.4003 1.5003	0.1873	0.3759 0.3854
0.0406 0.0049	-	1.6003	0.1919	0.3916
0.0432 0.0050		1.7003	0.1959	0.3944
0.0457 0.0050		1.8004	0.1954	0.3940
0.0483 0.0049		1.9004	0.1929	0.3901
0.0508 0.0048		2.0004	0.1886	0.3826
0.0534 0.0046		2.1004	0.1824	0.3716
0.0559 0.0044	0.0091	2.2004	0.1741	0.3568
0.0584 0.0042	0.0086	2-3005	0.1638	0.3380
0.0610 0.0038	0.0080	2.4005	0.1513	0.3151
0.0635 0.0035		2.5005	0.1364	0.2878
0.0661 0.0030		2.6005	0.1192	0.2559
0.0686 0.0025		2.7005	0.0995	0.2188
0.0711 0.0020		2.8005	0.0770	0.1762
0.0737 0.0013		2.9006	0.0517	0.1276
0.0762 0.0006		3.0006	0.0234	0.0721
0.0786 -0.0001		3.0926	-0.0055	0.0143
0.0798 -0.0002	0.0002	3.1006	-0.0083	0.0093
RADIUS (METERS)	= 0.2028	RADIUS	ITNCHES) = 7.9850
CHORD (METERS)	= 0.0788	CHORD) = 3.1012
ZCSL (METERS)	= 0.0416	ZCSL) = 1.6383
YCSL (METERS)	= 0.0049	YCSL) = 0.1937
	=0.000239	RLE) = 0.0094
RTE (METERS)		RTE) = 0.0089
X-AREA(SQ.METERS			(SO. IN.	1 = 0.4234
GAMMA-CHORD (RAD.)= 0.5316	GAMMA-C	HORD (DEG	.)= 30.46

	METERS			INCHES	
ZC	YP	YS	zc	YP	YS
0.0	-0.0002	0.0002	0.0	-0.0087	0.0090
0.0002	-0.0002	0.0003	0.0091	-0.0075	0.0093
0.0027		0.0010	0.1057	0.0055	0.0384
0.0054	0.0005	0.0017	0.2114	0.0191	0.0663
0.0081	0.0008	0.0024	0.3170	0.0318	0.0928
0.3107	0.3011	0.0030	0.4227	0.0436	0.1178
0-0134	0.0014	0.0036	0.5284	0.0546	0.1414
0.0161	0.0016	0.0042	0.6340	0.0648	0.1635
0.0188	0.0019	0.0047	0.7397	0.0742	0.1841
0.0215	0.0021	0.0052	0.8454	0.0826	0.2033
0.0242	0.0023	0.0056	0.9510	0.0903	0.2211
0.0268	0.0025	0.0060	1.0567	0.0970	0.2374
0.0295	0.0026	0.0064	1.1624	0.1029	0.2523
0.0322	0.0027	0.0068	1.2681	0.1080	0.2658
0.0349	0.0028	0.0071	1.3737	0.1121	0.2777
0.0376	0.0029	0.0073	1.4794	0.1152	0.2876
0.0403	0.0030	0.0075	1.5851	0.1173	0.2949
0.0429	0.0030	0.0076	1.6908	0.1184	0.2995
0.0456	0.0030	0.0077	1.7964	0.1184	0.3013
0.0483	0.0030	0.0076	1.9021	0.1174	0.3004
0.0510	0.0029	0.0075	2.0078	0.1152	0.2967
0.0537	0.0028	0.0074	2.1135	0.1119	0.2902
0.0564	0.0027	0.0071	2.2191	0.1075	0.2808
0.0590	0.0026	0.0068	2.3248	0.1018	0.2685
0.0617	0.0024	0.0064	2.4305	0.0950	0.2532
0.0644	0.0022	0.0060	2.5361	0.0869	0.2348
0.0698	0.0020	0.0054	2.6418	0.0775	0.2132
0.0078	0.0017	0.0048	2.7475	0.0669	0.1883
0.0752	0.0014 0.0011	0.0041	2.8532	0.0549	0.1599
0.0778	0.0007	0.0032	2.9588	0.0415	0.1279
0.0805	0.0003	0.0023	3.0645	0.0267	0.0920
0.0830	-0.0003	0.0013	3.1702	0.0104	0.0520
	-0.0002	0.0003 0.0002		-0.0060	0.0113
33032	0.0002	0.0002	3.2759	-0.0073	0.0080
RADIUS (M	ETERS) :	= 0.2281	RADTUS	ITNOHES	= 8.9819
	ETERS) :	= 0.0832	CHORD	(THE HES)	= 3.9819
ZCSL (M	ETERS) :	= 0.0436	ZCSL	(INCHES)	= 1.7149
ACRF (W	ETERS) :	0.0029	YCSL	(INCHES)	= 0.1125
RLE (M	ETERS) =	0.000236	RLE	(INCHES)	= 0.1125 = 0.0093
RTE (M	ETERS) :	0.000208	RTF	(INCHES)	= 0.0082
X-AREAISQ	.METERS) =	0.000263	Y-ADEA A	SO. IN	= 0.4074
GAMMA-CHO	RD(RAD.)=	0.6579		IORD (DEG.)= 37.69
					, - 5, •07

TABLE B-10

	METERS			INCHES	
ZC	YP	YS	2 C	YP	YS
0.0	-0.3002	0.0002	0.0	-0.0088	0.0090
	-0.6002	0.0003	0.0093	-0.0080	0.0129
0.0028	0.0000	0.0008	C-1104	0.0003	0.0320
0.0056	0.0002	0.0014	0.2208	0.0088	0.0538
0.0094	0.0004	0.0019	0.3312	0.0168	0.0745
0.0112	3.3006	0.3024	0.4416	0.0242	0.0940
0.0140	0.0006	0.0029	0.5520	0.0310	0.1122
0.0168	0.0009	0.0033	0.6623	0.0372	0.1293
0.0196	0.0011	0.0037	0.7727	0.0428	0.1452
0.0224	0.0012	0.0041	0.8831	0.0478	0.1598
0.0252	0.0013	0.0044	0.9935	0.0523	0.1733
0.3280	0.0014	0.0047	1.1039	0.0561	0.1856
0.0308	0.0015	0.0050	1.2143	0.0594	0.1967
0.0336	0.0016	0.0052	1.3247	0.0620	0.2066
0.0365	0.0016	0.0055	1.4351	C.0641	0.2154
0.0393	0.0017	0.0057	1.5455	0.0656	0.2229
0.0421	0.0017	0.0058	1.6559	0-0664	0.2290
0.0449	0.0017	0.0059	1.7663	0.0667	0.2331
0.0477	0.0017	0.0060	1.8766	0.0664	0.2348
0.0505	0.0017	0.0060	1.9870	0.0654	0.2343
0.0533	0.0016	0.0059	2.0974	0.0637	0.2314
0.0561	0.0016	0.0057	2.2078	0.0614	0.2261
0.0539	0.0015	0.0056	2.3182	0.0585	0.2185
0.0617	0.0014	0.0053	2.4286	0.0549	0.2086
0.0645	0.0013	0.0050	2.5340	0.0506	0.1962
0.0673	0.0012	0.0046	2.6494	0.0457	0.1814
0.0701	0.0010	0.0042	2.7508	0.0401	0.1642
0.0729	0.0009	0.0037	2.8702	0.0339	0.1445
0.0757	0.0007	0.0031	2.9806	0.0270	0.1222
0.0785	0.3005	J.0025	3.0910	0.0195	0.0974
0.0813	0.0003	0.0018	3.2013	0.0114	0.0694
0.0841	0.0001	0.0010	3.3117	0.0027	0.0397
		0.0002		-0.0060	
0.0869	-0.0002	0.0002	3.4221	-0.0066	0.0000
RADIUS (METERS)	= 0.2535			51 = 9.9799
		= 0.0869	CHORD	(INCHES	3.4222
ZCSL (METERS)	= 0.0451	ZCSL	(INCHE	51 = 1.7759
YCSL (METFKS)	= 0.0013	YCSL	(INCHE	s) = 0.0519
વાદ (METERS)	=0.000239	RLE	(INCHE	s) = 0.0094
RIE (METERS	=0.000188	RTE		5) = 0.0074
		=0.000253	X-AREA		0.3919
		= 0.7633		CHORD (DE	G.) = 43.73

METERS INCHES ZCYP YS ZC VP. YS 0.0 -0.0002 0.0002 0.0 -0.0088 0.0090 0.0002 -0.0002 0.0003 0.0093 -0.0083 0.0105 0.0029 -0.0001 0.0007 0.1146 -0.003C 0.0290 0.0058 0.0001 0.0012 0.2292 0.0023 0.0459 0.0087 0.0002 0.0016 0.3438 0.0071 0.9626 0.0116 0.0003 0.0020 0.4584 0.0114 0.0782 0.0145 0.0004 0.0024 0.5730 0.0154 0.0930 0.0175 0.0005 0.0027 0.6876 0.0190 0.1556 0.0204 0.0006 0.0030 0.8022 0.0222 0.1192 0.0253 0.0006 0.0033 0.9168 0.0248 0.1306 0.0262 0.0007 0.0036 1.0314 0.0270 0.1410 0.0291 0.0007 0.0038 1.1460 0.0287 0.1502 0.0320 0.0008 0.0040 1.2606 0.0299 0.1584 0.0349 9.0008 0.0042 1.3752 0.0307 0.1655 0.0378 0.0008 0.0044 1.4898 0.0310 0.1715 0.0408 0.0003 0.0045 1.6044 0.0309 0.1764 0.0437 0.00(3 0.0046 1.7191 0.0303 0.1803 0.0466 0.000: 0.0046 1.8336 0.0292 0.1830 0.0495 0.0007 0.0047 1.9482 0.0280 0.1841 0.0524 0.00(7 0.0047 2.0629 0.0265 0.1834 0.0553 0.0005 0.0046 2.1775 0.0250 0.1809 0.0582 0.0003 0.0045 2.2921 0.0232 0.1765 0.0611 0.0005 0.0043 2.4067 0.0213 0.1703 0.0640 0.0005 0.0041 2.5213 0.0193 0.1622 0.0670 0.0004 0.0039 2.6359 0.0169 0.1523 0.0699 0.0004 0.0036 2.7505 0.0145 0.1406 0.0728 0.0003 0.0032 2.8651 0.0120 0.1270 0.0757 0.0002 0.0028 2.9797 0.3092 0.1115 0.0786 0.0002 0.3024 3.0943 0.0064 0.0942 0.0815 0.0001 0.0019 3.2089 0.0034 0.0750 0.0844 0.0000 0.6014 3.3235 0.0003 0.0540 0.0873 -0.0001 8000.0 3.4381 -0.0029 0.0310 0.0401 -0.0001 0.0002 3.5460 -0.0059 0.0077 0.0902 -0.0002 0.0002 5.5527 -0.0061 0.0063 RADIUS (METERS) 0.2788 RADIUS (INCHES) = 10.4762 CHURD (METERS) = 0.0902 CHORD (INCHES) = 3.5527ZCSL (METERS) 0.0464 ZCSL (INCHES) = 1.8279YCSL (METERS) 0.0001 YCSL (INCHES) = 0.0039RLE (METERS) =0.000236 BLE (INCHES) = 0.0093H TE (METERS) =0.000170 RTE (INCHES) = 0.0067X-AREA(SQ.METERS)=0.000245 X-AREA (SO. IN.) = 0.3797GAMMA-CHORD(RAD.) = 0.8159 GAMMA-CHORD(DEG.)= 46.75

C. .

TABLE B-12

METERS		INCHES			
20	ΥP	YS	zc	YP	YS
0.0	-0.0002	0.0002	0.0	-0.0088	0.0090
	-0.0002	0.0003	0.0093		0.0105
	-0.0001	0.0007	0.1159		0.0280
0.0059		0.0012	0.2318		0.0458
0.0088		0.0016	0.3478		0.0623
0.0118		0.0020	0.4637		0.0777
0.0147		0.0023	0.5796		0.0913
0.0177		0.0027	0.6935		0.1047
0.0206	0.0005	0.0030	0.8115	0.0208	0.1164
0.0236	0.0006	0.0032	0.9274	0.0228	0.1270
0.0265	0.0006	0.0035	1.0433	0.0243	0.1364
0.0294	0.0006	0.0037	1.1592	0.0252	0.1446
0.0324	0.0007	0.0039	1.2751	0.0256	0.1517
0.0353	0.0006	0.0040	1.3911	0.0255	0.1576
0.0383	0.0006	0.0041	1.5070		0.1624
0.0412	0.000	0.0042	1.6229	0.0238	0.1660
0.0442		0.0043	1.7388		0.1685
0.0471		0.0043	1.8547		0.1699
0.0501		0.0043	1.9707		0.1700
0.0530		0.0043	2.0866		0.1684
0.0559		0.0042	2.2025		0.1654
0.0589		0.0041	2.3184		0.1607
0.0618		0.0039	2.4343		0.1544
0.0648		0.0037	2.5503		0.1466
0.0677		0.0035	2.6662	0.0047	0.1372
0.0707		0.0032	2.7821		0.1262
0.3736		0.0029	2.8980		0.1737
	-0.0000	0.0025	3.0140		0.0996
	-0.0000 -0.0001	0.0021	3.1299		0.0840 0.0668
	-0.0001	0.0017 0.0012	3.2458	-0.0032 -0.0043	0.0668
	-0.0001	0.0007	3.4776		0.0278
	-0.0001	0.0002	3.5871		0.0073
		0.0002		-0.0059	
0 0 0 7 13	0 60002	0 0 0 0 0 0 0	3.37.39	• • • • • • • • • • • • • • • • • • • •	340 01
RADIUS (METERS)	= 0.2872	RADIUS	(INCHES) =11.3080
		= 0.0913) = 3.5925
		= 0.0468			1 = 1.8443
		= -0.0002) =-0.0096
		=0.000239) = 0.0094
					= 0.0065
X-AREA(S	Q.METER SI	=0.000243			
GAMMA-CH	GKD (RAD.)	= 0.8204	GAMMA-	CHORD(DEG	·)= 47.00



MS	TERS		INCHES	
zc	YP YS	zc	YP	YS
0.0 -0.	.0002 0.00	0.0	-0.0088	0.0090
0.0002 -0.	0.002	0.009	-0.0084	0.0105
0.0030 -0.	.0001 0.00	0.1169	9 -0.0029	0.0278
0.0059 0	.0001 0.00	0.233	0.0025	0.0454
0.0089 0.	.0002 0.00	0.350	7 0.0072	0.0617
0.0119 0.	.0003 0.00	0.467	5 0.0114	0.0768
0.0148 0.	.0004 0.00	0.584	5 0.0149	0.0906
0.0178 0.	.0005 0.00	0.701	4 0.0178	0.1031
0.0208 0.	.0005 0.00	0.818	3 0.0201	0.1145
0.0238 0.	.0006 0.00	0.935	2 0.0219	0.1246
0.0267 0.	.0006 0.00	1.052	1 0.0230	0.1334
0.0297 0.	.0006 0.00	1.169	0.0236	0.1411
0.0327 0	.0006 0.00	1.285	9 0.0237	0.1477
0.0356 0	.0006 0.00	1.402	9 0.0232	0.1530
0.0386 0	.0006 0.00	1.519	7 0.0221	0.1571
0.0416 0	.0005 0.00	1.636	7 0.0205	0.1601
0.0445 0	.0005 0.00	1.753	6 0.0184	0.1619
0.0475 0	.0004 0.00	1.870	5 0.0157	0.1626
0.0505 0	.0003 0.00	1.987	4 0.0127	0.1620
0.0534 0	.0002 0.00	2.104	3 0.0097	0.1600
0.0564 0	.0002 0.00	2.221	2 0.0071	0.1566
0.0594 0	.0001 0.00	2.338	1 0.0046	0.1518
0.0624 0	.0001 0.00	2.455	0 0.0024	0.1455
0.0653 0	.0000 0.00	2.571	9 0.0004	0.1378
0.0683 -0	.0000 0.00	2.688	8 -0.0014	0.1287
0.0713 -0	.0001 0.00	2.805	7 -0.0030	0.1182
0.0742 -0	.0001 0.00	2.922	6 -0.0042	0.1063
0.0772 -0	.0001 0.00	3.039	5 - 0.0052	0.0930
0.0802 -0	.0002 0.00	3.156	4 - 0.0060	0.0783
0.0831 -0	.0002 0.00			0.0622
0.0861 -0	.0002 0.00			0.0448
	.0002 0.00			0.0260
0.0919 -0	.0001 0.00	3.617		
0.0921 -0	.0001 0.00	3.624	0 - 0.0058	0.0059
	ERS) = 0		S (INCHES	
CHORD [MST	ERS) = 0		(INCHES	
ZCSL (MET	ERS) = 0	.0472 ZCSL	(INCHES	
YOSL (MET	ERS) = -0	.0005 YCSL	(INCHES	=-0.0180
RLE (MET		00239 RLE	(INCHES) = 0.0094
RTE (MET			(INCHES	
M-CRIABRA-X			A (SQ. IN.	
GAMMA-CHORD	(RAD.) = 0.	8235 GAMMA	-CHORDIDEG	.)= 47.19

TABLE B-14

METE	2.5	INCHES	
ZC YP	YS	ZC YP	YS
0.0 -0.000 0.0002 -0.000 0.0030 -0.000 0.0060 0.000 0.0090 0.000	02 0.0003 01 0.0007 01 0.0012 02 0.0016 03 0.0019	0.0 -0.0089 0.0094 -0.0084 0.1179 -0.0030 0.2357 0.0025 0.3536 0.0072 0.4714 0.0114	0.0106 0.0276 0.0451 0.0612 0.0761
0.0150 0.000 0.0180 0.000 0.0210 0.000 0.0239 0.000 0.0269 0.00 0.0299 0.00	05 0.0026 05 0.0029 06 0.0031 06 0.0033	0.5893	0.1020 0.1130 7 0.1228 7 0.1314 2 0.1387
0.0359 0.00 0.0389 0.00 0.0419 0.00 0.0449 0.00 0.0479 0.00 0.0509 0.00	06 0.0038 05 0.0039 05 0.0040 04 0.0040 03 0.0040	1.4144 0.0223 1.5322 0.0210 1.6501 0.0193 1.7679 0.0168 1.8858 0.013 2.0037 0.0103	3 0.1497 0 0.1534 1 0.1559 3 0.1572 7 0.1574 2 0.1563
0.0539 0.00 0.0569 0.00 0.0599 0.00 0.0629 -0.00 0.0659 -0.00	01 0.0038 00 0.0037 00 0.0035 01 0.0033 01 0.0031	2.1215 0.0065 2.2394 0.0031 2.3573 0.0005 2.4751 -0.0015 2.5930 -0.0035	7 0.1502 9 0.1452 5 0.1388 7 0.1312 5 0.1222
0.0718 -0.00 0.0748 -0.00 0.0778 -0.00 0.0808 -0.00 0.0838 -0.00 0.0868 -0.00 0.0898 -0.00	02 0.0026 02 0.0022 02 0.0019 02 0.0015 02 0.0011	2.8287 -0.0069 2.9466 -0.0080 3.0644 -0.0090 3.1823 -0.0090 3.3002 -0.0080 3.4180 -0.0080 3.5359 -0.0070	0.1005 7 0.0879 0 0.0738 8 0.0586 2 0.0422
0.0426 -0.00 0.0428 -0.00 RADIUS (METERS	01 0.0002 01 0.0001) = 0.2999	3.6475 -0.0058 3.6534 -0.0058 RADIUS (INCH	8 0.0063 7 0.0058 ES) =11.8062
CHORD (METERS ZCSL (METERS YCSL (METERS RLE (METERS RTE (METERS X-AREA(SU-METERS GAMMA-CHORD(RA) = 0.0474) = -0.0005) =0.000239) =0.000163 RS)=0.000238	YOSL (INCH PLS (INCH RTE (INCH	ES) = 1.8674 ES) =-0.0242 ES) = 0.0094 ES) = 0.0064 N.) = 0.3694

TABLE B-15

METERS			INCHES	
ZC YP	YS	zc	YP	YS.
0.0 -0.0002 0.0002 -0.0002 0.0030 -0.0001 0.0060 0.0000 0.0091 0.0001 0.0121 0.0003 0.0151 0.0003 0.0151 0.0003 0.0211 0.0004 0.0241 0.0005 0.0272 0.0005 0.0332 0.0005 0.0362 0.0005 0.0392 0.0004	0.0002 0.0003 0.0001 0.0015 0.0019 0.0022 0.0025 0.0030 0.0032 0.0030 0.0035 0.0035 0.0036	0.0 0.0094 0.1188 0.2376 0.3564 0.4753 0.5941 0.7129 0.8317 0.9505 1.0693 1.1881 1.3069 1.4257 1.5445	-0.0089 -0.0085 -0.0036 0.0012 0.0054 0.0122 0.0147 0.0166 0.0180 0.0188 0.0190 0.0187 0.0165 0.0147	0.0091 0.0105 0.0268 0.0435 0.0589 0.0731 0.0861 0.0979 0.1084 0.1177 0.1258 0.1327 0.1384 0.1430 0.1464 0.1486
0.0422 0.0004 0.0453 0.0003 0.0483 0.0002 0.0513 0.0002 0.0543 0.0001 0.0573 -0.0000 0.0604 -0.0001 0.0634 -0.0002 0.0694 -0.0002 0.0694 -0.0003 0.0754 -0.0003 0.0754 -0.0003 0.0754 -0.0003 0.0815 -0.0003 0.0815 -0.0003 0.0875 -0.0002 0.0905 -0.0002 0.0934 -0.0001	0.0038 0.0038 0.0038 0.0037 0.0036 0.0035 0.0034 0.0032 0.0030 0.0027 0.0024 0.0021 0.0010 0.0010 0.0006 0.0002	1.6634 1.7822 1.9010 2.0198 2.1386 2.2574 2.3762 2.4950 2.6138 2.7327 2.8515 2.9703 3.0891 3.2079 3.3267 3.4455 3.5643 3.6770	0.0123 0.0094 0.0062 0.3029 -0.0002 -0.0052 -0.0071 -0.0087 -0.3099 -0.0106 -0.0109 -0.0108 -0.0102 -0.0091 -0.0076	0.1498 0.1498 0.1483 0.1465 0.1430 0.1382 0.1322 0.1249 0.1164 0.1067 0.0957 0.0836 0.0703 0.0559 0.0403 0.0235
RADIUS (METERS) CHORD (METERS) ZCSL (METERS) YCSL (METERS) RLE (METERS) RTE (METERS) X-ARFA(SO.METERS) GAMMA-CHORD(RAD.	=0.000241 =0.000152 ,)=0.000236	X-ARE	INCHE INCHE INCHE INCHE INCHE INCHE	S) = 12.0552 S) = 3.6831 S) = 1.6773 S) = -0.0320 S) = 0.0095 S) = 0.0060 I.) = 0.3654 E() = 49.26

TABLE B-16

METERS		1	INCHES	
ZC YP	YS	zc	YP	YS
0.0 -0.0002	0.0002	0.0	-0.0089	0.0091
		- • .	-0.0086	0.0104
		• • • •	-0.0049	0.0254
			-0.0012	0.0408
		0.3593	0.0020	0.0549
		0.4790	0.0047	0.0680
		0.5988	0.0070	0.0800
		0.7185	0.0088	0.0908
		0.8383	0.0101	0.1005
· · · · .		0.9580	0.0110	0.1091
0.0243 0.0003		1.0778	0.0114	0.1167
0.0274 0.0003	_	1.1975	0.0114	0.1232
0.0304 0.0003		1.3173	0.0110	0.1285
0.0335 0.0003		1.4371	0.0102	0.1329
0.0365 0.0003		1.5568	0.0090	0.1362
0.0395 0.0003	_	1.6766	0.0074	0.1385
0.0426 0.000		1.7963	0.0055	0.1399
0.0456 0.000		1.9161		0.1403
0.0487 0.000		2.0358		0.1397
0.0517 0.0000	_	2.1556		0.1381
0.0548 -0.000		2.2753		0.1352
0.0578 -0.000		2.3951	_	0.1310
0.0608 -0.000		2.5149		0.1256
0.0639 -0.000		2.6346		0.1189
		2.7544		0.1110
0.0700 -0.000		2.8741		
0.0730 -0.000		2.9939		
0.0760 -0.000		3.1136		
0.0791 -0.000		3.2334	_	
0.0821 -0.000		3.3531		
		3.4729		
		3.5927		
		3.7064	-0.0056	
0.0941 -0.000 0.0943 -0.000	_	3-7124	-0.0055	0.0056
0.0943 -0.000	7. 7.003.	34.14		
RADIUS (METERS)	= 0.3125	RADIUS		(S) = 12.3050
CHORD (METERS)			(INCHE	S) = 3.7124
ZCSL (METERS)			(INCHE	5) = 1.8857
YCSL (METERS)	= -0.0013	YCSL	(INCHE	(5) = -0.0411
RLE (METERS	=0.000241		(INCHÉ	$(5) = 0.009^{5}$
HTE (METERS)	=0.000140	ATE .	LINCHS	(S) = 0.0055
X-AREA (SU-METE	351=0.000233	X-ARFA	150. IN	1.) = 0.3608
GAMMA-CHORD (RAI	0.8825		-CHORDIDE	G_{\bullet})= 50.56

TABLE B-17 C. 1

METERS			INCHES		
zc	YP	YS	zc	YP	YS
0.0	-0.0002	0.0002	0.0	-0.0090	0.0091
	-0.0002	0.0003			0.0100
	-0.0002	0.0005		-0.0082	0.0215
	-0.0002	0.0008			0.0332
	-0.0002	0.0011		-0.0070	0.0442
	-0.0002	0.0014		-0.0067	0.0543
	-0.0002	0.0016	0.6108	-0.0065	0.0636
0.0186	-0.0002	0.0018	0.7330	-0.0065	0.0722
J.0217	-0.0002	0.0020	0.8551	-0.0066	0.0800
0.0248	-0.0002	0.0022	0.9773	-0.0068	0.0870
0.0279	-0.0002	0.0024	1.0995	-0.0071	0~0933
0.0310	-0.0002	0.0025	1.2216	-0.0075	0.0988
0.0341	-0.0002	0.0026		-0.0080	0.1036
	-0.0002	0.0027		-0.0085	0.1078
0.0403	-0.0002	0.0028		-0.0092	0.1112
	-0.0002	0.0029		-0.0098	0.1140
	-0.0003	0.0029		-0.0104	0.1161
	-0.0003	0.0030		-0.0110	0.1177
	-0.0003	0.0030		-0.0115	0.1187
	-0.0003	0.0030		-0.0119	0.1191
0.0590		0.0030	2.3211		0.1184
0.0621	-0.0003	0.0030		-0.0126	0.1163
	-0.0003	0.0029		-0.0127	0.1129
	-0.0003	0.0027		-0.0128	0.1080
	-0.0003	0.0026		-0.0127	0.1018
	-0.0003	0.0024		-0.0124	0.0943 0.0854
	-0.0003	0.0022	3.0541 3.1763		0.0753
	-0.0003	0.0019 0.0016		-0.0105	0.0638
	-0.0003 -0.0002	0.0013		-0.0095	0.0510
	-0.0002	0.0009	3.5428		0.0370
0.0400	-0.0002	0.0006	3.6649		0.0217
	-0.0001	0.0003	3.7816		0.0060
		0.0001		-0.0051	
0.0702	0.0001	0.0001	30.012	0.0031	000072
RADIUS (METERS)	= 0.3295	RADIUS	(INCHES	= 12.9722
CHORD (METERS)	= 0.0962	CHORD	(INCHES	= 3.7871
		= 0.0484			= 1.9053
		= -0.0016			=-0.0616
		=0.000244) = 0.0096
		=0.000127			
		=0.000224			
GAMMA-CH	ORD(RAD.)	= 0.9442	GAMMA-	CHORDIDEG	.) = 54.10

TABLE B-18

METERS		INC	HES	
ZC YP	YS	zc	YP	YS
0.0 -0.0002	0.0002		.0093	0.0091
0.0002 -0.0002	0.0002		.0095	0.0174
0.0032 -0.0003	0.0004	0.1255 -0	-0115	0.0252
0.0064 -0.0003	0.0006		.0136	0.0325
0.0096 -0.0004	0.0008	0.3766 -0	•U177	0.0393
0.0128 -0.0004	0.0010	0.5022 -0	.0172	0.0455
0.0159 -0.0005	0.0012	0.6277 -0	-0140	0.0512
0.0191 -0.0005	0.0013	0.7533 -0	.0208	0.0564
0.0223 -0.0006	0.0014		.0225	0.0612
0.0255 -0.0006	0.0016		.0241	0.0655
0.0287 -0.0006	0.0017		.0255	
0.0319 -0.0007	0.0018	1.2555 -0	0.0270	0.0693
0.0351 -0.0007	0.0018		.0281	0.0727 0.0758
0.0383 -0.0007	0.0019		0.0288	0.0785
0.0415 -0.0008	0.0020		0.0296	0.0703
0.0446 -0.0008	0.0021		0.0301	0.0828
0.0478 -0.0008	0.0021		0.0300	0.0846
0.0510 -0.0008	0.0021		0.0298	
0.0542 -0.0007	0.0022		0.0293	0.0861
0.0574 -0.0007	0.0022		0.0286	0.0873 0.0883
0.0606 -0.0007	0.0022		0.0274	
0.0638 -0.0007	0.0022		0.0259	0.0882
0.0670 -0.0006	0.0022		0.0246	0.0869
0.0702 -0.0906	0.0021		0.0232	0.0843
0.0733 -0.0006	0.0020	2.8877 -	0.0217	0.0804
0.0765 -0.0005	0.0019		0.0201	0.0752
0.0797 -0.0005	0.0017	3.1388 -	0.0183	0.0688
0.0829 -0.0004	0.0016		0.0164	
0.0861 -0.0004	0.0013		0.0143	
0.0893 -0.0003	0.0011	3.5154 -	0.0120	0.0423 0.0311
0.0925 -0.0002	8000.0		0.0097	_
0.0957 -0.0002		3.7665 -	-0.0074	
0.0987 -0.0001	0.0001	3.8870 -	-0 -0047	0.0054
0.0989 -0.0001	0.0001	3.8921 -	-0.0040	0.30-7
		0.405116	ITNCHE	(S) = 13.9709
RADIUS (METERS)	= 0.3549	RADIUS	(TACHE	5) = 3.8921
CHORD (METERS)	= 0.0989	CHORD	THE	(S) = 1.9327
ZCSL (METERS)	= 0.0491	ZCSL	THOME	S) = -0.0908
YCSL (METERS)	= -0.0023	4 C 2 F	1 T NIC 14	S) = 0.0095
	=0.000241	KLE	1.14044	S) = 0.0041
RTF (METERS)	=0.000104	KIE	TENDERS	(0.3213)
X-ARFALSO METER	S) = 0.000207	X-AKEA	7000101 134 - 1	G.)= 58.59
GAMMA-CHORDIRAD	.)= 1.0226	GAMMA-U	HUKUIU	-G • I = J. • J

			MET	TER:	S					IN	CHE	S					
	zc		Y	/P		YS		ZC	;		YF	•			YS		
	0.0	-	-0.0	0002	2 0	•00	02	0.0		-0	• 00	92	•	0.	00	91	
	0.000	2 -	-0.0	000	2 0	.00	02	0.00	95					0.			
	0.003	3 -	-0.0	004		.00		0.12						0.			
	0.006	5 -	-0.0	000		-00		0.25						0.			
	0.009	8 -	-0.0	000	7 0	-00	04	0.38			-02			0.			
	0.013	1 -	-0.0	000	9 0	-00	04	0.51						0.			
	0.015	3 -	-0.0	010		.00		0.64						0.			
	0.019	6 -	-0.0	01	L O	.00	05	0.77						0.			
	0.022	9 -	-0.0	012	2 0	.00	05	0.90						0.			
	0.026	2 -	-0.0	013	3 0	•00	06	1.02						0.			
	0.029	4 -	-0.0	014	• 0	.00	06	1.15						0.			
	0.032	7 -	-0.0	019		-00		1.28						0.			
	0.036	0 -	-0.0	015	5 0	. 00	07	1.41						0.			
	0.039	2 -	-0.0	016	• 0	-00	07	1.54						0.			
	0.042	5 -	-0.0	016	5 0	.00	80	1.67			. 06			0.			
	0.045	8 -	-0.0	016	5 0	-00	80	1.80						0.			
	0.049	0 -	-0.0	016	0	-00	09	1.93						0.			
	0.052	3 -	-0.0	015	0	•00	10	2.05						0.			
	0.055	6 -	-0.0	015	0.	.00	10	2.18	79					0.			
	0.058	8 -	-0.0	014	• 0	-00	11	2.31						0.			
	0.062					.00	13	2.44	-53	-0	.05	04	,	0.	044	92	
	0.065					•00	14	2.57	740	-0	-04	53		0.	05	35	
	0.068					•00	14	2.70	27	- 0	• 03	99		0.	956	58	
	0.071					-00	15	2.83	14	- 0	.03	49)	0.	058	97	
	0.075					•00	15	2.96	01	-0	• 03	100	ŀ	0.	05	91	
	0.079					-00	15	3.08	88	- 0	-02	55		0.	05	79	
	0.081					. 00	14	3.21	.75	-0	. 02	12		0.	35	52	
	0.085					-00	13	3.34	-62	-0	.01	73		0.) 5(80	
	0.088					•00	11	3.47	749	-0	-01	37		0.	044	48	
	0.091					•00	09	3.60	36	-0	-01	06		0 - 0	3.	72	
	0.094					•00	07	3.73	23	-0	-00	78		0.	021	79	
	0.098		-0.0			•00		3.86	10	-0	.00	58		0 . 1	016	57	
	0.101		-0.0			.00		3.98	55	-0	. OO	39		0 .	004	45	
	0.101	3 -	-0.0	001	. 0	.00	01	3.98	97	-0	• 00	38		0.	004	+1	
	DIUS	/ ME	TEP	()	_	^	בחפג	O A (% ?	uc	, .	T N 1 ~	uc	٠,	_	•	_	
	10KD							R AŬ Î									
	SL							CHOR									
	SL							ZCSL									558
	. E							YCSL									
	ΓE							RLE									
	-APEA(R TE	EA	100	I INU 1	TA	31	=	0	• ()	U41
. /	AMM A-C	HUB	U L D	AD	. 1 = -	1 1	154	~ ~ = K	CA Nace	136	4 •	D.L.	• 1	=	0.	• 2	e / /
_				~ U 4	, , –		ムノマ	SAME	「MTし	יי אַרוי.		UE		,=	0.3	5 • '	√ 1

	METERS			INCHES	
zc	YP	YS	ZC	YP	YS
0.0	-0.0002	0.0002	0.0	-0.0092	0.0091
	-0.0002	0.0002		-0.0098	0.0090
	-0.0005	0.0002	0.1311		0.0079
	-0.0007	0.0002		-0.0264	0.0068
	-0.0009	0.0002	0.3933		0.0061
	-0.0010	0.0001		-0.0499	0.0056
	-0.0012	0.0001	0.6555	-0.0471	0.0054
	-0.0013	0.0001	0.7866	-0.0525	0.0054
0.0233	-0.0015	0.0001	0.9177		0.0058
	-0.0016	0.0002	1.0488		0.0066
	-0.0016	0.0002		-0.0641	0.0077
0.0333	-0.0017	0.0002		-0.0663	0.0093
0.0366	-0.0017	0.0003	1.4421		0.0112
0.0400	-0.0017	0.0003		-0.0682	0.0136
	-0.0017	0.0004		-0.0677	0.0155
	-0.0017	0.0005		-0.0664	0.0199
	-0.0016	0.0006		-0.0641	0.0238
	-0.0015	0.0007		-0.0607	0.0283
	-0.0014	0.0008		-0.0564	0.0333
	-0.0013	0.0010		-0.0510	0.0393
	-0.0011	0.0012	2.4909		0.0460 0.0529
	-0.0009	0.0013	2.6220		0.0529
	-0.0007	0.0015	2.7531		0.0637
	-0.0006	0.0016	2.8842	-0.0162	0.0660
	-0.0004	0.0017		-0.0111	0.0661
	-0.0003	0.0017 0.0016	3.2775	the second secon	0.0639
	2 -0.0002	0.0015	3.4087		0.0595
	9 -0.0001	0.0013		-0.0020	0.0529
	2 -0.0000	0.0011		-0.0009	0.0440
	5 -0.0000	0.0008	3.8020		0.0329
	9 -0.0000	0.0005	3.9331		0.0196
	1 -0.0001	0.0001	4.0601		0.0045
		0.0001		-0.0037	0.0040
00103.					
RADIUS	(METERS)	= 0.3977	RADIUS		S) = 15.6572
	(METERS)		CHORD		S) = 4.0642
ZCSL	(METERS)	= 0.0505	ZCSL	(INCHE	S) = 1.9877
YCSL	(METERS)	= -0.0033	YCSL	(INCHE	s) = -0.1304
RLE	(METERS)	=0.000236			S) = 0.0093
RTE	(METERS)	=0.000104			S) = 0.0041
X-AREA(SQ.METERS)=0.000173			0.2675
GAMMA-C	HORD (RAD.)= 1.1675	GAMMA-	-CHURD(DE	G.)= 66.89

METERS			INCHES	
ZC YP	Y S	zc	YP	YS
0.0 -0.0002 0.0002 -0.0002 0.0033 -0.0005 0.0067 -0.0007	0.0002 0.0002 0.0002 0.0001	0.0093 0.1318	-0.0091 -0.0098 -0.0185 -0.0272	0.0090 0.0089 0.0071 0.0053
0.0100 -0.0009 0.0134 -0.0011 0.0167 -0.0012 0.0201 -0.0014 0.0234 -0.0015	0.0001 0.0001 0.0001 0.0000 0.0001	0.3953 0.5271 0.6585 0.7906	-0.0352 -0.0424 -0.0488 -0.0544 -0.0591	0.0039 0.0029 0.0022 0.0019 0.0021
0.0268 -0.0016 0.0301 -0.0017 0.0335 -0.0017 0.0368 -0.0018 0.0403 -0.0018	0.0001 0.0001 0.0001 0.0002	1.0541 1.1859 1.3176 1.4494	-0.0630 -0.0661 -0.0683 -0.0695 -0.0699	0.0026 0.0036 0.0050 0.0070 0.0094
0.0435 -0.0018 0.0469 -0.0017 0.0502 -0.0017 0.0535 -0.0016 0.0569 -0.0014	0.0003 0.0004 0.0005 0.0006 0.0008	1.7129 1.8447 1.9764 2.1082	-0.0693 -0.0677 -0.0651 -0.0615 -0.0569	0.0124 0.0160 0.0201 0.0249 0.0303
0.0602 -0.0013 0.0536 -0.0011 0.0669 -0.0009 0.0703 -0.0007 0.0736 -0.0005	0.0009 0.0011 0.0013 0.0015 0.0016	2.3717 2.5035 2.5353 2.7670 2.8988	-0.0513 -0.0439 -0.0360 -0.0281 -0.0207	0.0367 0.0437 0.0509 0.0581 0.0631
0.0770 -0.0004 0.0803 -0.0002 0.0837 -0.0001 0.0870 -0.0001 0.0904 -0.0000 0.0937 0.0000	0.0017 0.0017 0.0016 0.0015 0.0014 0.0011	3.0306 3.1623 3.2941 3.4258 3.5576 3.6894	-0.0145 -0.0093 -0.0051 -0.0021 -0.0001 0.0008	0.0658 0.0662 0.0644 0.0602 0.0538 0.0450
0.0971 0.0000 0.1004 -0.0000 0.1036 -0.0001	0.0009 0.0005	3.8211 3.9529 4.0807	0.0005 -0.0009	0.0338 0.0203 0.0045
RADIUS (METERS) CHORD (METERS) ZCSL (METERS) YCSL (METERS) RLE (METERS) RTE (METERS)	= 0.1038 = 0.0507 = -0.0034 =0.000236 =0.000104	CHORD ZCSL YCSL RLE RTE	(INCHES (INCHES (INCHES (INCHES) =15.8554) = 4.0847) = 1.9973) =-0.1329) = 0.0093) = 0.0041
X-AREA(SQ.METERS) GAMMA-CHORD(RAD.)				0.2620 0.5620

TABLE B-22

	METERS			INCHES	
zc	YP	YS	zc	YP	Y S
0.0	-0.0002	0.0002	0.0	-0.0091	0.0089
	-0.0002	0.0002		-0.0098	0.0098
	-0.0005	0.0002		-0.0190	0.0062
	-0.0007	0.0001		-0.0281	0.0038
	-0.0009	0.0000			0.0018
	-0.0011	0.000	0.5295	-0.0439	0.0003
	-0.0013		0.6619	-0.0505	-0.0008
0.0202	-0.0014		0.7943	-0.0562	-0.0015
	-0.0016			-0.0611	-0.0016
	-0.0017			-0.0651	-0.0013
	-0.0017	-0.0000		-0.0682	
0.0336	-0.0018	0.0000		-0.0703	0.0008
0.0370	-0.0018	0.0001	1.4562		0.0027
	-0.0018	0.0001		-0.0718	0.0052
	-0.0018	0.0002		-0.0711	0.0083
	-0.0018	0.0003		-0.0694	
	-0.0017	0.0004		-0.0666	
	-0.0016	0.0005		-0.0628 -0.0579	
	-0.0015	0.0007		-0.0520	0.336
	-0.0013	0.0009 0.0010		-0.0444	
	-0.0011 -0.0009			-0.0361	0. 485
	-0.0007			-0.0279	0.0562
	-0.0005			-0.0201	0.0618
	-0.0003		3.0448		0.0651
	-0.0002		3.1772		0.0659
0.0841			3.3096		0.0644
	-0.0000		3.4420	-0.0007	
0.0908			3.5744	0.0012	0.0542
0.0942		0.0012	3.7067		
0.0975		0.0009	3.8391		
0.1009	-0.0000	0.0005	3.9715		
	-0.3001	0.3001	4.0998	-0.0037	0.0046
0.1042	-0.0001	0.0001	4.1039	-0.0038	0.0041
0.407115 /	METERCI	= 0.4078	RADIUS	LINCHE	5) = 16.0534
CHORD (CHORD		
7CC1 /	METERSI	= 0.0510			S1 = 2.0064
703F (METERS)	= -0.0034		LINCHE	
RIF	METERS	=0.000236			5) = 0.0093
RTF (METERS)	=0.000104			SI = 0.0041
)=0.000166	X-AREA	(SO. IN	-1 = 0.2568
GAMMA-CH	ORD (RAD.)= 1.1928	GAMMA-	CHORDIDE	G.) = 68.34

Or Poor Contract

APPENDIX C

PART 1

STEADY BLADE STRUCTURAL DATA

BLADE LUCAL UNTWIST IN DEGREES (MIRROR MEASUREMENTS)

TABLE C-1

Grand Comment

Percent Chord Percent Measured Span Percent Design Speed From Lead-Measured 85 82 73_ ing Edge 54_ From Hub 5 0.57 1.03 95 1.15 1.28 0.92 25 0.54 1.01 0.33 0.71 0.42 50 0.78 38.0 1.52 70 0.33 0.80 1.04 1.13 5 0.47 30 0.90 0.53 0.42 0.72 25 9 0.81 50 0.39 0.64 0.37 0.79 70 0.38 0.52 0.78 0.71 5 0.57 0.35 75 25 0.68 0.52 0.26 0.45 50 0.00 0 0 5 0 66 0.21 0.09 0.11 0.12 25 0.72 0.66 0.51 5 0.32 55 0.39 0.36 0.29 25 0.19 0.11 0.09 0.11 50 0.04 5 47 0.33 0.40 25 5 0.5* 38 -0.13-0.05 0 0 20 25 25 35 0.33 0.90 0.71 0.43 25 Θú 0.52 0.58 0.25 0.51 76 50 0.0€ 0.09 J.J6 25 0.03 á6

^{*}Questionable data.

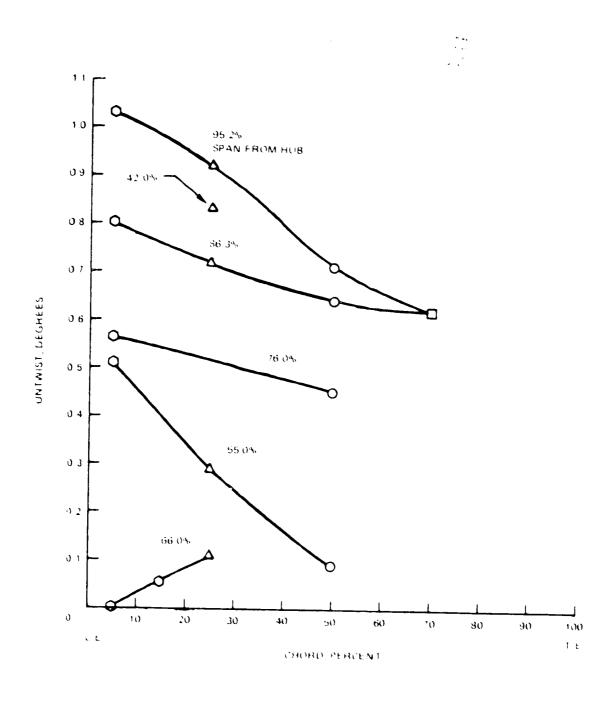


Figure C-1 "easured Untwist for TS22 Fan Blade as a Function of Chord at "3 Percent Speed"

OF HOOR WAR TO

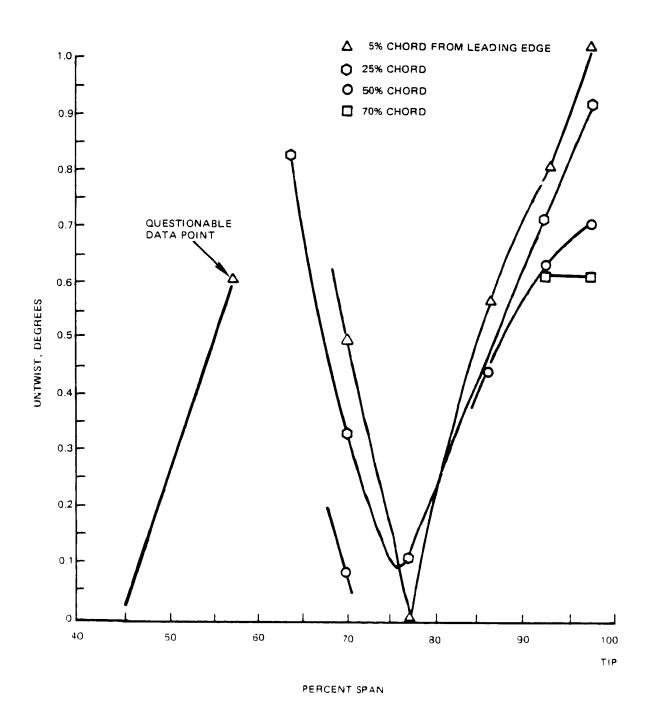


Figure C-2 Measured Untwist for TS22 Fan Blade at 73 Percent Speed Relative to Untwist at 25.4 Percent Speed



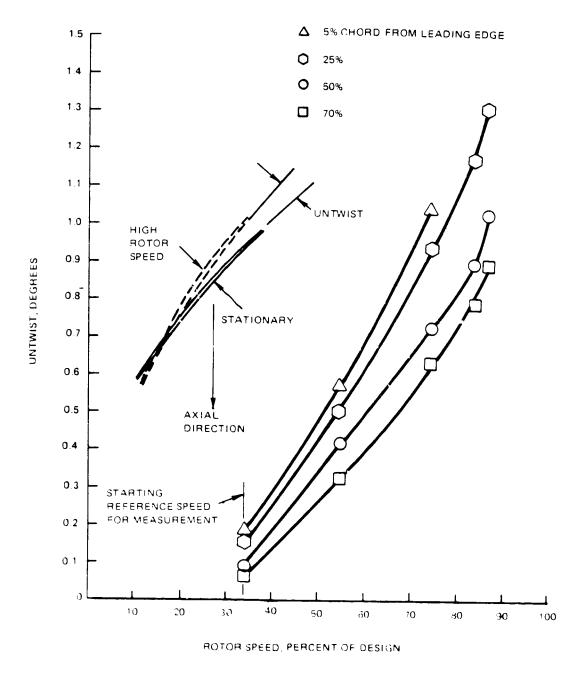


Figure C-3 Measured Untwist for TS22 Fan Blade as a Function of Rotor Speed at 95 Percent Span

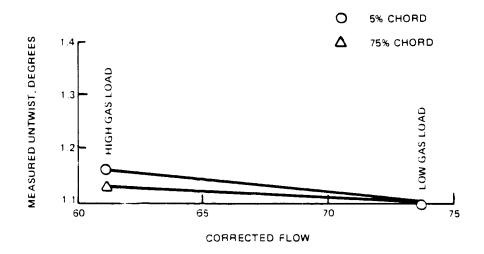
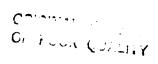
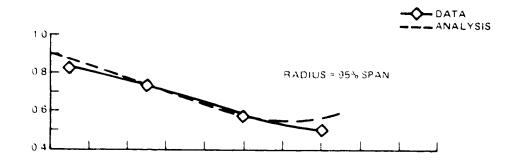
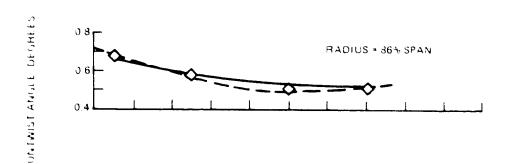


Figure C-4 Measured Untwist for TS22 Fan Blade as a Function of Chord at 73 Percent Speed







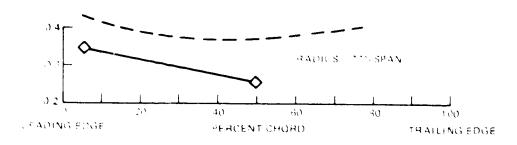


Figure C-5 Measured Untwist for TS22 Fan Blade and Predicted by NASTRAN Analysis for Rotor Speed at 65 Percent Speed

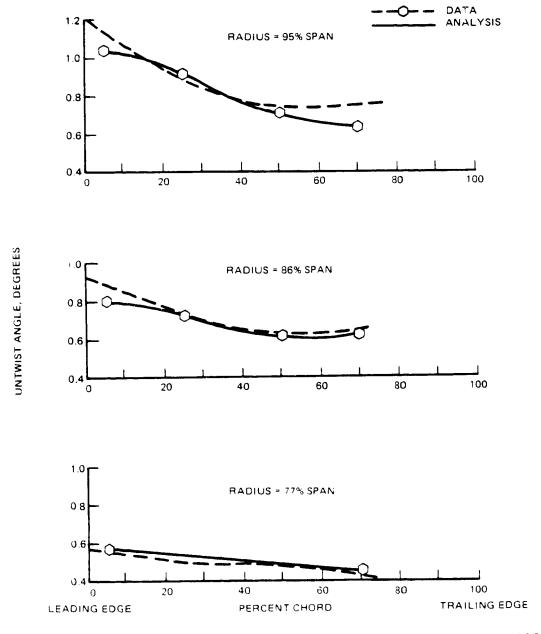
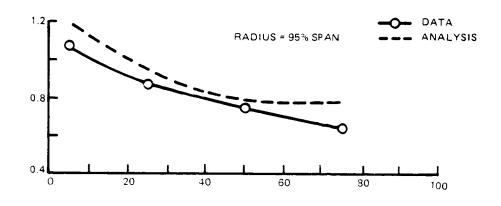
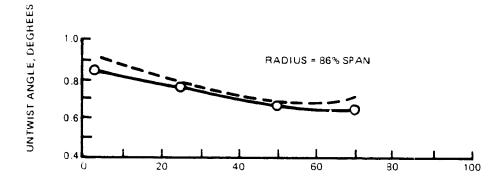


Figure C-6 Measured Untwist for TS22 Fan Blade and Predicted by NASTRAN Analysis for Rotor Speed at 73 Percent Speed





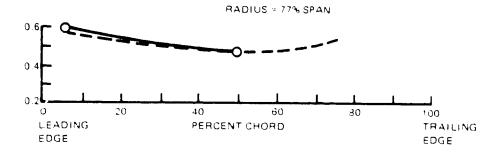
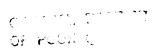


Figure C-7 Measured Untwist for TS22 Fan Blade and Predicted by NASTRAN Analysis for Rotor Speed at 75 Percent Speed



APPENDIX C

PART 2

UNSTEADY BLADE STRUCTURAL DATA

PROCEDING PAGE BLOOK NOT FILLED

TABLE C-2
STRAIR GAGE AMPLITUDE AND PHASES

Speed (Percen Frequency (Hz		67 619			72 €38			75 638	
Blade Position	(N/cm ²)	itress (lbf/in)	Phase Relative to Blade Number 3 (Degrees)	(N/cm²)	Stress (lbf/in ²)	Phase Relative to Blade Number 3 (Degrees)	S (N/cm ²)	(lbf/in ²)	Phase Relative to Blade Number 3 (Degrees)
1 2 3 4 5	2,275 2,482 2,068 2,068 2,068	3,300 3,600 3,000 3,000 3,000	123 0 280 248	2,275 2,620 2,068 2,895 2,482	3,300 3,800 3,000 4,200 3,600	97 70 0 283 255	1,723 2,275 1,723 1,585 1,585	2,500 3,300 2,500 2,300 2,300	120 0 290 251
6 7 8 9 10	965 1,103 1,241 1,034 689	1,400 1,600 1,800 1,500 1,000	99 128 102 164 42	1,034 1,378 1,310 1,241 965	1,500 2,000 1,900 1,800 1,400	90 117 94 155 32	827 1,103 896 1,103 689	1,200 1,600 1,300 1,600 1,000	104 148 120 182 49
11 12 13 14 15	689 344 413 551 413	1,000 500 600 800 600	42 22 336 255 264	551 344 344 551 551	800 500 500 800 800	31 32 347 280 272	482 344 413 551 551	700 500 600 800 800	55 50 47 295 270
16 17 18 19 20	482 551 551 482	700 800 800 700	258 278 204 126	689 827 1,034 827 896	1,000 1,200 1,500 1,200 1,300	256 271 240 204 138	482 482 413 482 827	700 700 600 700 1,200	267 291 254 200 153
21 22 23 24 25	827 827 413 551 551	1,200 1,200 600 800 800	94 69 318 264 113	1,516 1,241 551 620 344	2,200 1,800 800 900 500	82 56 316 235 101	965 827 896 896 827	1,400 1,200 1,300 1,300 1,200	130 88 25 343 244
26 27 28 29 30	551 275 551 413	800 400 800 600	107 318 301 287	413 344 551 827	600 500 800 1,200	188 270 287 267	344 482 965	- 500 700 1,400	128 328 299 278
31 32	137	200	321 202	1,172 965	1,700 1,400	261 19 4	1,172 965	1,700 1,400	334 203

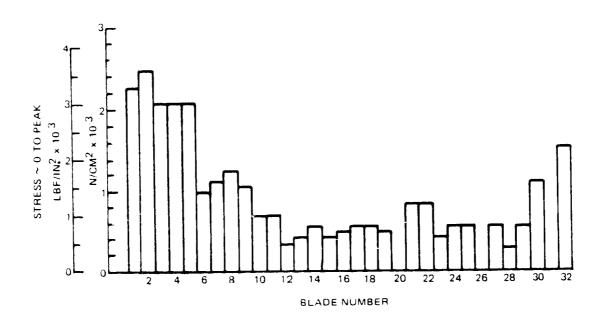


Figure C-8 Blade Flutter Amplitude for TS22 Rotor at 67 Percent Speed From Strain-Gage Measurements



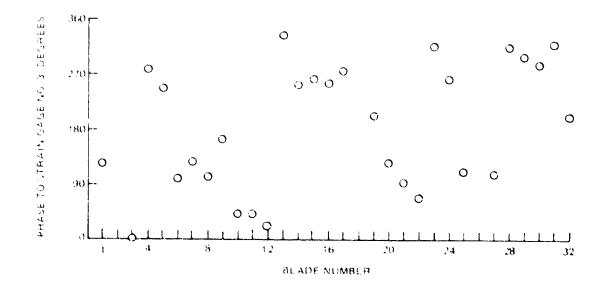
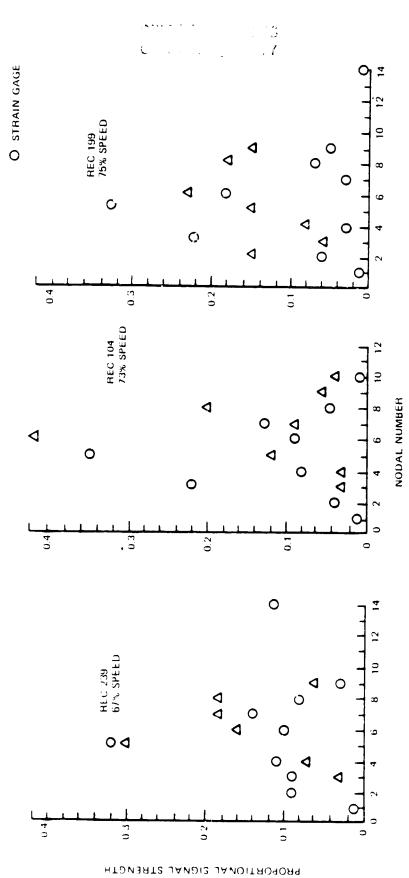


Figure C-9 Peripheral distribution of Blade Strain-Gage Angles in Flutter at 519 Hz. 67 Percent Speed



FROM LEADING EDGE)

△ KULITE (73% CHORD

Figure C-10 Spectral Comparison of Wibratory Rotor Pressure Amplitudes in Terms of Distribution Among Spatial Harmonics

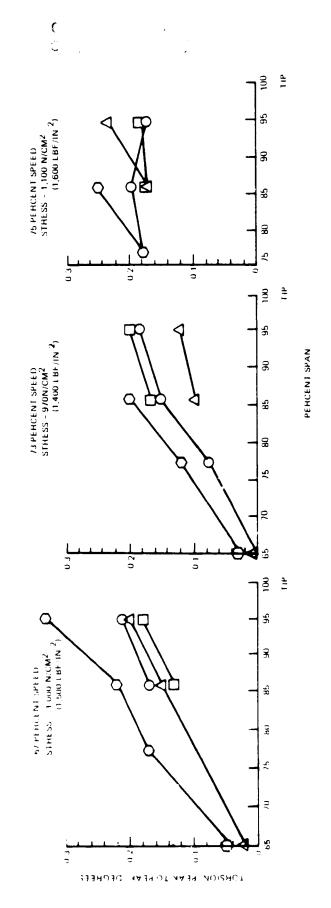
TABLE C-3

BLADE AMPLITUDE IN FLUTTER

(Measured From Mirrors From Still Photographs)

			67_Per	cent Speed	73 Per	cent Speed	75 Per	cent Speed
Blade Number	Percent Span	Percent Chord	Peak- to-Peak Torsion (Degrees)	Peak-to-Peak Axial Component Bending Slope (Degrees)	Peak- to-Peak Torsion (Degrees)	Peak-to-Peak Axial Component Bending Slope (Degrees)	Peak- to-Peak Torsion (Degrees)	Peak-to-Peak Axial Component Bending Slope (Degrees)
9	95	5 25 50 70	0.33 0.20 0.21 0.18	0.23 0.35 0.40 0.50	0.12 0.18 0.20	0.46 0.59 0.53	0.23 0.17 0.18	0.28 0.26 0.26
	86	5 25 50 70	0.22 0.15 0.17* 0.13	0.25 0.21 0.30 0.30	0.20 0.10 0.15 0.17	0.50 0.28 0.45 0.43	0.25 0.17 0.20 0.17	0.30 0.17 0.17 0.11
	76	5 50	0.17 0.17	0.18 0.21	C.12 O.08	0.43 0.25	0.18 0.18	0.2 0.2
	6 6	5 2 5	0.05 0.02	-	0.03 0	•	0.07 0.08	0.15
	55	5 25 50	- -	- - -	- -	: :	0.05 0.05 0.05	0.06 0.05 0.10
	47	25	-	-	-	-	0.03	0.10
	38	5	-	-	•	-	0.10	0.17
	20	5	-	-	-	-	0.05	0.08
3	86	50	0.44	0.48	0.54	0.69	0.24	0.40
4	86	50	0.50*	0.53	0.53	0.55	0.14	C.23
2	76	50	0.58	0.55	0.43	0.63	0.24	0.40
5	6 6	25	0.21	0.17	0.17	0.23	0.10	0.17

 $[\]star$ Relative to strain gages 4 and 9



О 5% СНОНЫ Д 25% СНОНЫ О 50% СНОНЫ □ 70% СНОНЫ

Radial Distribution of Vibratory Torsion Component in Flutter Measured by Mirrors; Still Pictures Used to Reduce Data Figure C-11

TABLE C-4

BLADE AMPLITUDE AND PHASE DEFLECTIONS DETERMINED FROM MIRRORS (Reduced from High Speed Movies)

Blade Number	Location Percent Span	Percent Chord	Bending Phase (Degrees)	Torsional Phase (Degrees)	Bending - Torsion Phase Angle (Degrees)
65% Speed					
9 9 9 9 3 4 9 9 2 5	95 95 95 86 86 86 87 77 77 77	25 50 70 25 50 50 50 50 50 50	41.1 -12.1 -72.6 31.9 0 -72.7 19.3 63.6 -0.3 49.4 -95.3	26.6 0.50 -28.9 36.3 0 65.9 -59.9 69.6 9.4 -18.4 -86.2	45.2 14.2 -8.9 25.1 31.8 -106.8 113.8 23.5 24.1 103.2 25.5
73% Speed					
9 9 9 9 4 9 2 5	95 95 95 86 86 86 86 77 77	25 50 70 25 50 50 70 5 50 25	-20.5 -6.1 8.8 -22.3 0 -125.8 14.4 -24.5 6.5 2.6	1.0 20.9 28.7 2.1 -99 34.6 -23 35 -19.2	-86 -91.9 -84.8 -89.0 -64.9 -97.8 -85 -66.6 -93.4 -76.2
75% Speed					
9 9 9 9 9 9 9 9 9 9 9 2 5	95 95 95 86 86 86 86 86 77 77 77	25 50 70 5 25 50 50 70 5 50 50 25	-5.9 0.4 2.0 4.2 0.7 0 -2.6 -6.6 -1.7 5.9 -5.5 -14.8 134.5	15.3 23.1 14.5 44.2 22.9 0 -117.0 -103.7 18.6 56.9 28.2 54.0 -115.2	-45.7 -41.1 -30.9 -67.0 -48.7 -15.0 99.8 31.9 -40.4 -101.1 -52.0 -83.3 -16.8

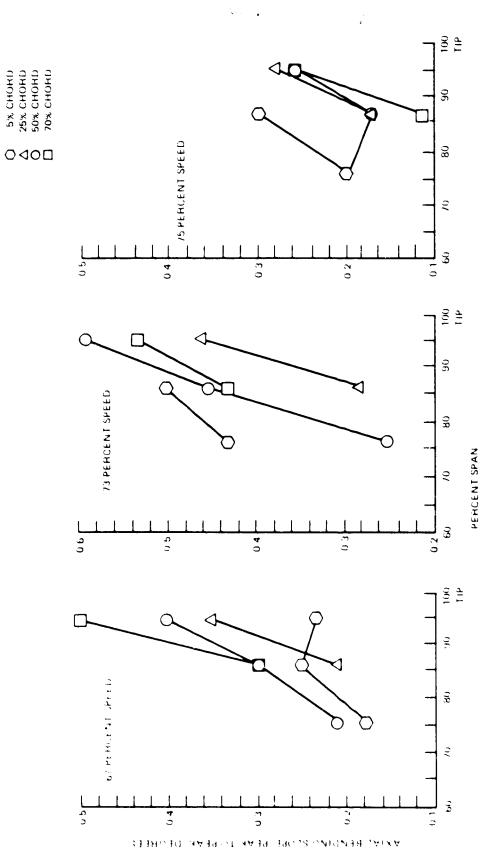
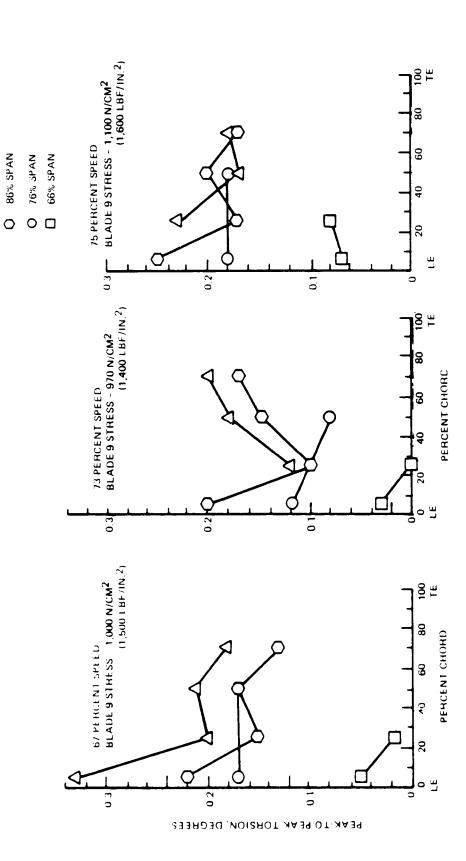


Figure C-12 Radial Distribution of Vibratory Bending Slope Amplitude in Flutter (Mirror Data; Still Pictures)



Chordwise Variation of Vibratory Torsional Amplitudes in Flutter (Mirror Data) Figure C-13

95% SPAN FROM HUB

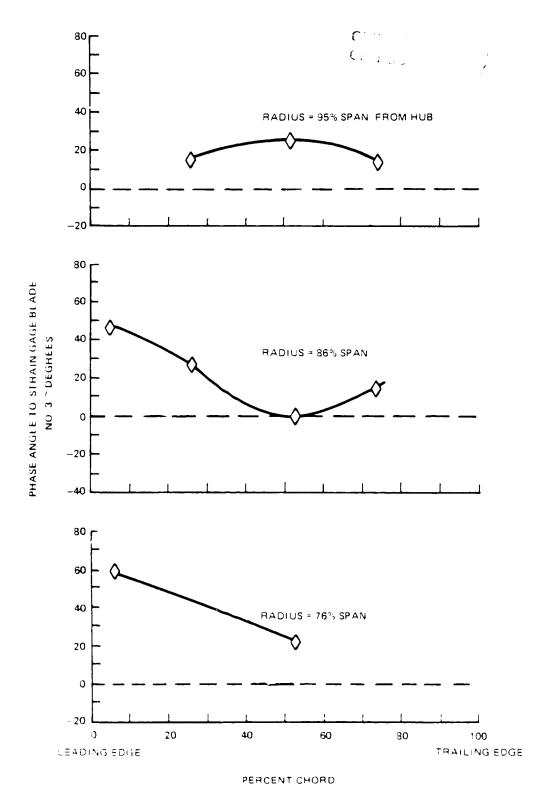


Figure C-14 Vibratory Phase of Torsional Deflection at 75 Percent Speed

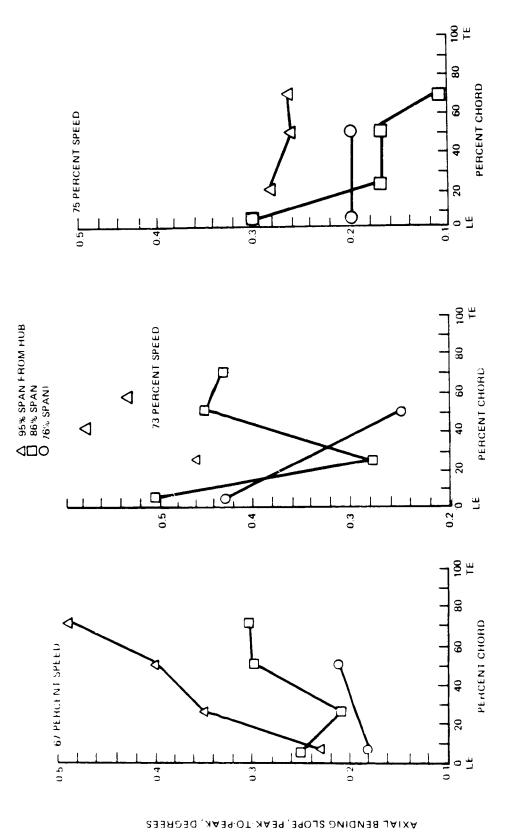


Figure C-15 Chordwise Variation of Vibratory Axial Bending Axial Bending Slope in Flutter

Communication of the Communica

APPENDIX D

PART 1

STEADY PRESSURE

NOTE: On the following tables, "Tangential" data represents the angular displacement on the rotor. Pressure data represents static pressure.

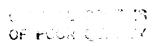


TABLE D-1

STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS

55% SPEED

RECORD 247

Inlet Total Pressure = $90,400 \text{ N/m}^2 \text{ (1888 lbf/ft}^2\text{)}$

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
-55.4	0.962
-15.1 - 3.6	0.962 0.971
9.4	0.964
22.2 34.6	1.004 1.029
47.5	1.041
73.4 99.3	1.053 1.063
141.4	1.065

RECORD 247 WALL KULITE STFADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 98.8 PILOPASCALS = 14.31 PSI

	<u>Carorrer</u>	
22.2 PRESSURC 92.1 92.1 92.1 92.1 92.3 92.8 92.8 92.8 92.8 93.2 93.2	2 4 4 4 4 8 8 8 8 8 8 4 6 4 4 4 4 4 4 4 4	25:11444366
# CHURD= TANGENTIAL (DEG. P. 137.6 - 137.6 - 135.6 - 135.6 - 135.6 - 135.7 - 1	1.22.4.2.2.4.2.2.4.2.2.4.2.2.4.2.2.4.2.2.4.2.2.4.2.2.4.2.2.4.2	20 - 2 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1
PRESSORE 91.9 91.9 94.3 94.3 96.1 96.1 13.5 13.5 13.5 91.2 91.2		986.33 987.5 99.5 99.5 99.5 99.5 99.5 99.5 99.5 9
	こうしょうしゅうしゅう りょうしゅうしょうしゅう	111111111 60.000000000000000000000000000
EMAXIMUM PRESSURE 94.6 94.6 95.4 97.4 97.4 97.4 97.4 97.6 97.6 97.6 91.1 91.1 91.1	995-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	887.1 997.4 997.4 997.4 997.8 997.8 997.8 997.9
080-	-223-1 -223-1 -223-1 -223-1 -223-1 -233-3 -113-3 -23-3 -113-3	11111111 1111111111111111111111111111
-15.1 PAK S S URE 94.2 94.2 94.2 94.2 94.2 96.3 99.6 99.6	ちょしゅうとりょうしゅり しょく	68 64 64 64 64 64 64 64 64 64 64 64 64 64
TANGENTIAL (DEG.)		
# CHORD= 16405011AL 10705 1070	- A R R R R R R R R R R R R R R R R R R	
A ST T ST S		. 4 5 2 F 4 5 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

	PRESSURES
TABLE 0-2 (Contd)	FCORD 2-7 MALL KULTTE STEADY STATE PRESSURES

FSSURG FSSURG	TIAL #	MAXI RESS	TANGENTAL	MAX 1/4U	TANSENTIAL	⊃	CENTTAL	SMAXIMUM	
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	ω	٠ ن	36.	_	•	7.		8° 36	
	1)	40	35.	-	-35.4	7.	•	6.94	
	3	-	•	3.16	105.0	6.16	S • FOI	2-25	
	٤	7	3		_	ಬ	- 4	5.6	
	15.	7.	30	_	•	•	•	41.1	
4777777777777	2	,	C.	7.95	٠.	50°C	-:2.2	1.15	
	. • !	ċ	31.		٠	۲.		47,4	
			5.	7.12	•	•	-	57.6	
200000000000000000000000000000000000000		1.76	29.	4.16	/ B	5.16	~	1.16	
44444444		45.6	•	47.2	~ .		.11	41.2	
		95.1	~				~	0.66	
				6,96			•	51.2	
2,42,42,4			u.		. 🕰			90 6	
77777			-25.0	9.16	-25.0		ω١.	7.15	
2000			•	98.1			.*	97.1	
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25.			2	95.3	(N)	•	C	97.5	
~			-		-	•	_	97.2	
			٠		-5°°-C	•		 	
7			٠,	•	-19.5	•	᠂	9.1.6	
			e.	97.2	7.31-	•	· .	9.1.6	
-17			۲.		-17.8	•	_	8.75	
-10	•		Ģ	1.96	-17.1	•	-16.9	1.16	
; ₹ -		93.3	ġ	7.95	n.	•	v٠	41.1	
			'n.	1.95	. 4 (4) (4) (•	st.	7. 2. 6	
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5 1		٠	7 • 6	2.07	- o		, a		<u>ر باد</u>
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21	•	u)	ζ.	97.2	4.5-	٠	۲۰۰۶	۲۰ <i>۱</i> ۰	
Ĩ.	•		-1.6	4.10	-1.5	٠	-	5.75	
í	•	•	•	9	٠٠٠ ١	•		\ \ \ \ \ \	
•	•	~	-:	S.	٠ <u>٠</u> ن	• زند		ا ند	
-	٠	46.8	1.1	٠ ٠	7.7	96.2	-	•	
• •	~	41.06	3.5	96.3	2.6			41.17	

San Barana and Aller

** MAXIMUM PRESSURE

CURVE CURVE

LRBEL VALUE

2 0.930000E+02

3 0.880030E+02

4 0.790000E+02

5 0.720000E+02

MAXIMUM STATIC PRESSURE 98.8 KPa (14.31 PSI)

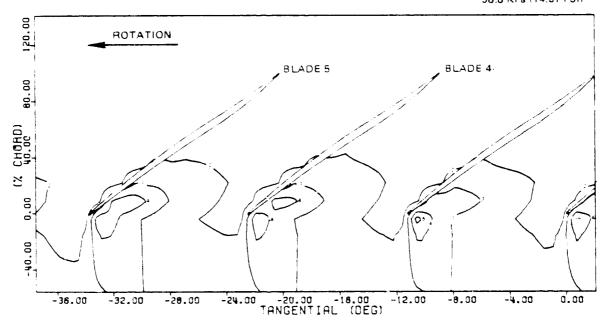


Figure 0-1 Steady State Pressure Contours at Blade Tip; But of Elutter, High Operating Line, 55 Percent Speed, 30 Percent Flow, Pressure Ratio 1.153

TABLE D-3

STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS

63% SPEED RECORD 71

Inlet Total Pressure = 83,410 N/m^2 (1742 lbf/ft^2)

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
-55.4 -15.1 - 3.6 9.4 22.2 34.6 47.5 73.4 99.3	0.935 0.941 0.958 0.949 1.002 1.018 1.020 1.019
141.4	1.038

TABLE 0-4

1.1	11.1 1.2 2.4 8 8.2 2.4 8 8.2 8 8.2 8 8.2 8 8.2 8 8.2 8 8 8 8 8 8 8 8 8
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	1

TABLE D-4 (Contd)

		Ι	RECORD 71 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 96.3 KILOPASCALS = 13.96 PSI	71 WALL URE SAMPLE	KULITE STEAD 0 = 96.3	Y STATE PR KILOPASCA	ESSURES LS = 13,96	PSI		P46£ 2
SAMPLE	# CHORD=	4.5.5	# CHURD=	-15.1	# CHCRD=	-3.6	Z CHORD=	4.6	# CHORD=	22.2
1,0749.8	17 NG FILL I AL	TMAXIM	UM TANGENTIAL T	MAX 14	IM TANGENTIAL :	UMI XAM3	M TANGENTIAL	*MAXIM	UM TANGENTIAL 3	ZMAX IMUM
	(1,66.)	PRE SSURE	(DFG.)	RESSUR	(DFG.)	PRESSUR	(DEG.)	PRESSU	(DEG.)	PRESSURE
3 4	4.6	. 1 e .	ی .	5000	١•١	63.3	2.5	65.9	2.7	93.1
6.	7.0		2.5	ີ. ເມ	1.4	63.1	2.7	67.6	3.1	7 2
, . .	4	 	(۲)		1.1	64.9	~4 • •)	61.9	G.)	E6.1
ć v	۲.,	81.0		91.8	ن• 2	67.5	3.4	6.69	0. 0.	86.6
53	1.0	٩1.1	3 • ° °	81.4	2,5	76.5	8.0	73.9	4.6	66.6
7:	٠,٠	01.1	3.1	21.3	2.P	P 2 - 4	6.3	70.7	0.4	86.1
ď	6.4	91.1	· ·	• m	3•3	1 * 7 6	4. £	7• ∂ 8	7.2	26.1
ζ;	7.7	1 - 1 6	Ð.,	30	5.1	86.1	5.3	82.9	7.6	85.7
	J. 6	91.1	6.4	82.1	7.4	39.	7.9	39.	й. У.В	35.6
σ •	9.,	9,1	£.,	82.3	9.1	1.26	6°8	4.10	5.1	31.1
30	11.3	01.1	10.1	87 . b	o.,	45.4	ア・3	44.7	6.4	89.6
4	ر ا ا		·	ur a	رد د	0 7 0	٧.	7 10	7	10

7 CHCRD= 99.3 RECOND 71 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 96.3 KILOPASCALS = 13.96 PSI \$ CHORD= 77.4 # CHORD= 47.5 \$ CHORD= 34.6

SS	ગ•6: ક	,	÷	7.0%				5	J	1.63	4.83	ر. م		•	7 C		,	٠	,	,	9: •3	•	.:	٠		\$ · · · ·	100	• 1 • 1	92	-	5	٠	ا ر د خو	•	* ·- > :	•) o o	•		۲,	5.50	Š	ě	63.6
0 Z Z	54.	74.	• : • • (-22-1	.2	7	•	•	,	-11.5	~	ġ.	• •	n a - ()	າ <i>∘</i> າ	\sim	∹	-	-10.2	1.6-	0	۰	-7.0	J • 1	Ĵ.		1.3.7	6	1-7	-7.0	-1	• -1.	•	•	, ,	۲ • ۲ • ۲ • ۲ • ۲ • ۲ • ۲ • ۲ • ۲ • ۲ •	, (5°2	•		**	4.5	.,
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5 × × × × × × × × × × × × × × × × × × ×	نڌ	ۍ ت	• •	E 0	n m	(F)	6	2.	α,	⊕	ě	8	ം ന (÷ ,	. a	• •	. 8	 .xo	8.	æ	æ	8	8	٠ چ	ند	<u>.</u>	F = 00	. 00	6	α; •	æ	•		o o	n a	e n c	ດ ຕ ເຄື່ອ ເຄື່ອ ເຄື່ອ	, 33	· æ	æ	ď	a :		
5. 5. 5. 5.	2,5	4	24	<i>ز ا</i> د	-23.1	2 2	2 2	22.	2.1	-21	50	1.,	\$ (• د ت	-14.5	: ;	•	9.1	S.		,	13.	3	.:	CT.	12.	-12-1			÷	9 · 4 -	œ1	ς,	ġ.,	22 M	•	14.0			i di	•		7.	9•)-
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TANGEMITAL (DEG.)	8.45-	₹. • • • · · ·	1.66-	7	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	, , , , , , , , , , , , , , , , , , ,	7	- 11.¢	1 :-	1. 2-	7 · · · · · · · · · · · · · · · · · · ·	•	1. · · · · · · · · · · · · · · · · · · ·	5.7.	· • / I - I			-16.2	-14.7	-14.5	-1564	5.51-	1.2.1		-11-	-:1.3	as c	3 3 3 3 3 3 3 3 3 3	7.5-	6.1-	4.9:	6.6-	7.4	- 6 - 6 1	, , ,	7 •	· · · · · · · · · · · · · · · · · · ·	• ;	, ,	· •	12.4	. 1	•	~ ·)-
SAMPLE	•	٠,	•	 .	()				$\bar{\Lambda}$	Ĺ	Ĩ,	V		•	15		<u>ئ</u> م	ć.	7.1	;		÷.	€.	ř.	7.	e. :	er v		, r	3.3	76	4°	40 F	7.	F (÷ .	., .	; 3		1.4			17	5

RECORD 71 WALL KULITE STEADY STATE PRESSURES MAXINUM PRESSURF SAMPLED = 96.3 KILOPASCALS = 13.96 PSI

			I	MAXIAUM PRESSI	URF SAMPLED	= 96.3	KILUPASCAL	PRESSURE SAMPLED = 96.3 KILOPASLALS = 13.90 F31			
νŻ	B THE S	T CHORD = IANGERITAL	34.45 34.45 34.45	CHCRD= CHCRD= M TANGENTIAL M	47.5 EMAXIMI PRFSSUR	% CHORD= JM TANGENTIAL RE (DFG.)	73.4 TMAXIMU PKr SSUR	% CHORD# IM TANGENTIAL (F (DIG.)	99.3 TMAXIMI PRESSUR	CHORD= JM TANGENTIAL RE (DIG.)	141.4 TMAXIMUM PRI SSUME
16	Ĵ			5 - C	5	4.	p p . 3	5.2	a) - C	n s	
,4	•	7.	1.	ر • ،	23.5	5 • ::	m c m c	7.0	7 30) • • •	
	٠,١	· ·	3)	~ ` `	୍ଟ . ଫୁଟ ଫୁଟ	5.5	n c 20 0	7 · · · ·	 		
	C .	••	5. or 1.	1:1	τ.	(1 c 0 c 0 c	r .	20 3	7.7	
	53	7.4	7.60	7.6	£.8	7 ·	ກ ເ ນ ເ	;. ~ • • • •	. J	7.5	
	54	4.5	00	٥,٠	ر. هر عد	•	n 6	- ر- ع د		7 7	
	3	ر ش ا	(o ;	: • •3.	.° .°	د. ه	າ (• () • G	
	5	6.4	56.3	•	33.5	C)	5 6 20 6 30 6	υ • •	7 7 7 7	• •	
	4.7	7.1	G 9 9	Λ· τ	3.5	4.	8	n .			
	·	Ç. • 3.	2-50	30 	93.5	რ. თ	F .	ຖຸດ	-i c	• • • •	
	3	7.0	2.89	11	5.63	10.7	(1) (C) (C)	5	7.16	3 4	
	<	4.1	6.00	70.01	F.P. 5	16.5	99.3	16.5	\$ 0 \$	C • 11	

Or Food & and

% MAXIMUM PRESSURE
CURVE CURVE
LRBEL VALUE
2 0.930000E+02
3 0.8 10000E+02
4 0.790000E+02
5 0.720000E+02
8 0.650000E+02
7 0.580000E+02
8 0.510000E+02
MAXIMUM STATIC PRESSURE
96.3 KPa (13.96 PSI)

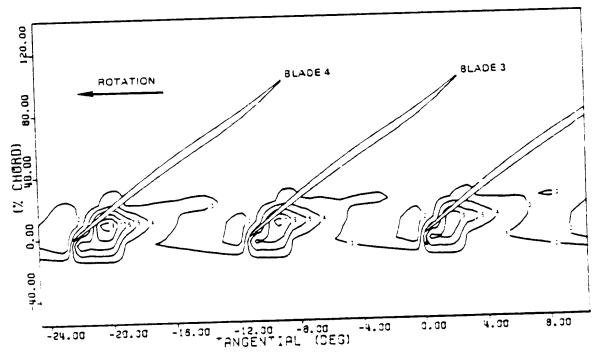


Figure D-2 Steady State Pressure Contour at Blade Tip; No Flutter, Low Operating Line, 63 Percent Speed, 65.8 Percent Flow, Pressure Ratio 1.1776

TABLE D-5

STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS
63% SPEED RECORD 82

Inlet Total Pressure = $88,770 \text{ N/m}^2 \text{ (1854 lbf/ft}^2\text{)}$

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
-55.4	0.965
-15.1	0.960
- 3.6	0.963
9.4	0.977
22.2	1.033
34.6	1.067
47.5	1.089
73.4	1.118
99.3	1.136
141.4	1.127

TABLE 0-6(Contd)

TABLE D-6(Contd)

	PSI
40	= 14.75 PSI
RECORD RY WALL KULITE STEADY STATE PRESSURES	= 101.8 KILOPASCALS =
WALL KULITE S'	SAMPLED = 10]
RECORD 82	MAXIMUM PRESSURE SAMPLED

PAGES

-																									Í																
241 244X PR:S	2.8.5	a.	٠,	v = 0	•	• •	٠	a.	a,	Ġ.	~	å.	-) o) =:	æ	٠.	5.85	ω .	0 4 0 4 7	ဆေ	9.08	đ)	9E.1	ے د	d . C 5	1.12	T. TP	6.1.5	9.75	1.12	97.9	5.8.5	5 R 5	e) 0	96.99	\$ 100 h	9. 9.	43.5	4.00	
<u>ي ح</u> ر	, ~	-3	•	. •	• .	• •		٠,		•	-	•	•	٠		~		•		• ·	• ;		•	•	• '	-11.0	•	۰	<u>.</u>	• •	-7.4		٠,	ې ا	m r r i	יו ה		2	•	_	
TMAXIMUM PRESSURE	6.86	٠	8	တေ		• •	0	5	۶.	66	ဲ	9.65	•	• •	, w	Θ	3)	77 1	20 (ם ע		6.	÷	٠.	• •	99.2	*	÷.	٠ د	• . o	٠,	٠,	٠	.	ر م م	•	, ,	6	5	1.64	
نشا لمت	27	26	25	-24.5	' '	2 2		Ċ	2	<u> </u>	3	-19.1	א נב	- ~	. ح	•		-14.9	3 1	0 0 0 0 1	~	-	_	•		0.6-	9)	e m	<u>,</u> ,		4	5.	•	• • •	-2.4					ස ී ු	
IMUM SURE	47.6	57.7	48.1	94.6					•			97.3								0.00 0.00		_	-			97.4		_	8°.				5	oc r	2.16		٠. ح	5	•	9	
TANGENTIAL (OFG.)	~	2	~	~ ?	, ,	. 6	5	64	2	C.	6	\overline{c}	J (· -	_	7	_	4		יי פי	\sim	-			• 6	-8.5		ب	∧ √	די ל	-2.7		£.[-	-		9,7	٠. ا	6.2	9.0	2.5	
ZMAXIMUM PRFSSURE	6	8	•	Λ.	3 4	; ;		7	9	·C	3	ė.	ہ ہ	, ,		•	-	٠.	•	43.4		<u>د</u>	46.3	•		96.1		•	2.96		•	3.	٠,	:	ກ ເ •	٠ _:	•	6.7		45.7	
ى 2 -	÷	÷	;	Ω.	•	· ·	``	•	.'	٠ ئ	•	~ .	٠.		-: (• -:	3	j	ζ.	å,	1 4 0	. 7	~	~	-11-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-	0		٠	စ် (- / -	: :	. , `	٠.	15.3	٠.	1 - 4 -		13.6		-1 . P		
24.0 ZNAXIMUM PRESSURE	6.	٥١	•	2.96.2			*	_	• :	LC.		-, -	r 1	, -	~	~~	7	_ /	**	~				ው ተ ዕ	• ~	32.0	- 4		~ ~		36.7	~	-	3. Fr	· · · · · · · · · · · · · · · · · · ·			٠		6.6.4	
. , , ^	٠,	9,490-	-56.	34.6	7.00		-7.41	7.06-	0.61-	-1H.7	-1P.4	् । व ।	2.7.7	-17.6	-17.4	-17.1		4.4		-11.5	9.01-) • 6 -	- / - /	, 2-	6.9-	٠Ç	-6.7	ડ પ	ۍ د	1.9-	6.4-	5.6	\.\.\.\.\.\.\.\.\.\.\.\.\.\.\.\.\.\.\.	\$. K	ب م م	7.5-	-1.(· -	,• 0	
SAMPLE NUMBER		Ŋ	~	4 1	٠.		a,	¢	01		~ 7	e	•	10	17	o ·	2	2.5	- (· 6.	1 7 1	٠,	26	~ o	. 62		1 6	25	د. لا دن ۱۱	t un	35	37	E (⊅ (₹) (- 4	4 6.7		77	4.5	4.6	

TABLE D-6(Contd)

	Σ	MAXIMUM PRESS	I PRESTURE SAMPLED = 101.8 KILUPASCALS = 14.75				•		
E CAUAD .		Y CHORD=		=CHOKD=	73.4	CHOKD=		# CHURD=	
TANCENTIAL		TANGFALLAL	ZMAXIMUM	TANGENTIAL	EMAX IMUM	IM TANGENTIAL	ZMAX IMUM	TANGENT IAL	
		(0.66.)	_	(056.)	PRESSURE	(086.)		(016.)	
			9.56	2.t	97.3	2.6		1.5	95.2
		3.4.	95.5	3.5	97.5	2.2		2.€	7.84
		. n]	6.55	4.9	91.6	2.E		2.5	6.18
. 4		4.7	96.5	6e 1	97.6	3•3		2.9	6.16
. ~			7. 36	6.7	6.16	3.6		4.3	: 4 • 33 →
· ·		() ()	6.05	7.4	96.1	4.2		4 • €	43.2
, (,		4	92.3	8.3	7.86	ස ැ		5.	5.06
		و و	65	ط . ه	000	5.1		7.6	ۥ64
3		7.5	93.4	9.2	m.	5.1		P.1	96.8
		.n	8 . 4	8.6	49.1	6.1		છ. • લ	53.7
0		7.0	56	16.1	7.86	5.8		6.4	¥8.9
•	96.8	10.2	6.95	10.1	5. 66	10.2		10.2	6. u 6

Of Four J

% MAXIMUM PRESSURE

CURVE CURVE

LABEL VALUE 2 0.930000E+02

3 0.860000E+02

4 0.7900U0E+02

5 0.720000E+02

8 0.850000E 02

MAXIMUM STATIC PRESSURE 101.8 KPa (14.75 PSI)

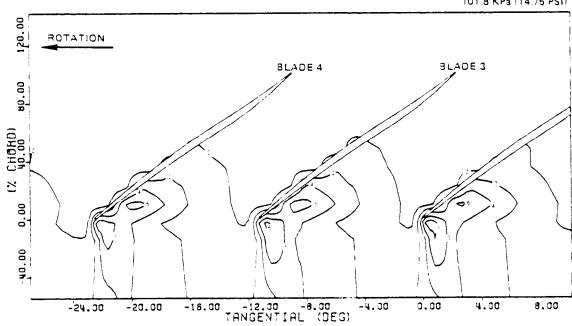


Figure 0-3 Steady State Pressure Contours at Blade Tip; In Flutter, High Operating Line, 63 Percent Speed, 53.4 Percent Flow, Pressure Ratio 1.2374

TABLE D-7
STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS

Inlet Total Pressure = $89,440 \text{ N/m}^2 (1867 \text{ lbf/ft}^2)$

66% SPEED

RECORD 239

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
-55.4	0.963
-15.1	0.960
- 3.6	0.962
9.4	0.981
22.2	1.041
34.6	1.079
47.5	1.100
73.4	1.130
99.3	1.149
141.4	1.139

CHORD=

= 15°00

XILOPASCALS = 1

RECORD 239 WALL KULITE STEADY MAXIMUM PRESSURE SAMPLED = 103.8 K

PAGE 2	22.2 EMAXIMUM PRESSURE 84.5 92.2 94.8
	T CHORDS ANGENTIAL (DEG.) P.2 9.3
PSI	9.4 RMAX IML 9RES SUR 89.6 91.9
RECORD 239 WALL KULITE STEADY STATE PRESSURES 4AXIMUM PRESSURE SAMPLED = 103.8 KILOPASCALS = 15.00 PSI	# CHORD= TANGENTIAL (DEG.) P.2 9.3
Y STATE PRE	-3.6 EMAXIMUM PRESSURE 90.3 92.9
ULITE STEADY ====================================	TANGENTIAL EMAXIMUM (DEG.) PRESSURE A.2 PR.3 90.3 90.3 16.4
239 WALL K URE SAMPLED	THAXIMUM PRESSURE 91.6 97.7
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x	-55.4 24.4 XIMUM 1 29.5 89.5 89.6
	ER TANGENTIAL E (116G.) 3 (1.2 9.3 9.3
	SAMPLE NIPAFR 49 51

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RECORD 239 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURF SAMPLED = 103.8 KILOPASCALS = 15.00 PSI

1 .4 X IMU	RESSURE	96.2	ا ب	6-16	- 1			- 0		٠.	å	٠,	•		٠,	:	_	•	.	•	Ŀ	98.3	نه	φ,	•	98.1		C)		1.85	ن ت	J.86	9.16	E	に よ れ り	B*16	8-16		•	υ,	ລ ເ	<u>.</u>	د	3. (ෆ .	•	y P . 1		45.0	
T CHORD=	(DEG.) P	(T)	•	_ ,	٠ د د	7.6%		•	٠ د د	4.	60	-22.7	71.7	23.6	59.	\sim	-27.3	•	\sim	\sim	53	2,5	٠ ئ	. 5 .	33.	- 1	-16.6	ů.	. 4.	53	17	•	-1	•	•	•	٠	•	·	٠.	•	•	٠	•		•)•;			
99.3 ZMAXIMUM T	ESSURE	00	3	66-1	י כד	ಬಿ	٠	20 (20	c)	٠ <u>,</u>	٠,	Ġ	6	œ	٠		96.1	٠	٠	66*3		1.66	5	7.66	æ	٥.	a.	1.86	6	6	L. 14	0	ċ	O.	ဆ	æ	۰ بد	e • 3	3,	20	Ĵ	→	5-56	~	9° a6		2.50	~	•
# CHORD=	(010)	3.54-	2	-41.3	0	3.0	1-85-	5	9	6.42-	-33.8	-32.7	31	•	5	-26.4	-27.3	~	-25.5	-24.1	-23.6	\sim		œ	ىت	~	•	3	•	"	\sim	-11.2	-16.1	٠, • ا ن	6°L-	٠	-5.8	٠	•	7.1-	-1.5	٠	(.)	a. I		•	•	•	1-7	:
73.4 PMAXIMIM I	SURE	95.8	4.96	6.16	97.2	97.1	٠		٠	98.5	•	47	96.3	6.96		97.3	•		6.16	4° 46	α.	~	8.96	7	8	9	8	e.	C 85	65		9.16	•	66.7	~	٠	۲.	-	~	е В	8	æ	1.56	5.	•	~		, ~	L . L0	٠
CHURD=	(DEG.)	•	ď,	-41.3	4 C.	9€	38.	۲.	36.	.7	33.	32.	~)	•	6		7	9	•1	4		-22.0	-21.9		٠	-	•	Š	•	۶,	€,	-11.2	-10.1		•	6.9-	-5.8	L.4-7	-3.6	•		4.0-			2.9		, c	- 4	 	
47.5		95.0		9.50			٠	91.6	93.2	94.3	95.0	9.70	,	5	1.96	5	4	2	4	Q	-	-		,		9	Š	_		· ~	3	٧,	S	•		96.1	45.3	93.0		93.2	•	ď.	•	9		٠.	2 () (r (
₹ CHOR	18%(cent 18L (016.)	, ~	1,-24-	-41.3	-45.3	-35.2	-36.1	-57.0	-36.	-34.9	-13.8	-32.7	7.11.	-3(.6	-29.5	-28.4	-27.3	-26.3	-25.2	-24.1	0.85-	-55-6	25.50	-19.5	-) H - 7	-17.6	-16.6		-14.4	-13-3	-12-3	-11-2	-10-1	C * 5 -	6-1-	•	± 0.00 €		3.	2	•	· -	~)				7 (C) 10 (A)	•	 	•
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TABLE 0-8(Contd)

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Contraction

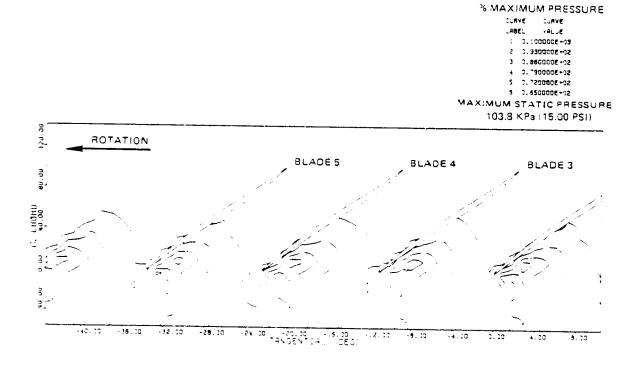


Figure D-4 Stoady State Pressure Contours at Blade Tip; In Flutter, High Operating Line, A6 Percent Speed, 54.5 Percent Flow, Pressure Ratio 1.26

TABLE D-9

STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS

67% SPEED

RECORD 141

Inlet Total Pressure = $82,500 \text{ N/m}^2 (1723 \text{ lbf/ft}^2)$

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
-55.4	0.931
-15.1	0.938
- 3.6	0.957
9.4	0.952
22.2	0.994
34.6	1.020
47.5	1.022
73.4	1.017
99.3	1.030
141.4	1.036

() _c	١.	TANCFE, ITAL
ORGANAL PAGE OF POOR QUALTY	3 lakes	KIM3. R

TABLE D-10

⁹ 10)		Ĭ	RECORD 1 MAXIMUM PRESSURE	141 WALL KUL] JRF SAMPLFD =	KULITE STEADY D = 97.6	STATE PR KILOPASCA	ESSURES LS = 14.14	PSI		PAGE 1
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	TANCFRITAL (LEGA)	ZMAX IMUM PRESSURE	7 3	SMAXIMUM	TANGENTIAL	KMAX IMUM	ENTIAL		ENT JAL	ZMAXIMUM Second
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4 (! ; ; ;	÷.	2.15-	-		•	. 4	٠ د	-36.3	•
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J.	\$ 1 32 (-28.3	٠ ت	-25.8		٠ د،>	~)	•	•
·, •	- 42-		-27.9		-23.3	94.2	-28.6	•		•
- :	3		4.12-	÷.	-22.3		-27.4	•		•
` .			-26.5 5.55	3 1	-21.9		~) •	FF.3	j	J* 92
<u> </u>	, ;			5 6	-2163	64.4	٠	<u>:</u>	ď.	50.2
<i>t</i> -	£ • • • • • • • • • • • • • • • • • • •		22.4	an.	-21.3		~ ((n)	٠,	67.1
· ·	7.4.7		1,25	7.00	6.02-	51.9	\sim $^{\circ}$	٠,	-23.5	43.4V
; <u>r</u>	7• ↑ . T		n :: 2-	•	0.17-	03.1	\ .	٠	• • (٠
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<u> </u>) a			67.3	C. V)·19		o Shiri	٠,	5
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, <u></u>	3 0 1			10	0			•	•	•
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<i>ج</i>	-16.2		-15.5	£5.6	-16		-17.5		٩	e :
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TABLE D-10(Contd)

180		Σ	RECORD MAXIMUM PRESSU	141 WALL JRE SAMPLE	KUL1TE STEAD D = 97.6	Y STATE PR KILOPASCA	CORD 141 WALL KULITE STEADY STATE PRESSURES RESSURE SAMPLED = 97.6 KILOPASCALS = 14.14	154		PAGI 2
3 1 db 1 E	% CHURD≅	-55.4	=QNOHO \$	-15.1	# CH080=	-3.6	=OROHO %		# CHI-CO=	22.5
X 1.55(1)	TATC: VITAL	THAX I HUM	TANSFULIAL EMAXIMUM	THAX I MUM	TAN	WMAX I MUM	TANGENITAL	2MAXIMUM	TANGENTIAL	THEX IMUM
	(DFG.)	PRESSURE	(1930)	PRF SSURE		PRESSIJAE	(0)(0)		(010)	PRI SSURE
۲)		11.6	0.5-	66.1		85.6	-5.3		6.4-	9.3.1
÷		G. 60	1.0-	36.06		92.4	5.5-		L.4-	F3.1
••		£2.3	-2.2	87.0		76.1	-2.3		-4.1	₹.0 ±
C .		03.4	-1.5	89.2		72.1	-1.5		13.4	4.08
,		P.3.6	6. T	F. C. 9		67.0	-1.0		-2.1	52.50
,		54.2	-1, -2	8.1.0		61.5	\$ ·)-		4.1-	12.9
*\ *\ *	₹•)-	L. 2 3	(• 2	7.54		63.4			ī) •[-	35.2
Ş		\$ • 000	,	64.3		65.0	C • 2		-0.2	7.61
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r •		73.9	1.:	64.2		63.3	1.6		1.6	86.6
7		74.7	ე• ₹	64.3		65.9	2.7	57.8	5.4	1.4.6
		72.9	2.7	61.7		64.1	2.8	55.4	2.1	12.2

RECORD 141 WALL KULITE STFADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 97.6 KILOPASCALS = 14.14 PSI

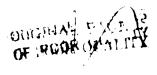
PAGE 3

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1,4	PRESSURE	26.7	16.7		ŝ.	•	•	•	æ.	اب	(a)	•	٠,	:	7 1 2			. c.	٠,	1.1.	- 1	- 1	n 1	1.1.2	61.5		67.2	7-19	4. I a	3.7.6	1-1-4		9. 5	2 0 0 0	7° 70 m		- W	18.2	h8.3	16.4	5. 9.	•	• :	-	•	-	1) 5	•
CHOK	TANCENTIAL (UEG.)	-22.5	-31.2	-00°	-28.6	6.62-	-27.5	-76.5	-25.6	- C - I	-24.3	7.5	2 : : : : : : : : : : : : : : : : : : :	-7.2.3	9-17-	٠.٠	1.,	5° 6 7 -	32 s 4. / 4. /	4.1.	•	. 6.3	Λ.	•	a) (יי אנג ו			F-;-			7.7-	φ•. 1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1	. • •	٠,	-2.1	٠.	۲ ۰ -	3 . (
99.3	PRESSURE	86.1	•	•	•	84.2	٠	٠	٠	٠	٠	•	•	•	-	•	•	٠.	٠.	٠.	٠.		•	_	•	•			·	*	P7.8	~3		· .	20° 5	• -	•		e Ti	•	7.8.	-	•		•	./3	F6.1	86.6
: CH0k	TANGENTIAL EDFG-1			_	-4	-26.7	- 5				a.	<u> </u>	3.	~	-5.I.e.Z	•	- 1	J	J	2	-+	_	-26.5	٤	ú	٠	5.6.4	6	2	€.	-10.3	_		ټ,	٠	•	1 7	- (101		_	-1(•	· 6-	- p • J	6.1-	-1.5	-7.1	- f. a.t.
73.4	TMAX IMUM					86.5																		10	. ~		~	-		~	~	_	•	~	€8 ••••••••••••••••••••••••••••••••••••	0.1	- 0	• •			.† • ; • a	•		\$		ė	8c.1	
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TABLE
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	141.4 #MAXIMUM PRESSURE 87.5 87.6 87.6 87.6 87.5 87.5 87.5 87.5 87.3 87.3 87.3
	## CHURD=
PSI	**************************************
SSURES .S = 14.14	## CHORD= ### (OEG.) ### (OE
STATE PRE KILOPASCAL	73.4 PRESSURE 86.3 P7.0 P7.0 87.4 87.4 89.3 89.3 89.2 84.1
RECORD 141 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 97.6 KILOPASCALS = 14.14 PSI	T CHORD= TANGENTIAL (DEG.) 1.0 -1.0 -1.2 -0.3 0.7 1.9 2.6 2.6
141 WALL	2MAX1MUM PRESSURE E9-9 F8-2 E7-7 E6-3 86-1 86-2 88-7 88-7 88-2
RECORD AXIMUM PRESSU	TANGENTIAL & CHORD= (DEG.) (DE
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	TANGENTIAL (0:6.1 -(.4 -(.7 1.1 1.2 1.2 1.6 2.6 2.7 2.7
	54 40 52 52 52 52 52 52 52 52 52 52 52 52 52



OF POUR QUALITY

% MAXIMUM PRESSURE
CURVE CURVE
LABEL VALUE
2 0.930000E+02
3 0.860000E+02
4 0.790000E+02
5 0.720000E+02
6 0.850000E+02
7 0.580000E+02
8 0.510000E+02
MAXIMUM STATIC PRESSURE
97.6 KPa (14.14 PSI)

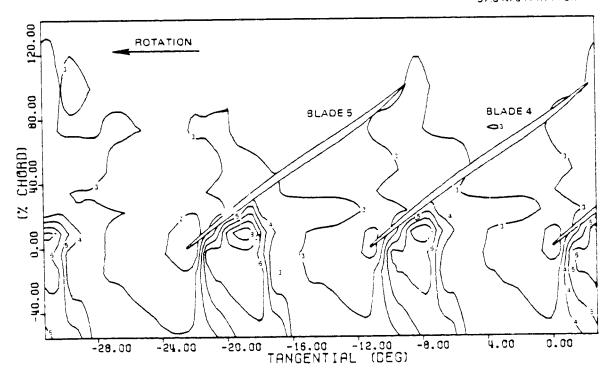


Figure 0-5 Steady State Pressure Contours at Blade Tip; Out of Flutter, Low Operating Line, 37 Percent Speed, 68.5 Percent Flow, Pressure Ratio 1.1900

22.2 PRESSURE 61.7 61.7 62.1 78.5 82.9 82.9 82.9 82.9 82.9 92.5 92.5 92.5 92.5 92.5 92.5 884.3 84.3 76.4 66.6 64.0 71.5 74.5 78.2 26.98 85.23 88.3 88.3 1.06 6, 2, 64.3 72.9 14.7 57.7 57.5 59.3 58.2 -6.2 -5.7 -4.7 -5.7 -2.6 1.5 86.9 86.8 88.9 88.9 990.7 990.7 991.0 88.9 56.5 49.5 61.10 78.5 6.78 86.9 86.33 56.5 7.75 CHORD= TANGENTIAL (DEG.) -36.6 -29.6 -29.6 -29.6 -27.9 -27.9 -27.5 -26.1 -26.1 -26.1 -26.1 -26.1 -26.1 -26.1 -26.1 14.19 1111266 111266 111266 111266 111266 -21.2 -26.7 -20.2 -14.6 -19.2 -18.6 -i7.1 STEADY STATE PRESSURES 97.9 KILOPASCALS = -3.6 RMAXIMUM PRESSURE 62.9 65.1 72.3 83.2 85.6 87.0 89.6 888.5 990.2 990.2 990.2 990.2 990.2 990.2 990.2 990.2 990.3 900.3 60.1 63.5 61.2 61.6 0-29 4.19 84.6 87.1 100.0 4.09 9.96 TANGENTIAL (DEG.)
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TABLE D-11 (Transient Data) (Cont'd)

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RECORD 28A WALL KULITE STEADY STATE PRESSURES
MAXIMUM PRESSURE SAMPLED = 97.9 KILUPASCALS = 14.19 PSI

141.4 Hanth	PRESSURE	• ·	<u>.</u> ,	å.	;	•	•	• .		۲۰۰۰ د ۲۰۰۰	•	•	0 4	•	•	، د	٠ ﴿	, .	3				,;	Š	15.7		ġ	Ġ.			٠,) 0	٠,	•		27.3		•	E 6.1	3	•		;		·	. ~	2 6	•
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₹ CHOR	TANGENTIAL	, ,	• •	6.5%-		-25.2	•	-23.7	-23.3	-22.8	-22.4	•	-21.6	•	-19.3	•	-16.5	-17.e	-17.1	•	-16.3	•	-1:04	•	-14.5	1 0 1 1	•		-11.6	: :	-10.5	un.	-	-	7	۲.	•	•	ν) . Ι	ď.	ġ.	.	4	40	•	ř	ω,	
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SAMPLE	NUMBER	•	→ ^	v 6	۱ ۷	٠ ،	۸ ح	۰ ،	- a	o or		2 =	- 2	13	· -	5	16	1,1	٩	19	20	21	22	23	54	52	2 ¢	- 80	2 C	۶ ر د د	÷ 7	, L.) (m)	7.17	35	36	37	3.8	39	67	4.1	75	43	44	54	77	17	

TABLE D-11 (Transient Data) (Cont'd)

PAGE 4	141.4 MMAXIMUM PRESSURE 36.5 86.5 86.5 86.5 86.2 86.4 86.2 86.4 86.3 85.4 85.4
	# CHORD= TANGENTIAL (DEG.) 2.3 3.0 3.7 4.4 4.4 4.7 4.7 6.2 5.5 5.6 6.1
PSI	2M AXIMUM PRESSURE 82.0 92.0 91.4 81.5 81.5 82.3 82.3 82.3 84.5 84.5
CORD 28A WALL KULITE STEADY STATE PRESSURES RESSURE SAMPLED = 97.9 KILOPASCALS = 14.19 PSI	TANGENTIAL (DEG.) 3.9 4.3 4.6 5.2 5.6 5.9 6.0 6.0 7.0
r STATE PRE Kilopascai	73.4 PRESSURE 81.6 P2.7 82.7 83.7 85.0 85.0 85.0 84.9 84.9 84.3 84.3
(ULITE STEAD)	# CHORD= CHORD= TANGENTIAL (DEG.) 3.1 3.5 3.9 4.6 4.8 5.3 5.3 6.3
28A WALL I URE SAMPLET	47.5 RMAXIM PRESSUR PR
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	SAMPLE VUMBER 60 00 00 00 00 00 00 00 00 00 00 00 00

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% MAXIMUM PRESSURE

CURVE CURVE

LABEL VALUE

2 0.930000E+02

3 0.860000E+02

\$ 0.790000E+02 5 0.720000E+02

6 0.850000E+02

7 0.580000€+02

8 0.510000E+02

MAXIMUM STATIC PRESSURE 97.9 KPa (14.19 PSI)

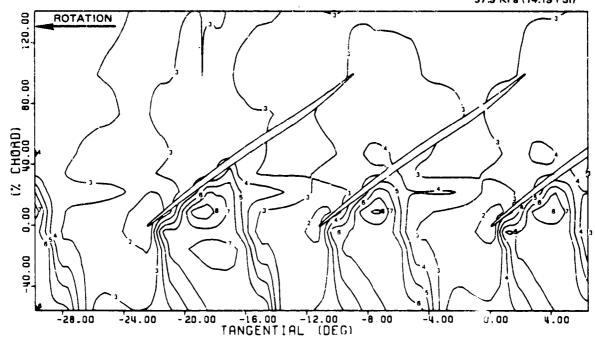


Figure D-6 Steady State Pressure Contours at Blade Tip; Transient Into Flutter, 70 Percent Speed, 74.5 Percent Flow, Pressure Ratio 1.2120, Incidence to Mean Camberline 5.6 Degrees

OF THE CONTRACTOR

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RECORD 288 WALL KULITE STEADY STATE PRESSURES MAXINUM PRESSURE SAMPLED = 151.5 KILOPASCALS = 14.70 PSI

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TABLE D-12 (Transient Data) (Cont'd)

		r	RECORD HAXIMUM PRESSI	288 WALL JRF SAMPLE	KULITE STEADY D = 161.5	Y STATE PR KILOPASCA	CORD ZEB WALL KULITE STEADY STATE PRESSURES RESSURF SAMPLED = 161.5 KILOPASCALS = 14.70 PSI	PS I		PAGE 2
SAMPLE	# CHORDE		CHORD*	-15.1	Z CHORD=	-3.6	CHORD=	4.6	CHORD=	22.2
NUMBER	TANCENTIAL	ZHAXIHUM	TANGENTIAL	ZMA XI MUM	TANGENT JAL	EMAX I MI	JH TANGENTIAL	ZHAX1M	UM TANGENTIAL	ZHAX IHUM
	(053.)	PRESSURE	(088.)	PRESSURE	(056.)	PRES SURE	(DEG.)	PRESSU	(086.)	PRESSURE
64	0.0	74.0	-(, -1	89.7	-0-1	93.1	1.3	78.5	1.9	64.7
0	1.7	73.3	6.		a. O	59.9	١.٥	66.3	2.5	74.0
5,1	7.1	71.1	1.1		1.4	63.1	2.2	56.5	2.6	73.0
52	2.8	69	1.0	62.7	2.0	6.7.9	5.5	52.9	5.5	66.7
63	4) e	65.1	2.1		5.4	61.3		4.65	3.1	61.4
40	4.1	63.3	3.3		3.6	60.1	3.5	48.2	ы. М.	6.53
5.5	4.7	62.1	4.5		۴.۱	60.0	٥. ٢	52.3	3.7	25.1
56	5.6	61.4	5.1		4.7	67.8	7.7	50.9	4.0	65.5
57	5.9	62.6	5.3		5.1	74.2	4.7	68.5	4.3	71.4
S.	6.2	7.79	5.8		4.0	81.0	۴.3	86.6	2.5	75.6
63	6.3	67.6	۲۰۶		5.8	85.0	5.6 .6	84.6	5.7	8.66
ψ	4.3	69.1	6.3		6.5	0.78	4.9	66.2	4.9	ور د د د

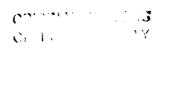
RECORD 200 WALL KULITE STEADY STATE PRESSURES
MAXIMUM PRESSURE SAMPLED * 101.5 KILOPASCALS * 14.76 PC

			, ,	34466	•	KILUPASLALS	LS = 14.70	I S d		
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35.00	10.03.1 10.66.3		(086.)	PRESSURE	COFGE	ZHA XIMUM PR F / CIB F	TANGENTIAL	MAN INCA	TAMGENTIAL	ZHAX INUM
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7	191	\sim	÷	\sim	-36.2	86.2	-36.6	,	-27.7	: 2
m ·	•	\sim	\$	e	•	86.5	-29.2		-26.3	
•	N (-	ند	9.48	•	86.1	8.63-	64.5	-25.5	6003
Λ,	~ 1			v	-27.3	85.6	-28.1		+25.5	•
ه د	~ 1 4	~		~	-26.7	6.48	-27.3	•	-24.6	-
٠.	• •	a.,	•	en i	-25.1	e5.3	-26.6	•	-54.5	-
1 0 (~ ·			جي	-25.3	86.2	-26.0	~	-23.2	
•	~ (-	-24.9	86.3	-25.5	~	-23.0	9
= :		•		91.3	-24.1	6.69	-24.7	~	-22.9	
- :		~		o .	-23.7	0°58	-23.8	•	T.22-	68.1
71		~ .		,-	-53.4	R 7	-23.1	a .	-22.1	
n . ⊣ ,		٠.	•	ň	-23.1	88.0	-22.5		-21.6	~
4 -					-22.7	1.50	22	•	-21-1	a.
<u>,</u>				۰	-22.5	85.3	-23.4	'n	-26.3	_
0 -	•				-22.3	95.1	-21.1	_	0.15-	67.7
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96			•	4	-17.1	97.4	-17.7		7.61-	8.7.8
27	•	-	٠		-16.4	87.2	-17.2		4.5.4	67.6
~ ?		•	•	÷		86.9	-16.8	.•	-12.1	1.10
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33	-9-2	•	•	•	v	,) « P @	7 :	•	5	67.9
34	. a.		5.01-	9-7-8	-11-		13.0	0 ° 0	m 6	e. /a
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36	-7.3	•	•	*	2	84.3	. ~	• •	6-2-	2000
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io d	v,	•	٠,	<u>.</u>	-9.4	9.48	J	٤.	-6.3	98.1
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4.3) -	000	# c	87.5		36.6
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TABLE D-121(Transient Data) (Cont'd)

		I	AXIMUM PRESSU	GRE SAMPLED	OLITE SIEAD!	K TLOPASCAL	CURD 2-50 WALL ROLLIE SIFAUT SIAIT PRESSURES RESSURE SAMPLED = 101.5 KILOPASCALS = 14.70	PSI		PAGE 4
SAMPLE	CHORD=		н	47.5	# CHORD=	73.4	Z CHORD=	600	E CHORDE	77.171
NUMBER	R TANGENTIAL	EMAXIMUM	TANGENTIAL	THAXIM	UM TANGENTIAL	THAXIT	TANGENTIAL	EHAXIMI	TANGENTIAL	ZMAX IMUM
	(DFG.)	•		PRESSURE	(DEG.)	PRESSL	(0,66.)	PRESSU	(0)(0)	PRESSIBE
	1.2			PP.2	-1.2	9 9 9	-2.5	88.2	0	0.68
	2•3		-2.5	89.4	0.1	83.3	-1.6	88.8	(a)	8. 9.
	5.5		-1.5	88.7	0.2	83.1	₩°0-	9 3 3	1,3	2,99
	3.6		-C-7-	88.6	6.0	83.	i • l	88.4	3.4	E.B.1
	4.2		-ú-2	87.8	1.9	83.5	1.4	87.8	2.6	88.2
	4.7		ن. د.	85.9	2.2	83.8	2.4	84.5		0.84
	6.4		1.0	84.6	3.5	86.1	2.0	B4.0	4.5	87.5
99	5.1		1.7	82.5	3.8	86.3		84.7	5.2	37.2
	5.4		7.2	81.4	4.5	86.5	4.4	83.2	9	87.1
	0.9			ea	5.3	96.4	5.1	83.9		86.4
	6.3		3.7	81.5	0.9	86.2	5.0	85.4	(,,)	8. 48
	4.9		4.0	15.7	9.9	85.6	6.2	86.4	9.9	6-98

7 17 18 **C**E 1800R QUILLEY



MAXIMUM PRESSURE

CURVE CURVE

2 0.830000€+01

3 0.860000E+01

4 0.780000E+01

5 0.720000E+02

6 0.620000E+02

0.580000E+02

8 0.510000E+02

MAXIMUM STATIC PRESSURE 101.5 KPs (14.70 PSI)

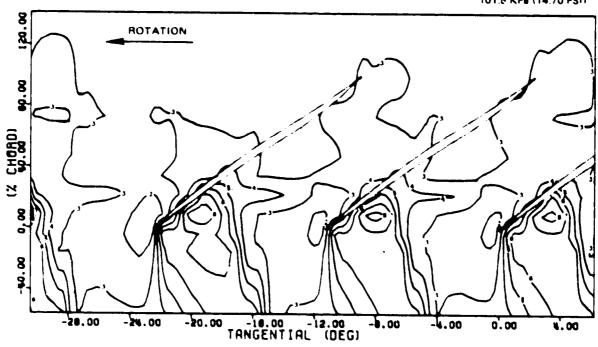


Figure D-7 Steady State Pressure Contours at Blade Tip; Transient Into Flutter, 70 Percent Speed, 72.5 Percent Flow, Pressure Ratio 1.2230, Incidence to Mean Camberline 6.35 Degrees

RECORD 28C WALL KULITE STEADY STATE PRESSURES HAXIMUM PRESSURE SAMPLED = 165.5 KILOPASCALS = 15.29 PSI

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72- 0.
.7 -26
97.8 -25.1
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TABLE D-13 (Transient Data) (Cont'd)

PAGE 2	22.2 #MAXIMUM PRESSURE 75.4 72.9 65.2 65.2 74.3 74.3 79.1
	Z CHORD= UM TANGENTIAL (DEG.) 3.4 3.7 4.0 4.1 4.4 4.5 4.5 5.8 5.8
PSI	PRESSINA 84.8 839.8 90.1 70.2 70.2 70.2 70.3 70.9 80.9
RECORD 28C WALL KULITE STEADY STATE PRESSURES PRESSURE SAMPLED = 105.5 KILOPASCALS = 15.29	# CHORD= # CHORD= # 16.3 1.3 1.7 2.5 2.9 3.3 3.6 4.6 6.0 6.9
Y STATE PR KILOPASCAI	FRA A 3
KULITE STEAD D = 105.5	# CHORD# IUM TANGENTIAL 20.8 30.2 30.2 40.3 40.3 60.3 60.3
28C WALL JRE SAMPLE	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
RECORD MAXIMUM PRESSI	#UM TANGENTIAL 1 FUNE (DEG.) F G. 2.3 3.0.0 5.3 7.4.1 1.4.5 6.3 6.3 7.6.9
	MASS RESS 98 98 97 77 77 75 75 96 97 97
	FR TANGENTIAL 1 (UEG.) F (UEG.
	N.M.B.R.N.M.B.R.N.M.B.R.N.M.B.B.R.N.M.B.B.R.N.D.D.D.D.D.D.D.D.D.D.D.D.D.D.D.D.D.D

H H A	S. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5.	TANGEN	73.4 EMAX IMUM	TANGE		T CHORD=	141.4 EHAXIHU
SSURE (DFG.)	PRESSUR	(086.)	PRESSURE	(066.)	SS	(050)	PRESSURE
1.0	•	• .	•	-36.5	•	-36-1	90.3
5.5 -28.	87.1	-27.2		7.62-	.	-28.7	, ,
3.0 -28.	•	2	0	-28.9	• a	-24.0	٠,
2.1 -27.	•	ŝ	8	-28.2		-26-2	• •
10/2-	٠.	å.	÷	-27.1	•	-25.7	6
26.3	7.00	-24.6	a :	-7 t . 3	3	-25.1	
7.2 -25.	87.9	• •	د	1.63-	ο.	-24.4	9.49
7.1 -25.	8	-22.9		7.76-	* * * * *		٠,
1.9 -24.	• 3	•	8	٠,٠) -		٠
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7.1 -2	• 00	200	2.06	8.0(-	7.06	-) F.9	1.36
5.8 -15.3) P	•	•	61.63	-1 Be 1	•
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5.4 -18.1		-15.9	89.1	2001		-17-3	\$ 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0
3.4 -17.5 P		5		- 4	7-176	1011	80 f
-17.0 e	•	-14.9	•	•	5.06	15.0	. 0
9 7 - 10 - 10 - 10 - 10 - 10 - 10 - 10 -	7.1	-14.0	•	-15.2	0.16	-14.2	2.68
1.0.08 1.	0 4	-13.5	90.1	4	91.1	-13.5	
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-14.4	; ;	-12.0		7:01-	61.9	-15.	89.8
1.94-	-	-11.2		: _	•	0 0 0 0	Э,
4.0		-11.1	87.4	. ~	91.2	1	ے د
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\$ · · · · · · · · · · · · · · · · · · ·	•	٠ ئى	67.6	•	•	-7.8	د :
7 0 1	7 0	•	87.7	Ġ	41.3	-7.2	9.16
	87.5	2.4- 6 9-	2.0	٠,	_ ,	9.7-	Š
-8- F.	. •	, L-	0 °	•	ر د د د د د د د د د د د د د د د د د د د	-6.2	8°06
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	,	•	•	•	9.16	•	7:16

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TABLE D-13 (Transient Data) (Cont'd)

PAGE 4	141.4 MMAXIMUM 90.3 90.3 90.3 90.3 90.3 90.3 90.3 89.3 89.3
	# CHOKD= TANGFNTIAL (DFG.) 3.1 4.1 4.7 5.0 5.0 5.0 5.0 6.1 6.1
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ESSURES LS = 15.79	T CHORD= 10H TANGENTIAL TANGENTIAL TANGENTIAL TANGENTIAL TANGENTIAL TANGENTIAL TANGENTAL TANGENT
Y STATE PR	73.4 MMAXIMUM PRESSURE 86.6 88.5 88.5 89.3 89.3 89.4 89.1
ECORD 25C WALL KULITE STEADY STATE PRESSURES PRESSURE SAMPLED = 105.5 KILOPASCALS = 15.29	CHORD= (UM TANGENTIAL (DEG.) (D.68 (D.68 (D.88
28C WALL	######################################
RECORD MAXIMUM PRESS	TANGFNTIAL (OEG.) -1.65
•	34.05 PRESSING 84.05 84.05 86.05
	2 CHORD= CHORD= 1 CHO
	SAMPLE Nymera 55 55 55 55 56 56 56 56 56 56 56 56 56

Comment of

% MAXIMUM PRESSURE
CURVE CURVE
LABEL YALUE
2 0.930000E+02
3 0.860000E+02
4 0.790000E+02
5 0.720000E+02
6 0.850000E+02
7 0.580000E+02
8 0.510000E+02
9 0.440000E+02
MAXIMUM STATIC PRESSURE

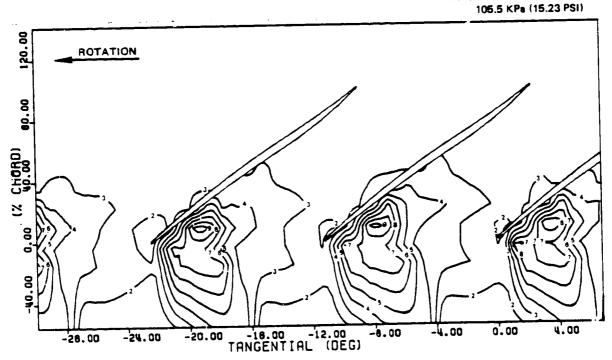


Figure D-8

Steady State Pressure Contours at Blade Tip; Transient Into Flutter, 70 Percent Speed, 66.8 Percent Flow, Pressure Ratio 1.2740, Incidence to Mean Camberline 8.05 Degrees

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PAGE	•	PRESCHER	73.2	75.0	74.4	77.4		هه ا ا ا		, c e	3° 75	0 · 4 · 6			7 · c · j		3 7 0	0 1		V	ר - ו ר - י	2 (x	٠ ا ا ا	7.03		F2.2	7000	ر ا ا				86.1	86.7	66.1	63.2	67.1	73.6	74.1	17.2	77.5	81.4	85.4	88.1	50.05	91.5	42.2	_		, ,	B 7	
	TANCENTE A	(0)	-30-4	-3(-2	429.9	-29.1	-24.5	1.67-	-28.7	-28-	-27.3	-26.4	125.4	2.4.6	-2	L.11.7	-21.4	C 1)C-	7 0 1		1140	ม . ม ง	1.01.	7 6 6		0.011	, ,	13.5	7.11-		1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4	-6-3	7.6	-7.4	6.1 -	-6.6	-6.3	-5-7	-5.2	٠. ٢	-2.8	-1.9	-1.2	-6.3	٥.6	1.5	2.3	C	3.3	
PSI	9.4 5.4	: 3	q	4	16.9	85.7	92.2	95.6	98.6	160.0	97.0	67.7	75.1	57.9	46.2	42.7	6.94	55.4	4.04	72.2	9.1	C - 78	1 (C)	3	0 4 0	97.6	, d	9.70	88.2	7.97	66.7	57.3	50.0	44.6	42.2	45.4	55.9	8.59	•		Or ∘	~	m	∽.	-Ω	_	12.7	76.3	55.0	0	
ESSURES LS = 15.07	RO=	(066.)	4.	-29.7	-28.5	-27.1	25.4	-24.1	-23.1	-22.6	21.8	-21.2	-2(.8	-20.4	-20.1	-19.7	-19.4	-14.1		-17.5	-16.6	-15.7	-14-7	-13.4	5.7.	5.11-	-11-3	-10.7	-10.0	9-6-	-9.5	J•6-	1.8-	۳. ع -	 	6.7-	-7.3	o.	Λ.	E 4 .	7.5-	6-1-	ο (-; ,	-(°-2			1.6	2.0		•	
' STATE PRES Kilopascals	-3.6 AXIMU		67.8	4.9	78.7	82.6	94.4	86.3	87.1	97.8	68.3	84.1	91.5	92.2	1.76	9.1.8	93.5	57.1	55.5	58.2	56.9	62.3	74.0	76.7	e1 - 1	84.2	95.7	86.7	87.0	9.68	91.3	93.5	96.2	8° 6	61.2	****	7 . 0	0 "	0.0	7.00	٠,٠٠	** 17		בי ה	, , , ,	4.0	P5.3	86.6	Œ	Ġ	
ULITE STEADY = 104.0	35	(DEC.)	-36.3	-59.T	-29.1	-28.5	-28.1	-27.4	-56.9	-26.2	-25.7	-25.1	-24.5	-23.9	-53.4	-22.6	-22.3	-21.5	-21.3	-21.7	-20.3	-19.4	-18.6	-16.1	-17.4	-16.5	S	•	-14.5	-13.5	-12.6	-12.0	-11.5	-11.2	1000			` «	•	2.6	7.1	9 4	1 4	٦ د	0.61	\$ \ F !		٠٠٠ ١٠٠٠			
28D WALL KULI RE SAMPLED ≖	-15.1 T maximum	RES	57.0	67.5	2°.3	9.	1 * 7 a	4 · 6 · 6	6.05	94.1	9.4.8	92.1	84.5	76.1	9.6	61.4		59.1	56.9	56.5	58.6	67.5	7.91	P1.4	e3 •1	85.9	80.2	89.5	92.1	93.1	87.4	8 · 5	1.69	9.04	57.0	¥ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	9 9	500						•	•		•	A 0 0 3		_	
RECOKD MAXIMUM PRESSU	U Z	(066.)	-32.5	-30.0	29.9	3.62-	6.1%	S 2 2 4	-25.1	4.22-	-22-B	-22.2	-22.0	-21.6	-21.5	-21.2	0.12-	-2 •5	5-52-	-15.2		-18.5		•	-16.8		~	-		= :	-11-	٠ -	ים ת	ro	٠.	a	, 🏲	•	4	,	•	41	15.0		. 6	, ,		7	•	•	
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TABLE D-14 (Transient Data) (Cont'd)

PAGE 2	22.2 ##AXIMUM PRESSURE 69.6 149.2 149.2 149.2 161.3 161.3 162.1 162.1 162.3 163.3 163.3	
	TANGENTIAL (DEG.) 3.9 4.6 4.6 5.7 5.7 6.3 6.3 6.3	
PSI	PRESSURE 47.7 47.7 45.6 45.1 66.0 66.0 72.7 78.2 80.6	
SSURES S = 15.07	Z CHORD= 2 CHORD= 2 0 1 2 0 2 2 2 0 3 2 3 2 3 2 3 2 3 2 3 2 3 2 3 2 3 2)
, STATE PRE KILOPASCAL	-3.6 FREAXIMUM PRESSINE 94.5 94.4 58.6 61.0 61.0 61.9 74.3 78.7	1
ULITE STEADY	2 CHORD= TANGENTIAL (DEG.) 10.1	•
28D WALL K JRE SAMPLED	115.1 PRESSURE 60.5 60.5 60.5 60.5 60.5 60.5 60.5 71.1 85.1	
RECORD 28D WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 104.0 KILOPASLALS = 15.07	CHORD= 1UM TAMGENTIAL 1RE (DEG.) 1.0 1.0 1.0 1.0 2.3 2.3 4.0 4.0 4.0	٥٠٧
Ĩ	######################################	7.7
	# CHCRD= TANGENTIAL 600.) 400.0 500.0 500.0 600.0 600.0 600.0	7.9
	SAMPLE NUMBER 50 50 51 53 54 55 56 58 59	C 9

	C C	· . ,	
X		,	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
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TANGENTIAL (DFG.) -31.2 -29.9 -29.2 -29.2 -29.2 -29.2 -27.3 -27.3 -27.3 -26.9 -24.3 -24.3 -24.3 -25.6 -24.3	27-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	7 1 2 2 3 5 6 5 6 5 6 5 6 5 6 5 6 5 6 5 6 5 6 5	
4.5.5 аастиповется в на 4.5.5 г. в на 4.5		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
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XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX			864-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1
# CHORD= 1ANGENTIAL DEG. -313 -213 -255 -27.4 -27.4 -27.4 -27.4 -27.4 -27.4 -27.4 -27.4 -27.4 -27.4 -27.4 -27.6 -27.6 -27.6 -27.6 -27.6 -27.6 -27.6 -27.7 -27.7		0 2 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0 0 - 0 - 0 - 1 - 1
PANAXAMUM MACAXAMUM MACAXAMUM MACACAMACAMACAMACAMACAMACAMACAMACAMACAM			
T CHORD= TANGENTIAL (DFG.) -25.6 -29.6 -29.5 -28.6 -29.5 -24.9 -24.9 -24.2 -25.3 -25.3 -21.9	C 24 = 2 = 2 = 2 = 2 = 2	14 5 4 4 C C C C C C F S	40 44 56 4 5 4 5 4 5 4 5 4 5 4 5 6 5 6 5 6
### # COM # CO # COM # CO # COM # CO # CO	11 12 12 13 14 18 18 18 18 18 18 18 18 18 18 18 18 18	できまさまままままま 多 C まできない なす B を C まかって できな B できな B できな B できる	644444444 044444444

TABLE D-14 (Transient Data) (Cont'd)

		π	RECORD MAXIMUM PRESSI	2PD WALL I	KULITE STEAD) D = 104.0	F STATE PRI	CORN 2PD WALL KULITE STEADY STATE PRESSURES PRESSURE SAMPLED = 104.0 KILOPASCALS = 15.07	P S d		PAGE 4
SAMPLE	LE CHORDE	34.6	₹ CHURD=	47.5	# CHORD=	73.4	Z CHORD=	600	# CHCIRD#	
NUMBER	TANGENT IAL	THA X I MUM	TANGENTIAL	THAXIMU	TANGENTIAL	ZHAX IMU	TANGENTIAL	ZHAX IMI	TANGENTIAL	
	(DFG.)	PRFSSURE	(056.)	PRESSUR	(DEG.)	PRESSUR	(0EG.)	PRESSUE	(0FG.)	
67	٠ ٠	91.9	-3.7	P7.P	-1.1	4.46	-2.5	95.3	-5-1	
53	ر.•٠	42.5	-3•3	87.0	9.1)-	93.4	-1.4	96.1	7-7-	
-4 V)	& C	52.7	-2.4	3.6	4°2-	92.2	() -	7.95	(-4-	
55	2.1	9°.0	-2.2	91.0	5.2	91.4		6.96		
53	J. 6	9., 6	-1.3	93.3	ى . 8	92.4	3. 	C.95	8. [-	
54	4.4	ን ን ን	j. 1	93.4	1.8	93.2	2.6	7 - 6	6.3	
5.5	6.4	· d d	1.2	6.56	5.4	93.4	2.9	94.5	5.0-	
9 (5.1	36.4	2.6	92.2	2.9	64.0	4.2	93.8	2.0	
2.1	٠,	84.4	4.6	95.6	3.8	94.1	4.9	93.6	1.	
a) ≀ an ≀	٠ ٠	P. 6 . 4	m •	92.3	4.6	93.3	5.6	44.3	7.7	
۲. د د	۴.2	87.2	£.1	91.3	5.6	93.5	6.2	94.5	3,3	
၁	6.7	3.5	6.1	90.1	6.7	93.3	6.8	95.0	8.9	94.3

C. C.

MAXIMUM STATIC PRESSURE 104.0 KPa (15.07 PSI)

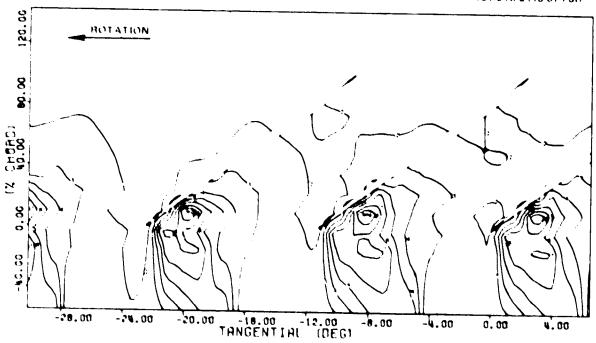


Figure D=0 Steady State Pressure Contours at Blade Tip; Transient Into Flutter, 70 Percent Speed, 62.9 Percent Flow, Pressure Ratio 1.2950, Incidence to Mean Camberline 9.2 Degrees

RECCRD 28E WALL KULITE STEADY STATE PRESSUMES MAXIMUM PRESSURE SAMPLED = 164.3 KILOPASCALS = 15.11

•	A CHO		£ 2	-15.1	# CHORD#	٠,	U	ó	Z CHORD*	22.2
K. M. W.	3	ZMAX1MUM	TAMERNITAL	ZMAK I MIJH	•	ZHAY INUM	1	*	HT IAL	EMAK IMUM
-	; •	Hafris S and	• (AF SS-JB	(pfc.)	FES SUM	ن.	RESSO	_	A.
٠,	י כ	- L	₽ .	5.73	0.05-	m	٦٠)٤-	•	-3: -1	74.7
۰ı ر		20.	∙ .	75.2	-59-3		-14.5	•	-23.4	16.3
٠ ،		2, 6			5-67-	•	-26.6	J	-26.4	44
r u			•		6.32-		7.8.		-67.1	1.78
٠.		> ()		1.62	3.5%		7.72-		-25.3	7.0
o r		6.15	••	92.3	-24.6	~	-25.2	•	5. 52-	9,.2
٠,	`;			93.4	-23.9	•	-24.1		5.22-	95.3
ar (٠,		• •	3. 7. 9.	-:53-	۸.	-1:01	~	4.15-	60.7
•	٠,٠	45		9	-22.3		-22.2		1.12-	\$6.3
	4 \	7.55		15.1	-22.1		-25		5.5.	5.45
- :	.1	100.0		72	-21.8		-2:.2		7.61-	4
12		6.68		65.	-21.6		-21.0P	_	-14.1	
· ·	·	ar 		67	-21.4		-20.6		5	4.16
٠.	<u> </u>	57.6		6 1	-20.6	_	-75		-16.6	76.7
• •	-	5.16		6,.,	5.6:-		-20.2		-: 5.2	7
4) ! 	3	62.2		1.65	-19.4		-26.1	Ĭ	-17.5	19.6
~ .	ייט	ر د ا	_	6.13	-18.5	•	-14.5	•	-16.6	25.4
• •		7. 7		64.5	-17.2	.*	-15.6	•	-15.0	45.6
» ,	ar f	7.7		7.06	-16.	•	-15.1	•	-14.3	
•	~ 1	1.67		75.4	- 1 4 . 8	•	-16.4	•		7 7
~ ·	- 1	~		1.61	-13.3	:	-17.7	•	2.5.5	92.0
	٠,	٠, ، د ، ،			-12.6		-17.1	•	-11.5	56
	٠,	93 6 43 5 5 6	-	3 A	-12.6		-: 6.3	•	7	
	٠,	P .	-		-11.5	. •	-15.5	•	1.5-	
, ,	.	RI F			-11.5	. •	-14.3	•	-6.	45.3
		3 , C		. n	F . 7 (-	•	7-51-	•	7.3-	
- a	Ň	7.7	-		-10.6	. •	-17.6	•	7	
	ř	7	-	*	-1.4.	•	5. I i-	•	6.4-	
• .	٠,		•	5.15	· · · · · · · · · · · · · · · · · · ·	٠	-11.4	•	-7.4	
. -	٠.	- F 4 3	-		1°.	•	6-31-	•	-7.3	
		6 6 6	•	72	3. 6. 6.	•		•	-7.	73
141	J		•		· •	•	ا د ا د	٠	-6.7	75.2
4		· · · · · · · · · · · · · · · · · · ·			f &	•) · 5 · 1		٠, به	1.05
10	•	72.1		7 77	• •	•		٠	۸ • ۲ ·	2.
4)	•	76.3		61.2		•	L 0 1	•	** °	٠ ا د ا
_	•	75.8	ŗ	61.2	203-	•	· · · · ·	•	• • • • • • • • • • • • • • • • • • • •	£3.3
•	•	77.9		53.1	6.4	•	7.4	•	•	
J	•	FC.7	•	57.7	-5.2	•	-6-2	•		7000
	•	86.98	-7.6	66.3	-2.7	4.	5.1-	, i ,	, , , , , , , , , , , , , , , , , , ,	
	;	\ .	۲.	65.1	-2.0	•	7.6-	~	•	
، ب	٠,	5 · 5 · 5		7 .2	-1.3	•	- (• 3	e 3	3	94.2
· · ·	٠,	1.56	٠,	76.2	5.7	•	Z	41	1.4	J
•	٠	~ 55	•.	િ 	m .)	1.06	•	63.2	?	44.7
ņ,	7.7-	~ ~ ~	•	o .	3	65.7	-2.E	26.5	3.5	93.5
o r	· .		٠,	F6.3	٠,٠	1.5.1	_	4.14	2.8	41.5
		- · ·	 ni .	67,7	C. C.	6.3	4.1-	93.5	3.1	
,		*	-	2.49	3.7	74.4	~	45.00	3.0	65.1

TABLE D-15 (Transient Data) (Cont'd)

PAGE 2	22.2 HHAXIMUM PRI SSURE 51.1 76.0 76.1 76.1 76.2 76.9 76.6 8.01 62.05 64.8
	# CHORD= TANGENTIAL (DEG.) 3.5 2.6 2.4 2.4 4.2 4.2 4.2 4.2 4.2 6.3 6.3
PSI	######################################
SSURES S = 15.11	### CHORD= TANGENTIAL (DEG.) 0.7 1.2 1.5 2.3 2.6 2.6 2.6 2.6 3.8 4.7 7.0
'STATE PRE KILOPASCAL	-3.6 RMAXIJUM PRESSURE 65.1 65.6 62.8 65.4 73.7 73.7 73.7 83.9
RECORD 28E WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 164.3 KILOPASCALS = 15.11	2 CHORD= TANGENTIAL (DEG.) 0.9 1.0 1.0 1.0 1.0 2.3 2.8 3.5 4.4 5.1 5.1 5.3
28E WALL D Jre samplet	######################################
RECORD AXIMUM PRESSI	# CHORD= TANGENTIAL (DEG.) -1 (0.4 (0.4 1 1 1 2 4 5 7 7
Ĩ	448 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
	# CHORD# 1066.1 1066.1 1.6 3.1 3.7 4.2 4.7 4.7 6.1 6.1
	NUM MAN MAN MAN MAN MAN MAN MAN MAN MAN MA

		x.	RECORD 2 MAXIMUM PRESSUR	ZPE WALL KULIT URE SAMPLED =	KULITE STEADY D = 104.3	r STATE PRESS KILOPASCALS	ES SUR ES LS = 15.11	PSI		FAGE 3
SAMPLE	# CHCRO#	34.6 Max I Hum	CHO	47.5 \$MAXIMUM		73.4 ZMAXIMUM	TANGENTIAL	99.3 TMAXIMUM PRESSIBE	TANGENTIAL (DEG.)	THAX IMUM PRESSURE
	(1056.)	F S S	(066.)	RESSUR	: :	K=5504		6-2-6	30.1	46.4
	μ,	92.8		7.76	o or	, r	•	8.96	-29.8	96.5 64.5
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4 4	1 0 0 C C		-27.5		-27.0	•	,	٥,	• •	, .,
Λ,	2 · B · C ·	1 - L d	-27.2		-26.5	•	2.7	•		
٩٤	1 2 L	0.69	-26.5	•	-25.9	•	, c	۵ ۷	ی .	, ,
~ a	-27.6	85.3	-26.1	Φ	-24.9	7.96	5.	•		5
o G	-27.1	88.1	-25.8	•	-24.5	•	• :	· ±		•
10	-26.2	7.00	-56.5	2	22.0	7.0	· ‹		-22.3	÷
11	7 -75.3	95.5	-24.6	7 - 7 6	-23.2	• •	5	98.3	22.	<u>, </u>
12	-24.3	0.46	1.52-	•	-22.5	4	2.	•	5:	· .
13	-23.5	45.6	3077-		-22.3	4	•	.	د	
51	-22-3	0	5.16-	, .ç	-22.0	4	J-	•	C•4+	• :
<u>.</u>) · [/ [6,43	-21.4	ું	-21.6	95.3	، ب	4. × 0	0.011	9.06 9.09
0 [0 0 1	94.6	-26.7	S	-21.1	ς.		7. L. Z		
- •	-10.3	33.0	-20.5	Š	-2 i. 7	ġ.	•	7 60	. 7	٠
, 6	, - w	45.7	-10.9	6543	· ·	ø	0 4	97.1	() () () ()	3
. (1.1.	88.1	4.61-	∙0	5 3	•	7.3.1	6.96	-15.6	3
21	-17.5	85.3	-18.9	٥.	- TB-5	• 4		6.96	4	Š
C.1	-17.4	64.5	-18.3	ب و	٠,	• 4	' 3	97.1	4	5
23	-17.1	P3.7	-17.9	40.8	• 2	9	-13.9	4.16	m	S
56	-16.7	85.J	7.11-	7	15.		-13.5	7.16	'U	s,
52		1.18	0 0 1	e Pop	, 4	9	-13.6.	T. 79		41 4
26		ກ : ສ ເ ສ ເ		• •	س.	ø	-11.9	97.7	77	7.06
27	-	5	15.1	•	2	9	-11.1		6-11-	3 4
5.7	7 6 4 1	4-66	7.7.	7.16	2	96.4	-10-1	200	-11:03	0
6. E	• -	93.9	-15.4	CI	-11.4	m, 6	7.01-	e i	2.1-	ು
31	-)• 35	-12.8	۳,	-11-2	734	• •		4.5-	96.2
Ci	-17.1	95.5	-12.4	•	<u> </u>		ىت	-	9-8-	5.96
33	_	J- 96	-17-0 -11-	, ,	9	3	£	7.76	5-6-	9.96
36	7	6 70	7	,	-9-7	•	-8-1	•	0.1	7 7 8
25 C	ן ניין	92.9	-6.	*		95.2	7-7-	3.16	• (•
) K	8 9	E9.7	-8.0	4	~		101	•	, 41	. 🔊
. œ	0.9-	80.7	÷	0.76	∞ ≀		0 1	•	7	•
36	-5.1	19.6	S 1	~ (7.1-	•		3	-4.2	J
64	-5.3	81.5	\$		0 0		١ - ٤	3	-3.8	•
4.1	6.4-	1.43	•	V 4	7 5		•	6.54	1-3-1	•
42	4 (6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.00	7 4 6		, ,	ં		•	-2.6	۰ ب
43	4.0	0 0	• • "	. 4		٥		ġ	0°2-	ο·
77	0 F	2.0	• (•	-	~	~	* F	JF
40		43.2) (1	• ز.	-1.3	~	٠,	4°16	•	67.
C #) r	94.3		_	•	۲.	_ ,	-	ر ا ا	
1 1 1 1	9.0	64.3		2	•	93.1	-1.2	8.76	•	-

TABLE D-15 (Transient Data) (Cont'd)

		x	RECORD MAXIMUM PPESSI	2PF WALL	KULITE STEAD D = 154.3	Y STATE PR KILOPASCA	ECORD 2PF WALL KULITE STEADY STATE PRESSURES PRESSURES = 15.11	PSI		PAGE 4
•		;	acrit.	, 17	# UMUMU #	73.4	: CHCRD=	6.65	# CHORD=	141.4
SAMPLE		0 1		7 2 4 4	TAMCEMETAL	PMEX MA	TANGENTIAL	THAX IN	TANGENT I AL	KHAX IMUM
4 1 5 E	A TANGENIAL		TANCENT TANCE OF THE PARTY OF T			1 1 5 5 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0.500	PRESSU	(066.)	PRESSURE
						0		3.26	w\ • •	47.
67	7.	**	· -		• •	, ,		9	1.1	8.08
5	2.3	500	5.	5		• • • •				44.7
1,5	. , ,	,,4,,	1.6	7.5	æ •	7.56	•	100	• •	- d
	, ,	1 (6	3.6	6.4.5	1.4	64.7	u\ •	2.36	, . ,	۲۰۰۶
	, ,	, ,			œ.	3.00	۲۰۰	6.7.6	9°01	8° 3.
	- •	# · ·	; ,	7 3		46.7	2.4	57.5	> *	9.76
	-:						, 0	0.7	4	46.6
	ر. ح.	E - C d	 	7.45	C• 7		• •			~
	0	23.9	n) • •	7.5	6.7	15.3	2.3	_	• • •	•
		4.2.9	a)	7.5	3.2	46.4	7° • • • • • • • • • • • • • • • • • • •	7	0	· · ·
۵ ۱	, (1 1 1	44	6	7.5	96.1	4.5	•	۲.1	ر د د د
			. ,	,	42	2.36	۲۰,	•	٠,	8.75
	i) 0	2.	· ·				7		7.1	9,44
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OF FOUR COLUMN

MAXIMUM PRESSURE

COULS COULS

LABEL VALUE

2 0.930000€+02

3 0.880000E+02

4 0.790000E+02

5 0.720000E+02

6 0.850000E+02

7 0.580000€+02

8 0.510000E+02

104.3 KPa (15.11 PSI)

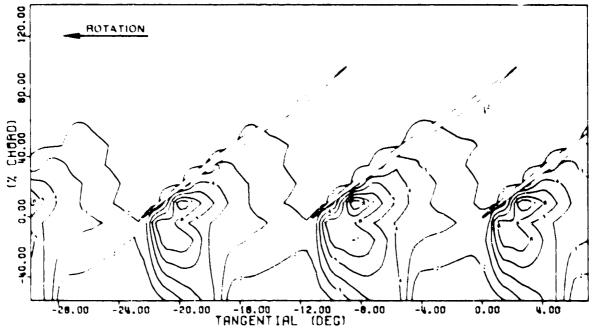


Figure D-10 Steady State Pressure Contours at Blade Tip; Transient Into Flutter, 70 Percent Speed, 59.8 Percent Flow, Pressure Ratio 1.300, Incidence to Mean Camberline 10.3 Degrees

OF PUBLISHING

TABLE D-16

STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS

70% SPEED

RECORD 25

Inlet Total Pressure = 80,100 N/m² (1673 lbf/ft²)

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
-55.4	1.258
-15.1	0.919
- 3.6	0.950
9.4	0.958
22.2	0.968
34.6	1.022
47.5	1.035
73.4	1.030
99.3	1.045
141.4	1.054

RECORD 25 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 98.3 KILOPASCALS = 14.25 PSI

		\ Cr ± .	
	677.04 17.06	0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	8 9 7 9 5 7 8 9 7 8 9 7
# CHCRD= TANSENTIAL (DEG.) -14.2 -13.4		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
9.4 TMAXIMUM PRESSURE 87.9 88.7	$m_N m_m m_N m_N m_N m_N m_N m_N m_N m_N $	66.24 7.88 7.88 8.5.4 9.5.6 9.5.5 9.5 9	
	これましいしゅうちょうちゅうけつ	- 1	A W W 4 4 4 4 4 7 7 1 F 8 9 5
SURE	F 0 4 4 0 0 E 0 0 0 E 0 3 4	5 F M 9 B 9 K F 5 S M R 7 9 5 7 1 1 9 5	60.00000000000000000000000000000000000
TANGENTIAL (DEG.) -14.2 -13.5		00000000000000000000000000000000000000	844666699999999999999999999999999999999
5.1 XIMUM SSURE 3.4 8.7		W B W 4 4 9 5 F B F 6 5 5 4 5 1 2 5 2	824000000000000000000000000000000000000
CHORD= NTIAL G.)	0.40.41111111 0.40.411111111111111111111	2 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	
IMUM SURE	647.5 688.6 687.5 687.5 688.6 68	11.00 17.00	
7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	112.1 112.2 110.2 110.3 10.3	0 - 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	40.00 40.00
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PAGE 2	1AL THAXIMUM PRESSURE 59.0 56.3 56.3 56.3 56.3 56.1 56.1 75.2 75.3	
	# CHORD= TANGENTIAL (DEG.) 14.1 14.6 15.1 15.1 16.3 16.3 16.3 16.3	
PSI	## ## ## ## ## ## ## ## ## ## ## ## ##	
CORD 25 WALL KULITE STEADY STATE PRESSURES RESSURE SAMPLED = 98.3 KILCPASCALS = 14.25	TANGENTIAL (0EG.) 11.0 11.7 12.1 12.7 12.7 12.7 13.6 14.6 15.6 17.1	
Y STATE PR KILCPASCA	AMAXIAUM PRESSURE 70.0 65.2 65.3 65.4 65.4 68.4 68.5 88.5	
KULITE STEAD D = 98.3	## CHORD= TANGENTIAL 10.4 11.7 11.8 11.8 12.4 11.8 11.8 11.9	
25 WALL URE SAMPLE	PM PMMA PMMA PMMA PMMA PMMA PMMA PMMA P	
RECORD MAXIMUM PRESSI	4 E CHORD= 4UM TANGENTIAL E 10.7 9 11.2 2 12.5 4 12.9 6 15.2 6 16.8 1 14.8 1 18.6	
I	24 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	
	TANGENTIAL (DIS.)	
	AN A	

RECCRD 25 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 98.3 KILOPASCALS = 14.25 PSI

ORD=	34.6	I CHORD=	47.5	# CHORD#	73.4	# CHORDE	0	T CHORDE	171	
×	T w	ENTIA	X	FATIAL	X	w	¥ a	ENTIAL	ZHAXII	
87.	,	4.2	9.4		• •	-14.2	0.88	-14.2	40° 50° 80° 80° 80° 80° 80° 80° 80° 80° 80° 8	
40		•	3	יי ריו יים		-13.7	8	•	•	
Š		3.		3	87.7	-12.9	8		B	
J.		2.	2	÷	•	-12.3	8	,	7	
n.		-11.6	93.	~	33.1	-11.4	£8.3			
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		:	- 1	0	•	٥	9.29		æ	
Α,		٠,	•	3		-8-3		٠		
~		'n	0°00	6	81.2		3°C	-5-1	S. 78	
~		3	٠O	-5.5	•		•	•		
<u>.</u>		ŝ	3	÷	•	-7.2		6*3-	-	
		•	æ	•	•	-6.5	•	9-7-	7	
~		,	÷	-8.2	•	6.5-		•	•	
		•	92.1	8.7-	93.9	1.4-	86.1	-5.8 8.3-	91.1	
·		m	93.		0.59	-3.5	•	-5.2	43.4	
÷		•	•	6.9-	•	-3.1		9.4-	5.0.5	
ς.			7.75	9.9-	•	-2.2		-4.2	67.4	
		•	4	1-5-	•	•	87.1	-3.6	86.8	
-		•	61.6	•		•	•	J.5.U	£ :: 3	
:		•	60.1	•	•	•	•	-2.4	91.4	
		•	e5.5	3	•	ن د د	•	-1.6	95.2	
:		•	72.1	6-6-	•		85.5	· 1 -	~	
:		•	9.69	-3.5	83.9	1.4	84.6	F 3	ė.	
•		•	9.69	-2.5	C. 50		83.3	6.7	,	IG F
•		•	•	9-1-	87.2	7.2	80.4	1.3	;	
•				-1.4	87.4		81.4	5. 1	'n	
٠.		•	6.17	<u>.</u> .		5.5	82.2	2-3	2	
٠.		•	•		80 (•• ,		81.3	0 °	۰	-
٠.		•	•	•		ဆ္ ₍	Э,	3.5	ر. د	
٠.			•	•		7.4	ъ.	.	G .	-
•		9	•			9.4	~ :	7.7	1.3	
• .		•		6.1	79.5	·	rJ I	7.,	4.5	15 1'Y
•		•	7.	2.3	_	จ	۳.	5.4	1.9	-
•			•	3.2	_	4.9	Š	æ5 •	:	
•		•	95.5	3.7		7.9	86.3	4.9	9	
•			9	•	84.2	•	66.7	3	16.5	
•		5	96.2	4.4	. •	9.5	J	•	ŝ	
•			Š	9. 4	,	10.1	ø	7.7	-	
•		ر	ä	9.	4	7	೨	8.2	2	
•		•	•	•	П	11.2	J	•	•	
•		_	85.6	•		12.1			e;	
•		12.3	9.1	7.7	۲.			9.6	63.7	
•		~		•			2		٠	

TABLE D-17 (Cont'd)
RECCRO 25 WALL KULTE STEADY STATE PRESS

		Ť	RECCRD 25 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 98.3 KII.OPASCALS = 14.25	Z5 WALL JRE SAMPLEI	KULITE STEAD D = 98.3	Y STATE PR KILOPASCA	ESSURES LS = 14.25	PSI		PAGE 4
SAMPLE	= CHORD=	34.6	CHOPD=	47.5	Z CHORD=	73.4	# CHORD=	00	- CHOODE	7 171
1UMB CR	R TANGENTIAL	THAX I HI	JM TANGENTIAL 1	EMAX14	IUM TANGENTIAL	EMAXIM	TANGENTIAL	ZHA X I M	TANGENTIAL	XMAY THIM
	(1) EG.)	PRESSU	(ufG.)	RESSU	(1066.)	PRESSU	(0)(6.1	PRESSI	(086.1	DEFECTION
	.4.3	79.5	12.9	76.5	16.1	97.8	12.4	82.7	1000	4.000
	14.0	77.9	13.2	73.5	10.7	86.4		9 6		100
	15.4	76.	12.5	72.1	11.9	81.3	1.4.	7.4		
5.5	15.5	13.4	14.5	77.8	12.3	81.2	14.5	P 3 5	14.1	77.6
	.5.8	74	14.6	6.69	13.0	(S)	14.9	82.7	1.4.5	76.3
	16.1	68.5	15.2	71.4	13.6	81.1	4.0	83.3	1 6 7	1 0
	16.2	70.5	15.7	74.2	14.3	92.6	16.2	64.3	3	7 × × C
	16.4	73.2	16.6	83.0	15.7	84.9	16.5	B5.2	16.4	74
	16.5	6.04	16.0	P3.7	16.2	P4.9	17.6	85.7	16.9	79.3
	16.9	83.6	17.3	83.7	16.8	0.23	17.3	e6.	17.6	75.4
	:7.6	85.3	17.9	86.3	17.7	64.7	17.9	96.4	10.0	74.4
	16.4	67.5	1a.4	90.2	18.4	84.8	18.4	96.6	7 8 6	7 26

Or Po

% MAXIMUM PRESSURE
CURVE CURVE
LRBEL VALUE
2 0.930000E+02
3 0.860000E+02
4 0.790000E+02
5 0.720000E+02
6 0.850000E+02
7 0.580000E+02
8 0.510000E+02

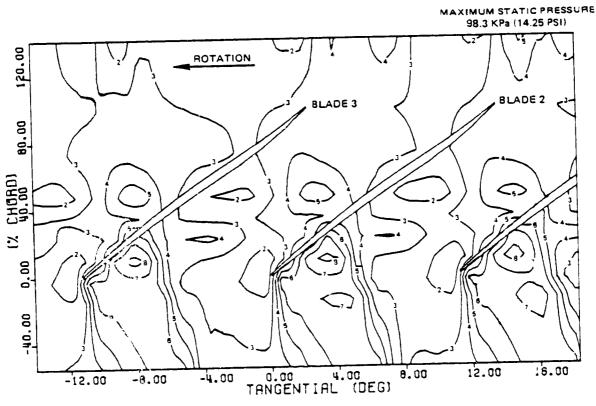


Figure D-11 Steady State Pressure Contours at Blade Tip; No Flutter, Low Operating Line, 70 Percent Speed, 72.8 Percent Flow, Pressure Ratio 1.2280

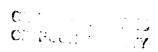


TABLE D-18

STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS

70% SPEED

RECORD 133

Inlet Total Pressure = $86,140 \text{ N/m}^2 (1799 \text{ lbf/ft}^2)$

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
· · · · · · · · · · · · · · · · · · ·	
-55.4	0.952
-15.1	0.954
- 3.6	0.957
9.4	0.973
22.2	1.061
34.6	1.108
47.5	1.128
73.4	1.152
99.3	1.171
141.4	1.161

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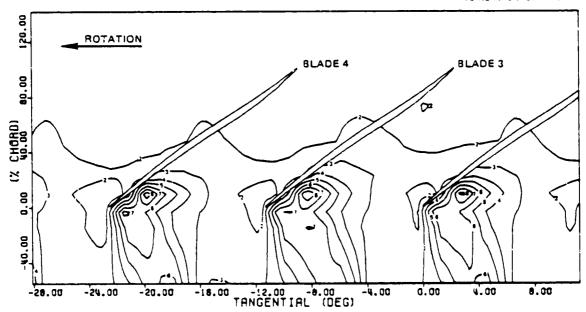
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•	PRESSURE	84.7	•
 | 69.7 | ာ့၊ | | | 2.5
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د د د د | 3°74 | · · ·
 | 7.78 | J | ۱۵ | • : | • : | , ,
 | ı. |
| * CHURD | ANGEN 12
(066.) | -28- | -27.0 | -25.9 | -24.7 | -73.5 | -22.4 | -21.3 | -21.1 | 2°01- | -17.7 | -16.6 | 7.5.4 | -14.3
 | -13.1 | -12.0 | -10.8 | 9.5- | -8-5
 | -7.7 | -6.1 | 6*5- | 3•દ− | -2.6
 | -1- | ٠٠
۲ | ٠, | 2 •. |
 | 7-7 | 5.¢ | 9.7 | | ۶, | ٠,
 | -4 |
| _ | PRESSURE | 79.6 | 86.3 | 91.5 | 94.5 | 7.95 | 300.0 | e
B | 45.4 | 61.4 | 71.7 | 8) • 1 | 86.2 | 91.0
 | 93.7 | 7.96 | 93.5 | 76.4 | 45.9
 | 53.1 | 72.4 | P.i. 5 | 86.4 | 3
 | 95.6 | 6.95 | (r) | • | m
 | Ð | _ | P 4 - 9 | ಎ•63
ಕ | 93.2 | •
 | ۲.
م |
| • | ⋖ | 2020 | -26.9 | -25.8 | -24.7 | -73.5 | -22.3 | -21.1 | 6.61- | -18.8 | -17.7 | -16.5 | -15.4 | -14.1
 | -13.0 | -11.8 | -10.0 | 5.4- | 7.8-
 | -7.2 | -6.0 | 6-4- | -3.7 | -2.5
 | -1.4 | 0.2 | J. C | 5. 8 | e.
 | 7.7 | 9.6 | ۍ د | ٠
٠ | O | ċ.
 | 11.4 |
| | | 8 78 | 1 1 | ٠ ٣ | • | 95.1 | | 55.00 | 63.9 | | B(1.7 | 85.3 | 86.9 | 8
 | - | | | • |
 | • | 77.5 | 9.48 | 86.5 | 67.6
 | 90.1 | 9.46 | 52.7 | • |
 | 8 | 64.0 | • | • | ė. | Š.
 | 86.6 |
| CHORD= | NGENTIAL | | 1-07- | -25.8 | -24.7 | -23.6 | -22- | -21.5 | -20-1 | -1 P.9 | -17.7 | -16.5 | -15.4 | -14.3
 | -13.1 | -11.6 | -10.4 | 7.6- | -8 .4
 | -7.5 | -6.1 | 6.4- | -3.7 | -2.5
 | -1.4 | 4-0- | 6.0 | 1.9 | 3.3
 | 5.5 | 5.6 | 6.7 | 4.9 | 10.2 | 10.8
 | 11.4 |
| -15.1 | EMAXIMUM
501001001 | FAE 350'AE | ; 0 | ; ; | | • | 0 2 | 6.0.4 | 53.0 | 7.10.3 | 8.2.65 | 85.5 | 8.00 | 90.1
 | 61.2 | 94.1 | 77.8 | 61.3 | 57.2
 | 62.1 | 75.0 | 3 | 4.68 | 89.5
 | 91.7 | 93.4 | 61.9 | 59.8 | 61.6
 | 75.8 | 3 | - | 6.63 | 61.0 | 3
 | 89.7 |
| ₹ CHOR | TANGENTIAL | 10 FG . 1 | 1.82- | 6.00 | 2.62- | 193 | 255.2 | -21.2 | 3. 7 - | • | -17.6 | -16.5 | 6.61- | -14.2
 | -13.0 | -11-6 | | 6.6- |
 | -7.2 | 0 0 | 6.4- | -3.7 |
 | -1.4 | -)•3 | 1.3 | 7.4 | 3.3
 | 4.4 | 5.1 | 5°4 | 7.99 | 9.1 | 16.7
 | 11.4 |
| -55.4 | HAXIMU | RESSUR | . | 7 r | | | ъ. | റ | 3.0 | 3 4 | • | | ·u | ٠.
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| CHORD= | ANGENT | 0.50 | 3 6 | • . | 9 2 | | ') (| " | 7 ? | <u>،</u> و | ם ב | | 4 | ` '
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 | C . | ≯ ∪ | <u> </u> | 2 - | - 6
 | 2 0 | , , | ` [[] | 1, | , ,
 | 76 | , , | 2,4 | | . 6
 | . 6 | , e | 31 | 3.5 |) (M) | 36
 | 35 |
| | E T CHORD = -55.4 T CHORD = -15.1 T CHORD = -3.6 T CHORD T SUCCESSION TO CHORD TO CH | T CHORD = -55.4 T CHORD = -15.1 T CHORD = -3.6 T CHORD = 9.4 T CHORD = GENTIAL THACENTIAL TANGENTIAL TANGENTAL TANGENTIAL TANGENTIAL TANGENTAL TANGENTIAL TANGENTIAL TANGENTAL | E CHORD= -55.4 % CHORD= -15.1 % CHORD= -3.6 % CHORD= 9.4 % CHORD= 22.3 % CHORD= 2.4 % CHORD | ### CHORD= -55.4 | ### CHORD= -55.4 | ### CHORD= -55.4 | E CHORD= -55.4 | TANGENTIAL TANGENT | TANGENTIAL TANGENTY TANGENT TANGENTY | TANGENTIAL THAXIMUM TANGENT THAXIMUM TA | THORNIAL THANGENTIAL THANGENTAL THANGENTAL THANGENTAL THANGENTAL THANGENTIAL THANGENTY | THOUSE TECHORD= -15.1 THOUSENTIAL TANGENTIAL TANGENTY T | TANGENTIAL TANGENTY TANGE | TOTAL THANGENTIAL THANGENTY THANGE | TUCHORD= -55.4 TO CHORD= -15.1 TO CHORD= -3.6 TO CHORD= 9.4 TO CHORD= 22.2 TANGENTIAL THAXIMIH TANGENTIAL THAXIMUM TANGENTIAL | THOUSEN THE THAXIMUM TANGENTIAL THAXIMUM TANGENTY TH | TCHORD= -55.4 \$\frac{2}{3}\$ CHORD= -3.6 \$\frac{2}{3}\$ CHORD= -3.6 \$\frac{2}{3}\$ CHORD= 2.2.2 \$\frac{2}{3}\$ CHORD= -3.6 \$\frac{2}{3}\$ CHORD= 2.2.2 \$\frac{2}{3}\$ CHORD= -5.4 \$\frac{2}{3}\$ CHORD= -5.6 \$\frac{2}{3}\$ CHORD= -5.7 \$\ | THOUSENTIAL THORNER 110. THORNE 9.4 THORNE 22.2 THOUSENTIAL THANTHUM TANGENTIAL THANTHUM TANGENTY THANTHUM | THOUGHTAL THANKININ TANGENTIAL THANKININI TANGENTY TANG | THOUGHTAL THAXIMUM TANGENTIAL THAXIMUM TANGENTY THAXIMUM TANGENT | ## CHORD= -15.4 ## CHORD= -15.1 ## CHORD= -3.6 ## CHORD= 9.4 ## CHORD= 22.2 ## CHORD= -15.1 ## CHORD= -3.6 ## CHORD= 10.5 ## CHORD= -3.6 ## CHORD= -3.7 ## C | THE TECHNOL -55.4 TO CHORD= -15.1 TO CHORD= -3.6 TO CHORD= -3.7 TO | THE THORNER55.4 TO CHORD = -15.1 TO CHORD = -3.6 TO CHORD = -3.7 TO CHORD | THE TECHORDS55.4 TO CHORDS - 15.1 TO CHORDS - 3.6 TO CHORDS - 3.6 TO CHORDS - 15.1 TO CHORDS - 3.6 TO CHOR | THE TECHORDS = -55.4 TOTAL TANKENTIAL THE THATHUN THANKENTIAL THATHUN TANKENTIAL THATHUN TANKENT THATHUN TANKENT TA | ## CHORDS = -55.4 | T CHORD= -55.4 T CHORD= -15.1 T CHORD= -3.6 T CHORD= 9.4 T CHORD= 1.5.1 T CHORD= -15.1 T CHORD= | The control of the co | THE TECHORDS -25.4 TOTAL TAYLOR | THE THANKING THANKENTIAL THANKENTIAL THANKENTIAL THANKING THE THANKING THANKENTIAL THANKING THE THANKING THANKING THE THANKING THANKING THE THANKING THANKING THE | THE THE THANKING THANKENTIAL THANKENTIAL THANKING THE THANKING THANKENTIAL THANKING THANKENTIAL THANKING THANKENTIAL THANKING THA |

TABLE D-19 (Cont'd)	

		I	RECORD MAXIMUM PRESSU	133 WALL URE SAMPLE	CORD 133 WALL KULITE STEADY RESSURE SAMPLED = 164.3	Y STATE PRESSURES KILOPASCALS =	ESSURES LS = 15.11	PSI		PAGE 2
Jahr	HOR	34.6	CHOR	47.5	₹ CHORD=	73.4	% CHORD=	99.3	Z CHCRD=	141.4
NUMBER	CENTIA	THAXIMUM	TANGENTIAL	THAXIMUM	TANGENTI		_	2	TANGENTIAL	KX IMU
	nFG.	RESSUR	£ G•	Ŗ	0	PRESSURE	(DEG.)	PRESSURE	(DEG.)	PRESSURE
-1	2	24 60 90 90	a)	95.8	-2	94.3	-25.1	9	o١	ن. ای
Ç.	,	5.06	۲.	6	27.		-27.1		•	
m		01.7	•	\sim	8-52-	95 .4	-25.8	9	-25.8	95.2
1	4	93.6	4	,	-24.6	96.5	-24.7	6.96	-24.6	
5		93.P	, 1		٠.	97.1	-23.5	47.3		
•		63.9	2.	96.3	~	94.1	-22.0	97.5	2	•
7	-21.2	93.7	-	-	-21.2	95.3	-21.2	4.1.6	-25.8	96.2
σ'n	2	42.7	٠			96.1	-21.2	6.96	-	
σ	- 1	92.3	-18.9	7.46	Œ	•	-14.2	•	8	95.6
1.	7	8 b 3	7.	. *	7	45.7	-17.6	86.38		
11	-14.5	69.3	3	ζ.	-16.5	45.4	-16.5	96.A	-16.5	45.2
12	3	ا ن ا	۷,		٠ د ي	95.3	-15.3	6.96	Š	94.2
13	7.	91.4	3	•	-14.2	95.6	4	6.95	-14.2	51.2
14		95.6	.71	,	-12.9	96.5	-13.0	97.2	-: 3.2	1.26
1.5	-11.9	43.2	2	64.7	-11.3	93.4	-11.9	97.3	-11.6	96.2
16	-1:-1	93.3		•	-16.5	93.P	-16.7	97.3	-16.6	45.3
1.1	5.6-	6.5°	Ġ	4	9-6-	64.3	6.8-	90.06	-10.(95.3
19	4.8-	61.7	æ	3		6.46	-£ ,2	9.95	-3.8	96.5
61	1.5.	6.06	-	۲٦	•	95.5	-7.2	90.1	-7.2	2.74
50	0.4-	86.2	•	•	-6.1	95.1	-6.2	96.1	0.0-	92.2
2.1	6.4-	J. 9 9	•	67.2	6.4-	95.3	-4.8	96.2	6.4-	95.2
22	-3.7	7.68	•	•	-3.7	95.8	-3.R	9.95	-3.7	45.6
23	-2.5	5°05		~	-2.6	o	-2.6	8.96	-2.6	•
5.4	4.[-	85.2	•	'n	-1.7			47.3	-1.4	i ai •
2.5	-0-5	45.48	•	3	0°0	\sim	-0-5	5.75	•	
3¢	6° Ū	92.5		94.2	٥•	65.3	6°)	97.6	6°)	9.16
27	7.1	95.3		6,1	2.1	*	٠	96.36	6• •	96.5
23	3.7	95.00	•	m	3.4	5.	3.2	4.76	3.6	6.96
53	4.4	91.0		~	4.4	S		•	3.9	1.56
33	5.4	87.6		\sim		S	5.5		5.4	96.3
16	6.3	8.68	•	٥.	9.9	•	6.7	•	•	4.46
32	7.0	91.2	7.3	92.3	1.9	95.4	7.7	96.3	7.9	
,33 53	9.1	92.3		.~	•	ø	J. 4	•	•	45.8
34	13.42	43.64	•	•	6	9.96		97.2	10.2	9c.96
5	4.1.	43.4		95.6	11.4	93.3	11.4	•	•	97.7

% MAXIMUM PRESSURE CURVE CURVE LABEL VALUE 2 0.930000E+02 3 0.8800000€+02 4 0.790000E+02 5 0.720000E+02 6 0.650000E+02 7 0.580000E+02 8 0.5100000€+02 MAXIMUM STATIC PRESSURE

104.3 KPa (15.11 PSI)



Steady State Pressure Contours at Blade Tip; In Flutter, High Operating Line, 70 Percent Speed, 59.8 Percent Flow, Pressure Ratio 1.3004 Figure D-12

ORIGINAL PAGE IS OF POOR CONTY

TABLE D-20

STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS

70% SPEED

RECORD 220

Inlet Total Pressure = $87,000 \text{ N/m}^2 (1817 \text{ lbf/ft}^2)$

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
-55.4	0.962
-15.1	0.957
- 3.6	0.962
9.4	0.988
22.2	1.056
34.6	1.098
47.5	1.120
73.4	1.158
9 9. 3	1.180
141.4	1.165

RECORD 220 WALL KULITE STFADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 118.7 KILOPASCALS = 17.20 PSI TABLE D-21

					# CHORDS	-3.66	₹ CHORD*	5. 6	T CHOR	22.2
SAMPLE	CHO	-55.4	E CHUKUF	PMAY I MIN	ENT I AL	X	Z	×	EN	Ϋ́
NUMBER	TANGENTIAL	FORTYPE		• 1	(056.)	SUR	ut G.	ESSU	(DEG.)	74.55UR
,	1016.1	5 ~	٠.	75.4	27		٠	ή.	٠,) · ·
-	9.17-	, t	•		26.		.•	_	٠.	7.00
~ ′	9.05-	10.1	• •		24.		•	•	۸,	1.00
η.	* c		' '	ੁ•	23.	•	•	•	•	
1 .	5.5.7	7.76	-2.8	81.5	-23.3	•	•	98.3	7.5.7-	7 · · · · · · · · · · · · · · · · · · ·
i	G (()	70.5	•		22.	:		7.46		
u [*] F		9 - 1	•	_:	22.	•	•	•		
- 0	10.7	60.2	•	,	å		•		4	1.11
1) (- r	7.05		~	21.	_	-23.5	٠,		
.				41		54.0	•	•		•
- ,	n 4	7		5	21.	÷		•	•	_
11	n	1 4 6 7			20	نه	-26.6	28.4	<u>, </u>	•
C: (2 t	7		•	ċ	\sim	\sim	ġ	· •	•
- 13	6-11-	יין ר ר	• :	_	6	-	•	•	· .	۲۰ ۲۰
·* :	1.1.	1305	•		8		m	•	•	• • •
51	-11.3	73.0	• •	, 4	•	4	~	0.79	٥	
16	-16.8	7.0			3	6.	~	•	5	.
	-16.2	1	٠.		-13.3		•	٠	*	,
en 	4.01-	n 0			·N	P1.5	•	•	Ν.	;,
13		۲۰۲۱	·	77.7	_		\sim	. 15	-11.3	٠,
. ~			•	,	· · ·		~		•	5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
21		5.01			6		•	•	₽.8 −	,
22				, ,	9	å	-16.2		٠.	٠.
23		0.27		•	6	Ψ,	Ŷ	•	انت	•
24	62 6 5- 6	> 10			0.6-	55.9	L-6-	41.3	-	;
5.2	ນ · ນ ເ	1.70	0	, ,	α,	ی	5.6-	٠	-	•
20	-1 · 6	7 · E ·			T. L-	•	•	24.2	•	•
27			• •	,	•	•	•	٠٠ ٠	;.	•
¢i (0-1-	7 6 7		2.75	-6-1	•	7 B	17.1	4 1	•
56	4.9-	2.00			-5.5	71.8	9•8-	_	'n.	•
G (301	7 6 6 7		•	4.4-	•		-^	;	•
31	n •					•	•	3 (•	•
C) (0.0	6 74	7-4-			•	-5.5	ന	•	•
47 F	? C	7.5.6	-2-1	17.9	-1.2		5. 5-	16.1	7•7	
P 40	2 4	75.	-1-3	6		J	٠,	თ :		•
C 6	7 1	74.9	9 ° 0 −	•	0.2	Š	~ ,	= 、	•	•
) 		75.6		3	•		- (- (• 0	•	•
- 0	-	76.0	ن•٦	•		4	• .	•	•	, ,
0 0	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	74.4	e. ⊙	Š		ď.	4.1	7.7		٠. (
.		79.1	1.0	54.9		Ġ	· -	• •	•	. =
7		45.6	1.7		2.2	Ė	٠. - (٠.	•	,
1 .	4 6	6263	2°U	•	•	•	7 - 7	•		• 4
`, C	, r	67,22	2.6		3.5	•	•	•		•
	, ,	7-55	3.4	3	•	ī	7 · F	• ,	٠	
; .	. 4	4.4.4	7,04	_	5	ζ.	•	.	•	
() ()	•	4 6 7		Š	1.1	14.7	4. N			٠ د
9!	٠. •		. d	2	٠,	7.97	L. 9	۵	· .	6.76
4.7	- · ·	•	- 4 - a	. ~	7.6	ည	6. b	ġ	•	
4 .	7.	•	F • • • • • • • • • • • • • • • • • • •	•						

JO POUR QUALLE

				L	TABLE D-21 (Cont'd)	Cont'd)					
		1.	RECORD MAXIMUM PRESSI	220 WALL URE SAMPLE	CORD 220 WALL KULITE STEADY STATE PRESSURES RESSURE SAMPLED = 118.7 KILOPASCALS = 17.20	Y STATE PR KILOPASCA	ESSURES LS = 17.20	PSI		PAGE 2	
u - 0	# C # C # C	15.5	% CHORD=	-15.1	2 CH0PD=	-3.6	# CHORD=		2 CHORD=	22.2	
יינו שור ביינו אור ביינו	TANGENTIAL	I X V NZ	TANGENTIAL	ZMAXIMUM	TANGENTIAL		TANGENTIAL	•	TANGENTIAL		
	() () () ()	S S a M C	(086.)	PRESSURE	(DEG.)	PRES SUR E	(DEG.)	PRESSURE	(066.)	PRESSURE	
07		4/	5 3	79.4	10.7	81.2	15.2	93.9	12.8	E4.7	
	7 4	. 72			11.0	A1.6	11.1	98.1	13.5	84 • 2	
	, ,				11 .4	78.2	11.5	59.3	14.1	£1. • 9	
4 6		7 6	4		11.8	72.9	12.5	86.6	14.5	76.3	
, ;			12.2		12.3	59.0	12.9	9.01	14.7	73.1	
C 4		9 4	12.5		12.4	6.99	13.1	59.6	14.8	11.11	
, 4		2 7	5.01		12.4	56.0	13.3	51.9	15.0	69.5	
1 4			7 6 1		13.0	59.6	13.4	45.4	15.1	68.2	
) h	0.01		7 0		13.2	61.1	73.66	42.2	15.3	67.7	
- 6	¥ 7 [7.7:		13.9	65.1	14.7	47.5	15.6	69.7	
	2 - 4	, ,			15.4	1.69	15.2	51.7	15.7	64.5	
6.0	0.91	6 3	200	9-69	16.0	70.6	15.5	53.7	16.0	70.2	

ORIGINAL PAGE IN OF POOR QUALITY

RECORD 220 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 11P.7 KILOPASCALS = 17.20 PSI

																			,					• •	(,		•		· 5																	
	E5.2		.n .	۲. ۱۰	•	•	٨,	^ '	ζ.	85.2	47	so.	64.7	• ! •	•••	• • •		Λ,	ŋ.		٠ د د د		0 r		o 4	9	· ~	. 60	5.9	86.2	٠.	J		ς,	n.	Λ,	Λ.			n ,	Λ,		٠ م <u>ـ</u>	47 4	S	9. • • •
CHORD= NTIAL S.)	•	-25.5	-75.2	7.4.4	7.7.	1 • 7 7 -	1-22-	-20.9	7 • 1 /-	S.	a 1	-18.c	~	5.51-	-14.4	-13.7	8 - 2 -	-11-	6.01-	٠,١٠٥	7°6-	1	5-1-1	-7.1	ς - 3	4 a	· 1		~	-2.4	-2 • i	-1.3	E • ,	4 ,	1•1	9.1	7.7	2.7	# 6 n 6		5.6	2.5	6.9	7.6	9 .	
	85.8	S	86.1	ġ.		- 1	_	86.9	-	_	ġ	9	86.3	66.1	86.2	96 • 2	86.5	66.7	8.4 9.1	86.7	87°C	8.0	36.3	66.5	αο ω «Γ. ω αο α) 4) 4) 6	١ ٧		Š	86.3	•	•	Ġ	~	•	•	•	. ė	0.98	٠.	•	۵	9	Ş	4.04	86.6
₩ ₩~	-27.5	•	æ	-25.3	•	\	,	٠ د	_	-19.6	-18.7	•	-17.4	•	wn.	-15.3	4	-14.1	-15.4	-12.6	~	J	به	-6.2	0.4	o 4	٠,	7 0	, ~	· 'N	-1.9	-1.2	?•°€	1.1	7.7	2.6	5.9	4) (7.4	، 4	w) ·	4-9	9°E	B. C.	٠.5	
3.4 XIHUM SSURE 4.6	4	85.2	u-		• •	•	3.	,	Š	65.5	Š	•	9	١	Š	ŝ	•	•	•	1.98	٠	۲.		•	s.	•	8,		٧,	9.5.6	•	86.4	2	4.	>	8 j • 9	~	0.48	S	\$	S		S	S	65.6	
CHORD≈ ENTIAL EG.)	27	26	٠.	S	, s.	2	22	\sim	_	-20.B	\sim	ᢐ	-1845	-17.8	~	92	-15.4	-14.7	-14.5	C)	-12.5	-11.6	•	-10.4	60 (60 (E	۵ ،	16.2	١ ٧	9.6-	-3.2	-2.4	-1.6	<u>-1 • ن</u>	5.7	-u-	9-0	1.3	7.7	3.4	4.1	ر. ۲• ن	6.2	7.0	ر. ف	3.5
7.5 XIMUM SSURE	1.11	78.4	73.5	8. s	e 1 • 8	83 . 0	83.R	£4•3	,	٠,	84.6	64.4	0.48	83.1	61.9	8 7	19.4	മ	B	79.2	-	e 3	~	^	. ·	η.	7. 6.	00 00 00 00 00 00 00 00 00 00 00 00 00	, ~	83.3	· ~	ന	-	٥	Ð	٦.	4.02	;		۲,	<u>«</u>			1,4		a)
# 55 O			26.	÷.	25.	,	23.	2.2	21.	:	19.	16.	17.	۲.	16.	j	ं	J	۷,	ď	·	•	•		٠.			. u	۰		• •	•	•	4			•	٠ <u>٠</u> ٠		•	•		•	5.4	د.،	
34.6 TMAXIMUM PRFSSURE	• •		•	•	:	:	•	<i>-</i> :	•	:	•		:	•	•	3	•	٠	_:	÷			m3	~	٠.	٠.	a.,		٠.		1 -	ر به	_	.=	٠.	~	٠,	~	_;	å	~	:	()	A	7	•
TANGENTIAL (DEG.)		7.	. 77	73.	55	21.	21.	15.	a)	17.	17.	17	۲.	Ý		۰	. •		12.	•	11.	٠			1-6-		•	•	٠ • •		• 4	۱٦,	_	٠-,	•	•		3.3	•	•	•	٠		6.5	•	(a)
AMPLE	- ^	ı m	7	۰	o	7	æı	•	٦٢	11	12	13	14	51	91	17	0;	0	5.3	2.5	2.2	23	72	5.8	5.6	2.7	23	53	<u>.</u> .	., e) r	36	. K.	3.5	37	39	39	0,	17	25	43	41	4.5	45	4.7	6. 1

TABLE D-21 (Cont'd)

		1	PRECORD 220 WALL KULITE STEADY STATE PRESSURES MAXIMJM PRESSIJGE SAMPLED = 119.7 KILOPASCALS = 17.20 PSI	220 WALL JRF SAMPLE	KULITE STEAD D = 119.7	Y STATE PR	ESSURES LS = 17.20	PSI		9 4 4
אם רע א	±C#CHJ ≱	34.5		47.5	#000H0 #	73.64	=04CH3 \$	6.99	TANGENT AL	141.4 7MAX 14
or u	TAITHTOTAL ST	MANIMAN POPULATION	TANGENITAL THANHAM	でする 1 mm 1	14455-4114C (555.)	こういい	(DEC.)	PRESSURE	(050)	1000 Jan
,		7		77.5		5.18	ۍ• د	26.50	10.1	5.63
	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	F 1 2		77.7		0.00	11.2		110.	165.7
, ;;				73.3	10.3	7.50	11.9	67.5	:::	P. C. S
• 1		, d.		7.4		84.1	12.6		11.5	v.
, ,	7.6	7		•		63.2	13.5		55.6	9.4
\ \	12.3			1919		92.9	39 · 61 · 4		12.7	25.7
) 				4.76		6.5.4	14.1		12.9	60
, 1	7	, n		.:\ a:		1.50	14.4		13.4	4.0.7
	14.2	יש יים יים		E4.1		65.3	5.71		14-1	۳. ۳.
. e.	5 9	ים מי		54.5		7	15.64		14.7	65.7
	6.5	6, 73,		34.1		80 7, 7,	15.7		15.0	3.
· ·	7 9 (, 10		6		4. 70	4.04		N. W.	E5.7

OF FLOR

% MAXIMUM PRESSURE CURVE CURVE VALUE 2 0.990000€+02 3 0.860000€+02 4 0.790000E+02 5 0.720000€+02 8 0.850000E+02 7 0.580000E+02 8 0.510000E+02 9 0.440000€+02 10 0.370000€+02 11 0.300000000000 12 0.230000E+02 MAXIMUM STATIC PRESSURE 118.7 KPa (17.20 PSI) ROTATION BLADE 2

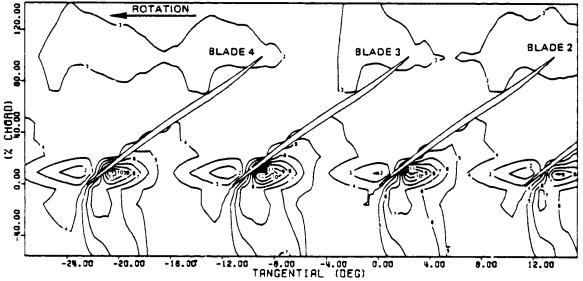


Figure D-13 Steady State Pressure Contours at Blade Tip; High Operating Line, 70 Percent Speed, 56.5 Percent Flow, Pressure Ratio 1.2978

TABLE D-22

STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS

73% SPEED

RECORD 92

Inlet Total Pressure = $79,960 \text{ N/m}^2 (1670 \text{ lbf/ft}^2)$

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
-55.4	0.911
-15.1	0.911
- 3.6	0.938
9.4	0.961
22.2	0.971
34.6	1.024
47.5	1.051
73.4	1.059
99.3	1.074
141.4	1.086

RECORD 92 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 102.5 KILOPASCALS = 14.85 PS

SAMPLE & CHORD= NUMBER TANGENTIAL (PEG.) 1 -29.5 2 -28.9 3 -23.2 4 -27.4 6 -27.5	7 49			6000	~		4.0	A CHURCH	•
TANGENTIAL (PEG.) -29.5 -28.9 -23.2 -27.4 -27.4			ŝ	* CHUX	•	TUDEN TO		CMT	3
(DEG •) -29.5 -28.9 -23.2 -21.1	AXI	ENTIA	ZHAX I HUM	SFR	ENAXINUM BD 11 C C 10 F	11 14	PRESSURE	(DEG.)	ESS
0 00 00 L L L	RESS	ٔ ق	RESSUR	1056.	֡֝֓֞֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֡֓֡	29.5	54.7	•	L* 59
80 22 77 7	•	÷.	9.00	, 0	6,64	28	S	\$	-
21	•	•	0.40	•	74.0		_		å
-	•	•	3.70	•	6-18	2 7	85.0	-28 · I	76.5
	•	•	Ø 7• C	• (-	6.4	Š	•	•	ż.
_	•	3	1 - 1 9 6	- 4	86.9	24	6		æ
			5 (2)	9 7 6		23	~	•	. ,
40	•		80.5	•	7 70	•	-0	•	'n
40	•	4	600	2	200	7	- 0	•	ċ
'n	•	۳.	6.18	•	•			•	•
4	•	? ? •	91.6		- C	•	52.5	•	•
	•		88.3	_	۶. د د د د	6 3 6	7-67	•	•
4	•	21.	8.5.8	-	7.00	•	8 77	•	•
٠,		٠ د	62.7	Э.	2.19	י ני	•	•	
	•	2	61.5	=	59.3	6-17-	***	• _	
7	•		62.0	J	59.5	-	23.5	F • 6 1 -	-
	•		56.7	a.	57.2	Û	56.5	J. 6.	-
-21	•	•	7-95	Q,	57.4	-16.3	5.8°C	F. 2	•
.6-	•	•		•	56.3	•,	58.6	-18.5	-
-19	•	7.07.	7 · C · 7 · I		57.3	-14.5	63.3	7.81-	
~	-	•	2006	, 4	4 4 4 6	-3	72.9	-17.4	_
۲-	_	-101-	0.00	١u	6.00	-13.9	83.5	-14.2	
• •	-	•	* :	1 W	75.64	ייו	87.1	-15.7	_
-		٠	200	, 4	0.08	~	88.8	-15.4	
1.2		•	0 0	,	· · · · · · · · · · · · · · · · · · ·	_	69.66	-15.2	
		•	7 1 10	7,1	88.2	-10.8	93.0	-14.8	•
_		٠	0 0		91.2	_	8.76	-14·ú	_
_	_	•	7 - 60	• -	45.7	ு	84.4	-15.0	
		•		-	4-16	-9.5	78.0	-12.2	•
_	_	•	n 0		20.00	-8-3	56.6	-11.7	•
		•	4.55	<i>-</i>	59.1	, ,-	52.9	5.)	
	_	•	0.00		4.19	-	48.7	6.5-	
	_	٠.	0.4.0		54.9	- 1 -	47.8	-B-9	•
_	-	٠.	n 4	_	61.2	1.9-	50.5	-8-5	٠.
-7.8			63.3	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6.09	6.4	55.3	-5.2	•
-7.2	-	• .	7.04		65.3	-5.7	58.8	- 0	٠,
-6.5	• • •	•	7. K	-6-3	0.09	-5.0	15.1	-7.7	.
		•	0 ec	-5-7	62.0	7.5-	80.6	٠٠٠	•
6.4-	-	•		9.5-	6.49	-3.6	83.0	-7.3	
-4°5	1.09		, c	6.4-	19.9	7.1-	87.4		63.1
-3.7	. .) e	-4-5	83.5	-0-1	91.4	1.5-	•
ν.	Λ.		9 6		85.5	1.1	74.1	2. S.	φ.
6) ((0) (-n 1		7 4 4	5 -	61.9	1.4	89.1	-4.5	۵.
3.5-	~ ~		54.5		95.8	1.9	81.7	-3.7	٠.
8.2-	11 6		L	7.0-	4.56	7.7	71.1	-2.8	۰ ۵
9	2		0 76	-0-	96.3	3.1	50.5		٠, ,
٠,			104	100	63.1	3.5	53.4	6 · ·) -	ວ• ເລ
e. [-			· 6) (F)	59.0	0.4	•	5.0-	87.4
-1.2	m		6.70		7.64	4.4	Ġ	0.0	4.88
•	~		6.29	1.1	•	•			

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E D-
E D-
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	2	:	E (u															
	PAGE 2	22.2	ZMAXIMU	PRESSURE	93.4	75.3	68.3		70	26.4	58.4	58.7		100	69.5	74.1	76.5	F. J.	
		CHORD=	TANGENTIAL	(DEC.)	1. 0	2.9	5,46	, ,	7 • 0	. 4.I	F • 4	7	1	0	6.2	6.7	(°		1.6
	PSI	4.6		PRESSURE	54.2	59.5	63.54		٠٠,٠	15.6	90.08	70	•	2.08	85.9	86.5	87.0		0.10
	SSURES S = 14.85	T CHOKD=	TANGENTIAL	(DEG.)	5.2	\$°	4) : •	٤.3	7.1	7.4		ن -	ن ت	8.3	9 9	7) (٧•٥
(D)	STATE PRE KILOPASCAL	-3.6	IAXIMUM	PRESSURE	60,09	61.6	a 0	0.40	28.1	58.6	4, 67		07.0	67.3	82.8	85.0	4) f) • (B)
IMPLE U-23(LONED)	ECORD 92 WALL KULITE STEADY STATE PRESSURES PRESSURE SAMPLED = 162.5 KILOPASCALS = 14.85 PSI	I CHORD=	TANGENTIAL	(DEG.)	2.4	9.6	, n	• • • • • • • • • • • • • • • • • • • •	4.1	5.0	- C	•	£.4	8.9	7.4	7.7	. 7	r (0
¥	92 WALL K	-15.1	ZMAXIMUF	PRESSURE	61.0	, 4 , a , a		53.5	58.4	57. A		2.1.0	62.4	8 3.4	83.0	6 4 9		* 100	6.78
	RECORD MAXIMUM PRESSU	ORU=	TANGENTIAL	_			0 (7.4	5.5	7	•		7.5	6.2	 	3	, (7.6	7 0
	Ĩ	-55.4	ZMAXIMUM	PRESSURE	- C - C - C	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		78.4	0.14	. , ,	1 • • •	61.9	4.09	4.04		7		69.5	44
		# CHORD=	TANGENTIAL	(066.)		• •	۲•۰	1.6	3-6			6.7	6.1		- 0	ت ن ن	\$ (٥.	
		RIGHTS			,	* 1	Ę,	51	,	1 6	5 .	24	55	7 3	0 6	- (en Liv	59	

TABLE D-23(Contd)

RFCORD 92 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 102.5 KILOPASCALS = 14.85 PSI

141.4 EMAXIMUM BASS STUE	Kr>50 84.5	•	62.9	•	•	•	\$ • • • • • • • • • • • • • • • • • • •	71,0	0 ° 6 0	7.00	D • F	0 f	- 0	* * * * *) () () () () () () () () () () · · · · · · · · · · · · · · · · · · ·		C 7 9	3,6	7 8) · · · · · · · · · · · · · · · · · · ·	7.76	0 0	6.44	4 4 6	2.4.3	2.48	64.5	1.55	F.5.7	0.49	85.6	E 4 . 7	84.2	E 4 • 3	9.78	6.49		P5.7		ň.	Δ,	1.64		7.50	ີ ພາ	
GENT	(DFC.) -29.2		-27.5	<u>.</u>	. .	•	å.	:		٠.	<u>.</u>	•		1	٠,	٠,	ے د	• •		•	, ,	٠,	7 11-	:	; 0		, H						m	m	Ñ		. 4	a .	<u>۔</u>	ت د ا	ز:	7•3	9• I	5.4	3.4	y•1,	5.2
W # 1	S S	EC. 5	0.18	81.8	82.7	E3.4	6.65	P 4 - 7	85.2	85.6	65.1	65.4		84.1	83.1	62.4	F4 - 1		20° C								6.79		0.10										85.2			85.6		•	٦.	•	•
	(066.)	, ,	~	27	27	27	ç ۲	2	-24.8	5	23	22	-	~	. 그	-20.1	5	(i)	<u>۔</u>	_	J	J)	2.CI-	Ω,	\$ (41	<u> </u>	╮.	-	- ·	1000	•	٦,	- ر	• •	-5.6	1.4-	G.	-7.B	٠.	•	•	•	•	1.7	•	2.4
AUM HUM	RESSUR	•	83.3		•	•			•	•	•	•	•	•	•	•	•	•	•	•	•	-	-	•	-	-	-		-				_				_		•		•	:	•	•			82.6
TANGE	(DEG		o ~	-27.6	_	-26.2	-25.9	-25.3	-24.8	-24.2	-23.9	-23.6	-23.3	-22.9	-22.2	-22.1	-22.f	-21.B	-21.7	-21.5	-20.9	-20.5	-2i.o	-19.5	-19.2	=	=		_	-	Ä,	٠,	· ·	* *			, ,	12.	=	,,,	6	6	65	ب		•	
47.5 ZMAXIMUM	S	ş,	n -		2	•	71	٠,	69.3		4	~	*	7.87	8	8	ູ	9	۵.	;	•	_	•	Ġ	ŝ	ċ	ċ		66.3	:	•		٠,		•	• .		ی	, _~	0		. ~	-,	9	- C		E7.1
HORD= 11AL	(DEG.)	•	125	• -	•	: :		•					•			en en		٠	9		41		3							_	-12.1	11.	<u>.</u>	•		•		•	•	e Suri	• \ \	•	•		٠.	•	
24-6 1	~ ~		•	•		•	• (•	• •	•	•	• (•			•	•	•	•	, ,		,	•	•		_							_==										٠.	a -			78.9
# CHORD=	(DFG.)	7	a ⊃ (יס כב		٠.	ب د	. ~	ιĊ	• •	• (2 0		7 -							. 7					_	_	ŭ	E 6 -	-8.6	J • 8-	7.1	-6.8	0.9-	-5.8	2.5	-5.5	٦. د.	2 u) ())	7.5-	7 - 1	6. 0	. ·	a (3.2
SAMPLE	NIMBER	-	2	m ·	o r u	n •	، ٥	~ 6	ro	• •	<u>:</u>	C	7 -	n 3	† 4 •	2 4	2 -	~ œ	2 0		21	100	2.7 F.C	76	2 5	2,4	27	4 <	62	, F	31	32	33	34	35	36	37	6. (c)	39	C 7	*	6.5	.	+ 1	40	4	4.4 4.8

TABLE D-23(Contd)

# CMCKD= 73.4 TANGENTIAL #MAXIMUM (DEG.) PRESSURE -1.4 83.9 -1.9 95.2	TANGEN (DEG (DEG	# # # # # # # # # # # # # # # # # # #	# M M M M M M M M M M M M M M M M M M M	·
	111	PRESSUA B	(DE5.) PRESSURE 5.3 R6.0 1.4 80.5	PRESSUPE (DES.) 75.4 2.3 72.4 1.0 65.6 1.4
				75.4 0.3 72.4 1.0 65.6 1.4
-1.9 95.2				72.4 1.0 69.6 1.4 67 6 1.0
				65.6
				1.9
				45.2 2.4
				5.5 4.47
4.4 81.4				71.3 3.1
				74.
				75.1 6.3
				91.1
				7.0
				85.3

CT 1

% MAXIMUM PRESSURE
CURYE CURYE
LABEL VALUE
2 0.930000E+02
3 0.860000E+02
4 0.790000E+02
5 0.720000E+02
6 0.850000E+02
7 0.580000E+02
6 0.510000E+02
MAXIMUM STATIC PRESSURE



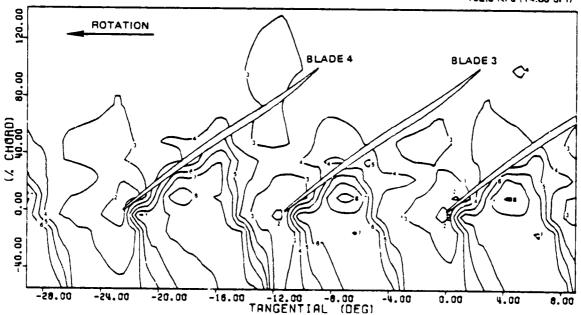


Figure D-14 Steady State Pressure Contours at Blade Tip; No Flutter, High Operating Line, 73 Percent Speed, 74.7 Percent Flow, Pressure Ratio 1.2687

TABLE D-24

STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS

73% SPEED

RECORD 104

Inlet Total Pressure = $86,280 \text{ N/m}^2 (1802 \text{ lbf/ft}^2)$

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
-55.4	0.953
-15.1	0.948
- 3.6	0.953
9.4	0.981
22.2	1.066
34.6	1.177
47.5	1.143
73.4	1.184
99.3	1.206
141.4	1.190

TABLE 0-25

																			े। Oi	₹!: F				. 1			: (1)	Ţ																		
	PAGE 1	22.2 \$HAX IMUM	PRESSURE	• •	76.7	•	83.1	86.2	9.69	45.7	•	•	94.0	76.37		81.3	•	87.9	91.1	94.1	4.96	97.1	42.4	i. 17	ر د د د د د	78.9	82.6			6.40	96.2	•	~	O (6.46	78.0	P1.5		8	-	M ·	•	1.76	r v		
		T CHORD=	W *			36.	37.	36	5.	34.	33.	32.	131.6	100-	-28-5	-27.4	-26.4	-25.4	-24.3	-23.3	-22.3	-21.2	-20.5	-19.2	1.81.	-17-1	1.91-	0.61-	1 1 4 C	0 - 1 - 1	-10.9	6.6-	-8-6	-7.E	2) P	1.7	-3.7	-7.6	-1.6	9 (n .	د• ۱	C•7	9*6	•	
	PSI	_ O ×	•,	93.6		÷	•	e7.9	41.3	95.3	97.3	9.88	\$ \$ \$ \$	4.44	73.3	80.3	85.2	6.88	92.3	95.8	9.96	26.7	-	•	0.70	.		n o	6,69	26.43	96.1	83.2	90.05	0-05	1.72	77.9	82.8	e7.3	~	63.9	6.26	- 1		70.50	7.7 B	83.0
	SSURES S = 15.40	T CHORD=)EG.)	0-134	-39.e	8	37	3	-35.7	1-34.7	-33.6	-32.6	3.75	29.5	-78.5	-27.4	-26.4	-25.4	-2403	-23.3	-22.3	-21.2	-201-2	-19.2	1.81-	-17-1	1.6.1	0.01-	0.41-	0-11-	-10.9	•	8 . 9	-7.e	2 C	F-4-	(1)	-2.6	-1.6	91	٥.	٠. د		9.0		• •
	KILDFASCALS =	-3.6 EMAXIMUM 1	PRES SURE	7. 67	۱	-	82.1	83.6	85.4	88.2		;	n a			82.0	83.0	84.3	86.4	8.68	15.4	0.53	66.5	71.5	15.6	79.5	92°1	97.	8 4	3 0	72.0	~	63.5	67.5	8 7 7		82.0	82.8	4	87.6	•	7.40	2.66	2.77	•	. E.
IABLE U-23	ULITE STEADY = 106.0	TANGENTIAL	(066.)	7	6	a)	-37.8	36	35	34	33	32	91.00	•	-28.5			-25.4	-24.3	-23.3	-22.3	-21.2	-20-5	-19.2	1.81-	•	v v	۲,	200	0 - 1 -	-10.9	0.9	8° 8'	e	2° 4° 4° 4° 4° 4° 4° 4° 4° 4° 4° 4° 4° 4°	-4-7	•	\sim	-1.6	9	•	٠. ۲	•			6.7
	104 WALL KULITE JRE SAMPLED =	-15.1 THAX IHUH	RES	4.74		_:	3		÷	-	83.4	٠.		67.0		~	\$.	•	91.1	•		*	₼.	• .	· .	ا ا	•	•	: -		•		~ ·	7.17	. ^	. •	_	•	88.2	\$ (٠. ١	7	٠,٠	٠	83.9
	RECORD 104 MAXIMUM PRESSURE	TANGENTIAL	DEG.	ے .	39.	38.	37.	36.	35.	34.	£4.	32.			2 8	27.	26.	250	24.	23.	25.	21.	٠ د د د	<u>.</u>	91,	17.			, ,	• •		•	စ. ၈ ၊	۴,	8 6 4	, 4		2.		•	•	•	•	•		6.1
	Ä	-55.4 \$HAX IHUH		2.79	63.9	74.7	83.0	65.6	86.2	65.9	83.9	79.4	13.5	, c4	63.0	73.2	84.5	87.1	87.6	87.2	84.9	75.7	72.9	67.0	63.9	0.99	80°0	7.00	80.1	· 40	83.8	78.0	71.4)•99 (4 7 Y	66.4	82.9	87.2	87.4	96.1	2.5		C*11	, , , , , , , , , , , , , , , , , , ,	7.07	
		# CHORD= TANGENTIAL	DEG	•	39	41 C.		36.	35.	C 1	-33.6	-35.6	-31.6	26.5	- 20.5	-2704	-26.4	-25.4	-24.3	-23.3	-55-3	-21.2	-2:.2	-19.2	1.8.1	-17.1	-16.1	0.01-	* F T 1		-10.9	Ţ	•	8°.'-	2 6	-4-7	-3.7	-2.6	-1.6	9 ·	٥.	 	6.2	9	2	6.1
2	132	SAMPLE NIMBER 1	•	- ~	4 W	1	ĸ	•	^	€0	Φ ;	2	11) J	7	5	16	17	18	10	0.2	21	22	23	52	\$2	56	7 .	5 6	, y	31	32	33	34	د د م	37	38	39	5 2	17	2 :	43	t 4 1			. 6

TABLE D-25(Contd)

PAGE 2	22.2 EMAXIMUM PRFSSURE P5.4 88.7 91.9
	H G
	# CHORD= UM TANGENTIAL # RE (DEG.) P 7.7 8.7
PSI	84.4 RESSUN 87.3 90.5
SSURES S = 15.40	T CHCRD= TANGENTIAL (DEG.) 7.7 8.7 9.8
Y STATE PRE KILOPASCAL	-3.6 RMAXIMUM PRESSURE 92.9 84.5 86.5
KULITE STEAD D * 106.0	T CHCRD= -3.6 TANGENTIAL TMAXIMUM (DEG.) PRESSURE 7.7 92.9 8.7 84.5 9.8 86.5
104 WALL	-15.1 #MAX1MUM PRESSURE 85.0 89.2 97.6
RECORD 104 WALL KULITE STEADY STATE PRESSURES NAXIMUM PRESSURE SAMPLED * 106.0 KILOPASCALS * 15.40	T CHCRD= -15.1 T CHCRD TANGENTIAL THANGENTIAL (DEG.) PRESSURE (DEG.) 7.7 85.0 T.7 89.2 8.7 9.8 97.6 9.8
I	M G B G G G G G G G G G G G G G G G G G
	15 TANGENTIAL 1 (BES.) P 7.7
	SAMPLE NUMBER 49 50 51

OF Louis Commy

		en e	
141.4 RRAXINUM PRESSURE 94.8 96.5 96.5 96.8 96.8	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	99999999999999999999999999999999999999	67.5 67.3 67.6 67.6 69.0 6.0 6.0 6.0
# CHORD= TANGENTIAL (DEG.) -41.9 -40.9 -50.9 -39.6 -39.6 -36.7 -36.7 -35.7 -34.7		11511111111111111111111111111111111111	30 m m m m m m m m m m m m m m m m m m m
99.3 PRESSURE 98.2 97.3 96.7 96.6 97.8 97.8	99999999999999999999999999999999999999	6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	999999999999999999999999999999999999999
# CHORD= TANCENTIAL [DEG.] -41.9 -40.9 -39.8 -37.8 -36.7 -35.7	1 1 1 2 2 2 3 3 3 3 4 4 4 5 5 5 6 6 6 6 6 7 5 1 1 1 1 1 2 2 2 2 3 3 3 4 4 4 5 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6	1.3.4.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	00 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0
. ₩	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	96 99 99 99 99 99 99 99 99 99 99 99 99 9	99999999999999999999999999999999999999
HT 6 6 6 8 6 7 7 7 7 8 8 8 7 7 7 7 9 9 9 9 7 7 7 7 7	13.5 13.5 13.5 13.5 13.5 13.5 13.5 13.5	111511111111111111111111111111111111111	62 m v m 4 n 4 3 4 n n n 4 4 4 4 4
47.5 PRESSURE 94.5 94.3 93.8 91.2 91.2 91.5			
m m m c c a p p v v v w	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		
34.6 MAXIMUM PRESSURE 92.7 91.5 96.2 96.2 96.2	, 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	よきいころですようらりこうてい	
4 0 0 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		- 454 45 45 45 45 45 45 45 45 45 45 45 45 	
n a	4 4 8 4 8 4 8 4 8 4 8 4 8 4 8 4 8 4 8 4	. 4 F B B B B B B B B B B B B B B B B B B	0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -

ORIGINAL TO SEE

TABLE D-25(Contd)

PAGE 4	141.4 THAXIMUM PRESSURE	3. C
	# CHORD= H TANGENTIAL 3 E (DEG.) F	- ac
PSI	99.3 EMAXIMUM PRESSURE 98.3	99.2
SSURES S = 15.40	# CHORD# 99.3 TANGENTIAL #MAXIMUM (DEG.) PRESSURE	- E-
r STATE PRE KILOPASCAL	73.4 EMAXIHUM PRESSURE 97.1	97.5
ULITE STEAD	CHORD= 73.4 I TANGENTIAL EMAXIMUM COEC.) PRESSURE 7.7 97.1	- 6.
104 WALL W Re Sampled	47.5 SMAXIMUM PRESSURE 88.7	92.7
RECORD 104 WALL KULITE STEADY STATE PRESSURES HAXIMUM PRESSURE SAMPLED = 106.0 KILOPASCALS = 15.40	TANGENIIAL SHAXIMUM TANGENTIAL (DEG.) PRESSURE (DEG.)	2 6
ī	34.6 TMAXIMUM PRESSURE 87.8	93.3
	T CHORD= 34.6 TANGENIIAL THAXIMUM (DEG.) PRESSURE 7.7 87.8	60
	SAMPLE NUMBER 49	

% MAXIMUM PRESSURE

CURVE CURVE
LRBEL VALUE
1 0.1000000E-03
2 0.800000E-02
3 0.800000E-02
4 0.700000E-02
5 0.720000E-02
6 0.6500000E-02
7 0.380000E-02
9 0.510000E-02
MAXIMUM STATIC PRESSURE
106.0 KPa (15.40 PSI)

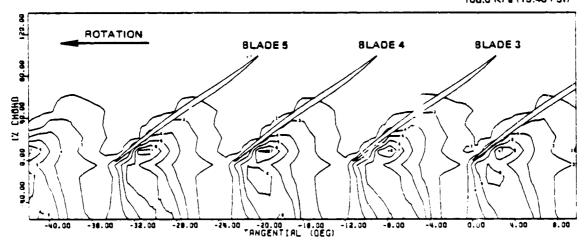


Figure D-15 Steady State Pressure Contours at B'ade Tip; In Flutter, High Operating Line, 73 Percent Speed, 60 Percent Flow, Pressure Ratio 1.3317

- Para Landity

TABLE D-26

STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS

75% SPEED

RECORD 181

Inlet Total Pressure = $79,480 \text{ N/m}^2 (1660 \text{ lbf/ft}^2)$

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
-55.4	0.909
-15.1	0.907
- 3.6	0.928
9.4	0.961
22.2	0.974
34.6	1.026
47.5	1.057
73.4	1.072
99.3	1.087
141.4	1.102

PAGE 1

																					(Oi	r	i.	ت	۔ ا			د رو د کم			À																	
22.2	BRESSIRE	.		•	• -	9	; ;	3,6	,	` .	٠,-					.0	8	6	•	•	Š	9.69	•	26.7	•	12.8		75.3	a• 6.) · (2)	7.63		74.1	5.03	0.8.	ತ	÷.	٠.	•	i a	3 ~	, =	: -		. J		~	
T CHURD=	1 1 A L	•		5.77-	4-17-	10:2-	0 6 7	-16-4	-17.9	-16.9		7.67	7.5.7	-14.8	-14.2	-12.9	-11.7	6.01-	2.6-	-8-6	-7.t	-7.3	-6.7	-6.2	-5-3	-5.1	-3.9	-3.2	-2.1	7.0-	e .	•	0 -	3.8	4.1	۲۰۶	2.4	20 v	0 f	- a	0 0		• •	3.2.6	12.0	14.5	14.P	
	ZMAXIMUM	700	6.16	95.3	7 · 86	5° 55	7.16	144	4 67			, c	4.00	72.5	8 6 6				96.1	68.3	51.9	٠.			17.0		94.6	89.4	93.B	٦.	41.1	•	** 7 G		61.2		•		2.06	•	0.00	75.0	•	2.4.5		•) }
€ CHOR	Z.	2	23	147	22	~ .	s (0.01	•		• •	107	0-011	7 7 7 1	D . C	12.00	-12.2	-	-10-1	-6-2	4 6	-7-2	-6.5	2.4-	8.4-	4	-3.1	-1.1	-C • 5	•		•	e c	4 4 8 4		6.3	7.4	8.2	٥. د.	0.11	0 - 1 - 0	17.3	•	٠) · ·		•
	THAN	PRESSUR	45.	96	100.	55.	-19	20 A	,		• .	٠.	٠.	•	٠.	61.5	• ~	٦.	•	•		7.04		•	, ,	. 0	7.65	N		84 °E	88.5	•	6	N C) en	14	C	_	9.09	Φ .	∞ 0.	ગ :	,		- r	† C	3 ° 0 7	•
₹ CHORD≈	TANGENT IAL	(DEG.)	-23.7	-23.1	-22.5	-21.2	-53.T	-26.3	C*61-	-18.9	7.81-	-17.6	6.91-	4.01-	-14:-	-15.4	1001	0.21-	-11-0	0.11	7.7	1.01-		7 • • • • • • • • • • • • • • • • • • •	7.7-		4 6	-5.2	-4-3	-3.7	-1.9	-0.5	-6.2	7.0	1.0		2.3	5.9	3.5	7.0	. S.	6.3	5°,	7 · 8 · 5	o	1 .	* * * * * * * * * * * * * * * * * * * *	C • 71
-	7.	2	ě			•	•	57.0	•	•	٠	٠	٠	٠	٠	•	٠	٠	٠	•	0 ° °	5 × 5	• • •	90.00	2	7 . 0	r 0	60.00	86.9	96.7	91.6	87.2	63.4	61.3	63.0	57.7	57.0	57.6	57.2	59.6	61.9	84.3	85.6	82°	∵ 66	88.2	91.1	1.05
Z CH080=	VI IV	10FG.1	2	-22.4	2.2	2	٠,		ď	0.91-	4	•	61	\sim	•		1 (Ġ,	۲. ۱	;	E		٠.	•		•	.	•	. 2	-	-				2.5 c.5	•						•	•	•	•	÷.	٠	:
	HAXI	ES	60					74.1		٠					:	C 1.	:	m	<u>.</u>			72.5	Λ	2	O			Λ.		`~		•	_	-	61.4		" —	·o	4.	~	~	Ð	•	Œ	0	9	_	æ
=00001	ENTIAL	COFG	7.6	, ,		, ,	21.	-20.1	6	-18•3	9.	7.	13	\sim	\sim	-12.2		-4	_	c.		€	_	-5.5	4 1	~	-3.	6.7-	- 2 - 1			. , ,		3-0	9.6	* •	n er		7.6	6.6	ċ	ċ	•		14.2	\$	16.7	a.
110000	NIMBER		-	• ^	.,	n 4	· •∩	• •0	7	60	œ	o1	11	12	13	1.	*1	16	17	13	19	5.7	21	22	23	54	52	26	7 6	n 6	۲, د	;	32	E)	34	35	30	. 0	י ס ה	6.4	41	42	43	77	4,5	94	4.7	4.8

	PSI	6
	SSURES = 14.83	# CHOKD= 9.4
Contd)	V STATE PRES	٠٩٠٤
TABLE D-27(Contd)	RECORD 181 WALL KUL <u>ite Steady</u> State pressures Maximum pressure sampled = 102.4 kilopascals = 14.83 psi	# CHORD= -3.6
•) 181 WALL M Sure Sampled	-15.1
	RECORE AXIMUM PRESS	1.4 % CHOKP = -15.1 % CHORD=
	Σ	4.0

22.2 SMAXIMUM													
T CHORD=	10k6.)	1001	15.0	7 7 7	2 4	7.0.7	7) · · ·	۲• <u>۲</u>	19.4	71.7	22.6	23.2
9-4 ZHAXIMUM	FRESSURE SS B	2 0	6,74	40.5	7 7 7	2 2	200	900		40.6	53.1	95.7	1.46
E CHORD= JANGENTIAL	1,000	2.7.1		σ.	0.0	2 0	3	2 4 5 6	0	0*17	22.2	22.9	23.2
-3 .K THAX JMU., 625 S110 G	5 B - 3	45.4	6.00	61.1	57.4		4.44	, , ,		60.0	6.46	ر. 96	72.3
# CHORD # TANGENTIAL	12.5	13.0	13.6	14.1	16.0	17.7		19.5			22.0	22.4	23.2
-15.1 ZMAXIMUH PRE SHRE	0440	61.7	62.6	58.7	55.9	57.0	63.9	83.2	9.4.4	• • • •	82.8	91.8	82.4
% CHORF= UM TANGENTIAL RE (DEG.)	12.8	12.9	13.4	14.7	16.5	18.5	14.3	5.0	2.03	•	D	22.5	23.2
-55.4 THAXIHIPRESSUI	56.4	56.7	59.8	63.5	4.69	76.0	P1.0	84.8	36.9		9 9 9 9	88.	84.7
R TANGENTIAL (DEG.)	19.7	20.1	23.6	5: • 9	21.0	21.2	21.4	21.4	21.6	7 10	7 7 7	0.27	23.2
SAMPLE	65												

RECORD 131 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 162.4 KILOPASCALS = 14.83 PSI

141.4 TMAXIMUM PRESSURE	95.2	41	6.53	Š	ď	Š	•	\$	•	5	4		\$	P5.8	Ġ	٥	ú	٠,	4)	86.1	Ω,	an u	Λ 4	4 6 6	ď	1 41	41	۵	J.	3	in .			, 4		-3	•	3.	35.58	;	66.5	•	9	~;	Š	•
₹ CHORD= TANGENTIAL (DEG.)	3.7	~	•	-		ç.	-18-3	7.	•	S	4	14	-i 5.4	\sim	~	B. 11-	ؿ	-9-3	•	o. (5. .	0 0 0 4 1 (7 ~ ~		, ,	-2.2		L.0-	•	1.0	ພ : (7.0		7.7			•	•		:	_;	12.7	C	- (
99 e3 ZMAXIMUM PRESSURE	85.3	5.	85.6	Š	5	4	m,	,	,	•	\$	4	5.	5.	Š	•	•	o	•	\$ (•	4 c		• •		0.4°	S	85.1	Š	S	٠. د	• •	• •		12°C	_:	•	2.	'n.	P4.5	•	٠,	85.7	~ 7		•
X CHUKU= TANGENTIAL (DEG.)	23.7	23	22	2	~	٠,	3	a:	-13.5	-16.1		2	-15.9	S	4	m	٠,	-11-1	٠	-5.2	x	7• R-		2.4	9	• •	•	•	•	•	•	•	•		4.1	•	5.2	•	•	•	8 • S	•	•	_;		4 1
7.5 c4 &MAXIMUM PRESSURE	95	5	85.6	\$	e.		å	٠.	å	÷		~	÷	~	·		•	•			•	•	•	84.5						•	-	_			82.1			_			84.5	٠	85.3	4.	3	,
* CHURUE TANGENTIAL (DEG.)	23.	23.	-23.2	22.	22.	2].	21.	-20.4	19.	8	~	-16.9	J	S	S	-14.3	ו ויי	\sim	_	្ន	• - c	γ α	•	- 6	, 4		-3.2	•	•	•	•	•	•		4		4.0		•	•	٠	6	10.4	ċ	11.3	
TMAXIMUM PRESSURE	89.7	6	84.6	. ,	•	6	•	÷	-	67.8	•	m	5	•	ď		٠,		•	• •	• •	1 1	• •		_	. m	u)	_	-	•		<u>.</u>	` .	7.77	78.5	e en		•	en en		•	•		•	76.9	•
TANGENTIAL (DEG.)	23.7	23.	•	5	÷ .	٠ ا	7	16,	3	Ä	٠,	Š	14.	7	ď,	2	2 :		٠. ا	•	•		• .	1.0	7		m	ď	•	•	•	•					•	1 • 3	¢.			2.	13.4	4.		١
ZMAXIMUM PRESSURE	89.4	~	6	m	α 1	_	~	S.	.+	n	~	~		œ.	· .	<u> </u>	٠.	~	Ĕ.		: .		:	0 0				:	:	٠.	٠.	• -	• -	٠.	•	•	•	•	•	•	•	•	•	٠		•
TANGENTTAL (DFG.)	23.7	22.	•	19.		7.	16.) ć.	5.	15.	14.	7	<u>.</u>				<u>.</u> 1	ات	•		: ,	ö		-5.2	7		,	m,	ċ	ζ,										6•3	•	•	7.7	·	11.2	•
SAMPLE NUMBER	-	2	m	7	ن م	•	7	o n	Φ	10		12	13	5 1	15	16	7 1	a :	61	را ر بر د	17	۶,	2,2	52	56	27	23	0 (٦) ا	31	נט ני ניו ני	ر د د د	3.5	36	37	39	39	04	41	75	63	74	45	46	17	

1. 2. las

TABLE 0-27(Contd)

T CHORD= 34.6 ANGENTIAL THAXIMUM (DEG.) PRESSURE 13.2 P1.5									
			47.5	CHORD=	73.4	CHORD=	66-66	CHURD=	141.4
PACS P1		ļ	EMAXIMUM	TANGENTIAL	ENAXIA	TANGENTIAL	ZMAXIMUM	TANGENTIAL	EHAXIMUM
P.1	SSURE		PRESSURE	(0£6.)	PRES SU	(050)	PRESSURE	(DEG.)	PRESSURE
(1.5		17.6		62.0	13.9	83.9	14.9	85.7
20	2.1		75.5		82.6	14.1	63.7	15.6	2.49
	7.5	17.6	73.9	15.2	83.3	15.1	83.5	16.1	34.6
	33 •		72.9		83.3	15.6	83.1	17.1	64.6
	5.7		75.4		83.5	16.1	82.8	18.2	84.3
	5-5		78.2		83.5	16.5	82.8	15.3	84.5
	1.5		B S		83.2	17.5	83.8	19.5	85.2
	6.0		8 * + 3		84.2	18.3	84.8	20.05	1.18
	2.2		P7.2		85.1	19.3	85.4	21.2	95.8
	••1		99.4		6545	21,3	0.03	21.7	56.4
•	7.1		87.8		83.9	27.4	86.5	72.4	66,7
	9.0		86.1		82.7	23.2	86.5	23.2	86.4

OF FOUR

% MAXIMUM PRESSURE

CURVE CURVE
LRBEL VALUE
2 0.990000E+02
3 0.880000E+02
4 0.790000E+02
5 0.720000E+02
6 0.850000E+02
7 0.580000E+02
9 0.510000E+02
MAXIMUM STATIC PRESSURE
102.4 KPs (14.83 PSI)

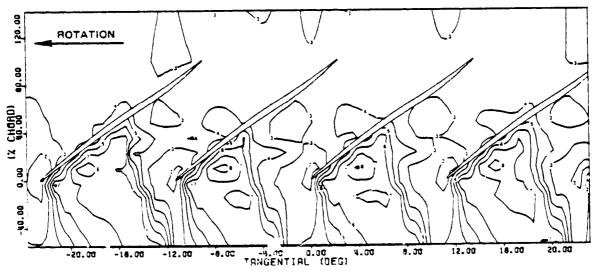


Figure D-16 Steady State Pressure Contours at Blade Tip; Out of Flutter, Low Operating Line, 75 Percent Speed, 75.3 Percent Flow, Pressure Ratio 1.284

OF FLUX COMMY

TABLE D-28

STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS

75% SPEED

RECORD 199

Inlet Total Pressure = $85,610 \text{ N/m}^2 (1788 \text{ lbf/ft}^2)$

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
-55.4	0.981
-15.1	0.948
- 3.6	0.951
9.4	0.981
22.2	1.065
34.6	1.117
47.5	1.145
73.4	1.185
99.3	1.207
141.4	1.190

RECURN 199 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 112.2 KILOPASCALS = 16.30 PS

PAGE

POOR/QUALITY 22.5 #MAXIMUM PRESSURE 88.4 53.1 59.2 66.1 7:7 77.7 85.3 94.4 43.3 98.2 100.0 96.6 75.1 58.3 9.58 75.1 81.2 81.8 87.8 93.0 93.8 93.8 84.5 49.1 56.3 86.8 13.0 61.9 84.7 01.1 64.3 90.3 90.3 55.4 54.1 CHORD= TANGENTIAL (DEG.) 142.1 141.0 146.0 138.0 138.0 138.0 138.0 138.0 138.0 138.0 138.0 138.0 138.0 138.0 138.0 -25.6 -22.6 -21.5 -21.5 -19.5 -26.7 -23.6 -17.4 -18.4 -1 b . 4 ##AXIMUM 63.3 63.3 71.8 71.8 71.9 71.9 63.6 63.6 72.7 73.7 73.7 80.8 80.8 80.8 83.4 69.2 59.2 59.3 69.3 77.3 77.3 77.4 77.4 77.4 77.4 77.4 59.3 6.99 61.0 65.1 68.9 73.3 76.1 77.5 78.7 60.3 60.3 65.7 69.3 76.1 CHORD= TANGENTIAL (DEG.) -42.1 -41.0 -39.0 -36.9 -35.9 -31.8 -31.8 -28.7 -27.7 -26.7 -25.6 -24.6 -23.6 -7.2 -6.1 -----14446 -5.1 600.5 44.2 44.2 600.5 60 P4.5 61.3 53.2 61.3 67.5 73.5 # CHOKD= TANGENTIAL 9 (DEG.) -42.1 -42.1 -42.1 -42.1 -38.0 -38.0 -35.4 -35.4 -35.4 -31.8 -31.8 -25.06 -27.66 -21.5 -20.5 -11.3 -11.2 -9.2 --, -7 -26.7 -27.7 -25.0 -15.4 -14.3 -13.3 -18.4 -17.4 -8-2 -7-2 -6-1 -5-1 -3-1 -2-0 -1-0 -26.7 -16.4 2.1 2.1 4.1 5.2 6.2 HAKXIA HAKXIA PRESSIRE 69.6 64.2 76.2 76.2 83.3 83.3 60.1 64.1 64.1 61.3 63.7 24.1 84.7 84.8 63.5 79.8 13.9 63.2 61.9 70.6 81.3 83.3 53.7 80.6 75.4 69.3 64.4 # CHORD= TANGENTIAL 1 1DEG.) 1 -42.1 -41.0 -4.0 -25.0 -35.9 -35.9 -35.9 -35.9 -36.9 -37.7 -27.7 -25.6 -24.6 -23.6 127.cc 127.cc 127.cc 127.cc 127.cc 126.cc 114.33 1.11.33 64444 -2.ti -15.4 -4.1 SAMPLE NUMB! R ~ U m 4 5 0 1 0 5

ORIGINAL/PAGE IS

TABLE 0-29(Contd)

	PSI
~	= 16.30
JRE	u
PRESSL	SCALS
STATE	KILOPA
RECORD 199 WALL KULITE STEADY STATE PRESSURES	112.2 KILOPASCAL
11	
짚	•
WALL	SAMPLE
199	u.
ECORD	MAXIMUM PRESSURF SAMPLED
Œ	E

PAGE ?

	_	MAXIMUM PRESSU	JRF SAMPLED	112.2	KILUPASCALS	PRESSURF SAMPLED # 112.2 KILUPASCALS = 16.50 PSI	7		
©HO ₽	₹ CHGRD= -55.4 % CHORD		-15.2	CHORD =	-3.9	CHORD=	9.3	CHORDE	22.5
MGENTI	AL THAXIMUM		THAXIMIN THE	ANSENTIAL	MAXIMUN	ANGE NT I AL	THAX I HUM	TANGENITAL	TOTI XYN2
(066.)	P RE S SUR E		PRESSURE	(016.)	RES SURE	(DEC.)	PRESSURE	(010.)	PKL SSUKE
7.2	30.A		80.4	7.2	76.8	7.2	80.5	7.2	74.8
3.	83.1		P 2 . 9	P. 2	78.4	P.2	R3.8	8.2	0,2
6.6 9.8	83.7		35.4	9.3	80.3	9.3	E7.3	5• ۲	65.2

																			,			٠.	٦.	-		t	i																		
PAGE 3	14 HAA PRI	42.1	91.3	۳. ه د د د	2 4	0 3		6.59	5.68	87.6	6.75	41.6	41.2	1 · C ·	0 C	2.60	5° (6	47.16	51.5	47.4	45.4	43.4	42.7	91.1	ئ ئەر		y 6	2006	E 3.7	9.1.1	7. 16	T	3-15	・・ン	64.7	۰ ۲. ۵	-		.	- 0					
	TANGENTIAL (UEG.)		~			ο.	3 6	٠.	. പ	5.45-	~	٠.	Jr.	.	• •	J	٠,٠	٠,٠	-22.6	-21.5	-26.5	-19.5	-16.4	-i 7.4	-16.4	# 0 4 1 1		1	-11.3	-12	-5-5	/* a-	177	-5-1	•	-3.1	\sim	3) • ; (7	7 - 7		6.3	
PSI	99.2 #MAX IMUM PRESSURE	92	Ġ	6 0 0 0		. د	•	• _ '	: -	· -:		•	•		•		~ ~		. ~		. •	•	~	•	_		- 4	~			94.6	~ ^			- 17	_	_	~	÷.	m -		• -	• 3	96.1	
ES SUR ES LS = 16.30	TANGENTIAL (DEG.)	_	-41.0	3.77	- A - C	2 0 P	25.0	75.6		10 10 10 10 10 10 10 10 10 10 10 10 10 1	-31.6	-3v.e	-29.7	-28.7	1-17-	7.97-	9.77	7 2 4 6 5 1	-22.6	-21.5	2.25-	-19.5	-16.4	-17.4	-16.4	٠,		1000 1000 1000	, ~		2.5-	יוסס	7.1		-4.1	-2-1				·		7. ~		6.2	
/ STATE PRES KILOPASCALS	73.4 THAX IMUH PRESSIBE	84.7	•	6 6 6 8	~ ,			- 0			\sim	$\overline{}$	•	œ.	ъ.			-		۰.	-		4.116	0	~	91.5	-	_ :	9	ن	C* 15	9.06) F () G		•		•		-		9.06	•	5°06	
KULITE STEADY D = 112.2 1	₩ ७ €	; –;	-41.7	4	,	-38-0	Y-05-	9.05.	۰.۲۰۱ ۹	-32.8	-31.3	-30.9	-29.T	-26.7	-27.7	-26.1	9-52-	0	-22.4	-21.5	-20.5	-14.5	-16.4	-17.4	-16.4	-15.4	-14.3	-13.3	-1153	-16.2	-9.2	-e •2	7.1-		-4-1	-3.1	-2.0	-1.0	e•==	1.1	2.1	 	- C	6.2	
199 WALL M URE SAMPLED	47.6 #MAXIMUM		88.6	83.6	8 ° 8	- C = C = C	83.0	0 ° C	7 ° ° °	2.08	- C - C - C - C - C - C - C - C - C - C	9.8.6	FR.4	83.6	85.5	83°0	6.73	- C	ر د . م	7	4 W)	4.0.2	1.64	9.6	87.0	84.4	9.49	85.3	0.10	4.69	6.00	64.5 6.0		13° 13	82.3	6 - 3	93.1	84.9	64.3	87.7	88.5	E3.7	•	67.1	
RECORN MAXIMUM PRESSI	- ロマ:	42.1	-	* U *	35.	بر ا	36.	35.		9.7K-	31.	-	25.	٠ در	27.	26.	25.		,,,		-	, ,	* * * * * * * * * * * * * * * * * * *	7	•	5.	٠,	٠,	ا ،	• •	حل .	•	٠.		• 4		2	_	() ()	•			•	2.0	•
Ž	34.4 EMAXIMUM	, C	: .•	76.5	_:	•	:		•	• •	•		_	-	$\overline{}$	~	•		_		` ^			f1 >		•	٠.	~		•	88.1	~	?	∙ .	0 0	• •	S	٠.	0	•	\sim		٠.	3 ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °	•
	H (5 (111=6.1	· 4	٠,	(-)	С.	9	5.		ם פנייון פרייון	: =	: 5	. (1)	٠. م	27	26	4	7	[] ("	→ C			17.	16.	15	. 4.		?:	-10.2		-B.2	-7.2	-6-1	7	•	, ,	_			•	•	٠	5.2	•
246	SAMPLE	-	. ~	ĸ	1	s	٥	٠ -	مي (• •	2 =	12	13	14	15	16	17	æ, ;	61	7 .	12	7 6	2.4	25	26	27	28	62	30	1 C E	3 E	34	35	36	- o	n o	, c	71		43				L 5 7	

TABLE D-29(Contd)

4	-				
PAGE 4	: 141.3 EKAXIMUM	PRESSURE	34.5	9.7.6	ۍ• ر≱ ا
	CHORDS	(1)(6.)	7.2	E.2	4.5
PSI	59.2 CHAXIM	RESSU	4.04	91.5	42.7
ECORD 199 WALL KULITE STEADY STATE PRESSURES PRESSURE SAMPLED = 112.2 KILOPASCALS = 16.30 PSI	TANGENTIAL	(DEG.)	7.2	8.2	6.5
r STATE PRI KILOPASCAI	73.4 THAX INUM	PRES SURE	91.0	7.16	41.7
KULITE STEAD' D = 112.2	TANGENTIAL THAXINUM	(066.)	7.2	9.2	9.3
199 WALL	47.6	PRFSSURE	P.3. P	85.7	85.4
RECORD MAXIMUM PRESSI	TANGENTIAL CHAXIMUM	(DEG.)	7.2	٥.	5.2
1,	34.4 MAXINUM	R-SSURE	61	85.7	87.3
	E TANCENTIAL 3	(neg)	7.2	8.2	6°.9
	SAMPLE		64		51

CHARGOR CORLINY

% MAXIMUM PRESSURE

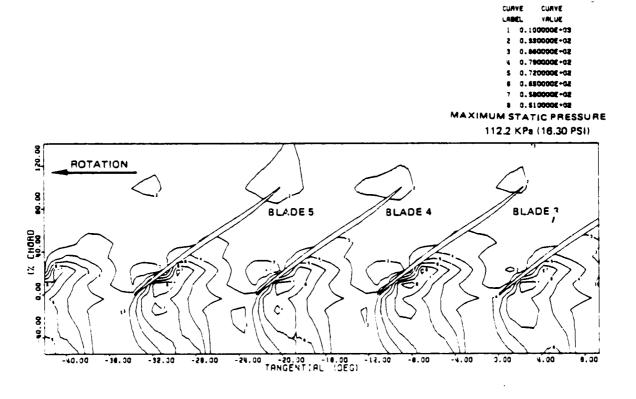


Figure D-17 Steady State Pressure Contours at Blade Tip; In Flutter, High Operating Line, 75 Percent Speed, 60.3 Percent Flow, Pressure Ratio 1.3369

PAGE 1	RD= 22. AL TMAXI PRESS	ء د	4		•	4 M	m	95.5	B. € 3	•	6.17	55.		•	ė	67	₽ (.	· · ·	475	25	76	a i	9,	3 4	7.7	7.	34		, <u>-</u>	2	78.	P6.	හ :	• • •	4	67	49	46	4	24	7
	TANGENTIAL (DEG.)	-25.4		6.55-	-22	-22-6	-21.6	-25.6	-2n - 1	3	7.51-	, 60		ာ	-17.2	Ç	٠١٠	4,	2.6.[-	-	•	Э-	۵.		7.8-	0 - L	-6.7	-t.2	7.61	0 5	-2-9	-1.6	٠, ١-			1.7	, m	3.7	4.1	4.7	 	,
FSI	9 X X X X S S S S S S S S S S S S S S S	. .	0 -	93.4	•	6.79		8	29.3		37.1				73.9			4. 7.	2.08	1	•	•	29.7	5	ພ ລ.	0 6	56.0	5	72.9	20 (4000	82.2		~	32.6				4		-	
PRESSURES ISCALS = 15.16	T C C T ANGEN	-25	. 4 × c	25	• . c	-24.3 -20.B	2 0	20	S.	8	-18.2	- <	ວ ແ	-15.4	•	6	•	_	پ د	9.01	• •	S & & -	-6.4	7.7-	-7.2	7.4	, 4	-4.5	-3.5	Ν,	1.0			1.2	2.9	.	P 4	. 4		7.1	G.8	
STATE	-3.6 THAXIMUM PRESSURE	81.0	S	on .	•	0.101	48.2	44.1	_	C:	52.2	ე ა	5.07	53.7	63.1	71.3	86.98	P7.8	1.96	52.7	46.3	52.2	46.1	57.3	49.5	•	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		•	76.7	84.8	۱ –	52.5			.	5.7			3	63.5	
KULITE STEADY D = 104.6 P	TANGEN TANGEN	-25.	•	C) (ή,	-22.8	v -	: :	•	ن	-19.5	10		• •	-15.3	-14.3	-13.1	5	.	\$*:JI-	ے ز	6	-6.9	-8-2	7.7-	9	V-C-	•	-3.7	-2.1	Z-1-	7 7			1.6		•			6.3	•	١
IRD 297 WALL KULIT	-15.1 EMAXIMUM PRESSURE	82.9	7	•	٦.;	C. 86	40.4 4.5.4	J 37	56.2	-	-11	٠,	٠,	47.0			3	7.	œ,	2.68	0 - 10			53.0	8	7 0 P	47.8 46.6	9	7		60.3		ນ • 6 ຍ	-3	68.7	71.2	4.00	67.6	•	47.5)
RECORD MAXIMUM PRESSU	\$ CHORD= TANGENTIAL (DEG.)	25.4	24.	24.		•	. , ,	, ,	7.		٠	•	• •			-3	٠,	J	.	٠.	• -	•		•	Ġ.	دن	6.7-		•	•	ė,	•		٠.	r1 (3	•	•	•	•	, ,		
Ì	-55.4 THAXIMUM PRESSURE	51.6	٠	•		7.5	: -	•	• . •		•	•	•	•	• !	•	_:	•	7	:		•		•	•		52. 5.0.3	• :		•	÷.	٠,				÷	72.9	: -	•	٠,		•
	17 13 6	5.4	7	7	7	6	יט נ	<i>></i>		. 6	3 [_	9 ;	7 .	 	7	_	=	_	= ;	 	⊣ 1	0.6-	∞ ∞	5.9-	-6.1	4.0	6 · 7 -	-1:1	ات • ھ	9-0-	9 6	(• () ·		6.0	1.5	6 (7.7	6.7	7 5	6.7	
	SAMPLE NUMBER		7	9	1	2	• 1	~ ₀	n Or	1)	11	12	13	7 7	- - -		· a -	18	۲)	5;	22	25	1 U	5 c	27	2.9	C1 C		32	33	36	35	o r	er Or	, 6 .	67	7	77	4.			

250		I	RECORD 287 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 104.6 KILOPASCALS = 15.16	287 WALL URE SAMPLE	KULITE STEAD D = 104.6	r STATE PR KILOPASCA	ESSURES LS = 15.16	. PS1		PAGE 2
SAMPLE		-55.4	₹ CHORD=	-15.1	CHORD=	-3.6	CHORD=	4.6	# CHORD=	22.2
NUMBER	یـ	THAXIMUM	TANGENTIAL	EMAXIMUM	TANGENTIAL	ZMAX IMUM	JM TANGENTIAL	EMAXIMUM	TANGENTIAL	EMAXIMUM
		PRESSURE	(DTC)	PRESSURE	(DEG.)	PRESSURE	(DEG.)		(DEG.)	PRESSURE
67		57.5	7.3	52.0	9.8	84.6	11.4		ئ. ھ	69.4
63		65.3	و د م	64.3	11.9	96.2	12.3		9.1	7.97
51		12.9	5-5	P.7.	11.6	71.4	12.9		10.7	38.5
52		ည • • •	10.2	87.5	11.9	55.0	13.3		11.7	9).(6
رب (د)		E.B.4	11	6.56	12.3	4.1.4	13.7		12.8	91.2
54		94.3	3. T	83.3	12.9	53.1	14.2		13.6	88.6
52		85.6	11.9	73.8	13.5	50.6	14.8		14.2	0.77
99		15.7	12.7	53.2	14.2	52.4	15.3		14.5	63.7
57	14.0	67.3	13.2	55.1	14.9	27	15.8		15.4	46.9
۳, 80		62.C	14.1	1.364	15.6	50.7	16.1		15.9	48.2
59		56.9	14.8	44.5	16.3	49.5	16.4		16.7	46.1
60		54.3	16.9	47.6	17.9	49.5	8.91		17.1	8-97

Cr. FOOR Q. Can

250

TABLE D-30(Contd)

_																		Č.	i f Vo			بار ان	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	¢	∆	V	()	A A																	
PAGE 3	141.4 \$MAXIMUM	PRESSURE Rise		•	R2 • 3	82.4	63.1	87.6	: ځ	.	• •	ה הי הי הי	, ,	· **	P2.5	£ 7 • 5	82.5	82.5	62.3	82.1	62.2	619	62.5	63.1 63.1	V	n e	82.6	82.4	82.7	82.3	6.19	31.9	82.5	82.6	92.9	P3.2	83.6	e3 . 7	m) n n) n n) n	יי ה מיי	0.77	27.7	, –	•	-
	TANGENTIAL	۰ رو ک	-24.3	113	-72.5	-71.9	-21.3	-21.0	·	\$ • · · ·	* c	2 AT	-17.6	-17.1	-16.3	-15.5	4.4.	-13.9	-13.3	-12.7	-12.2	-11•3	-11 -	7°.17-	7.61	-7.3	16.2	\$ \$ \$ - \$ \$ - \$ \$ -		-3.7	-2.e	-2.1) 	ر د	3.0	1.4	2°0	2.5	2°5	7 7	P <u>-</u>	, C. 3	7	1-2	9.6
PSI	99.3 THAXIHUN	3 .7	86.1	•	91.c		•	6.58	•	7.10			79.2	_	•	8°08		81.5	•	62.3	82.8	8.28	7.78	•	7.70					78.7	79.0	19.2	٠,	19.9	•	= 0	ور د د	7.10	6 1 6 F	٠	, ,	٠.	٠.	2.11	~
SSURES S = 15.16	CHORD= TANGENTIAL	, ~	-24.6	•		6.22	7.77-	5° 1'-	. /	7 31-	4.81-	-17.4	~	•	-15.5	•	-14.0	-13.5	-12.7	-12.4	-12.0	** 1 1-	٥ و د د د د د د د د د د د د د د د د د د د	r 0 1		- t.5	-e •0	4.1-	17.6	4.9-	-5.6	7.6-	7-2-	-3.0	-2.2	4.1-		•	1.2	•	2.8	•	•		1.5
VY STATE PRESSURES KILOPASCALS =	T3.4 ZMAXIMUM PRESSIBE	8	-	٠.		74.2	0 6	2007	9.00	78.7	. 60	79.5	79.5	78.8	79.3	8 Je 1		•	83.3	9.14	٠: ا د : ا	1001	9.50	76.9	77.	77.1	76.9	17.71	78.1	74.3	79.5	61.0	81.3	7.	C	73.6	1.51) (9	7	۰۰	•	8	•
WALL KULITE STEADY Ampled = 104.6	CHORD= TANGENTIAL (DEG.)	-25.	6.42-	24.	23.	, ,	,,,	, ,		•		-10.6	Œ	-16.1	9.3!-	Λ,	n,	T (-12.9	-17.3	90 71	0.01	8.6-			1.1-	-7.2	-6.2	-5.1	0.1	7.6	-2.1	-1.5	9•n-	۳. ت	n •	7-7		3.6	•	•	5.7	•	7.2	
287 JRF S	47.5 *MAXIMUM PRESSURE	73	∙ ∙		٠.	. ~	•	• •	•	•	٠	•		٠.		٠.	٠.	•	•	•	•	•	• •			74.1	74.3	12.2	65.0	•	•	9,99			٠	•	• •				_		73.0		:
RECORD MAXIMUM PRESSU	TANGENTIAL (DEG.)	4 • 1	24.0	·, r	٠,	,	• .				-	ŝ	-i 6.4	٠.	Λ i	- u	7 P 7 T	. :	^ ~	5 0	· .		. 0	22	c i	~	٥		٠.		•	-2-1		•.	•	•	• • • • •	2.6	3.2	۲.,	4.5	•	9• 4		
ì	34.6 ZMLXIMUM PRESSURE	စာ	ο,	* *					•	•	_	•	-		Ξ.	-			•	•	•	•	•	•	•	•	•	•	٠	•	• •	9.08	•										_		
	O Z G	~	4.4.6	, ,	, ,	-21.1	2.	19.	18.		17.		ì,		1.45			-	-11-3			-8-6	4-1-	-6.5	0.9-	9.6	2-5-	1.4.	· · ·	4.7	2 6		3.0	٠	•	4.4	5.2	6.1	7	7.7	8.5	6	10-01	.	· .
	SAMPLE NIMBER		~ ←	^ 4	r vr	۰.۵	_	•	σ	10	. 4	12	£ .	* u	36		· 6:	2 -	2.5	27	22	23	54	52	25	72	27	\$ \frac{1}{2}	3.5	٠ د د	33	3.4	S	30 7.5	- a	0 00	40	41	24	4 3	77	45	91	15	d n)

TABLE D-30(Contd)

# CHORD=	3.4.5	T CHORD=	47.5	T CHORD=	73.4	CHORD=	99.3	₹ CHORD=	141.4
TANGENT JAL	HOWIX WHE	HUM TANGENTIAL	EMAXIMU	TANGENTIAL	THAX IMUM	TANGENTIAL	ZMAX IMUM	TANGENTIAL	XMAX IMUM
	PRESSURE	(086.)	PRESSUR	(0.66.)	PRESSURE	(066.)	PRESSURE	(DEG.)	PRE S SURE
	82.3	7.1	64.5	8.9	81.0	4.9	78.3	a•5	81.5
	61.8	7.8	69.5	4.7	92.2	7.1	78.9	16.5	81.9
	80.3	3°¢			78.)	7.9	79.3	11.5	91.6
	76.3	7.6			73.1	9.1	10.4	12.3	82.5
	69.69	10.4			75.6	6.6	60.2	15.1	P3.3
	6.39	11.			77.5	11.2	e1.1	13.7	£2.9
	62.5	12.			77.8	12.3	82.2	14.4	82.4
16.5	59.3	13.6			17.8	E - E -	81.1	14.5	82.3
	54.5	4.4			17.2	14.0	80.2	15.7	82.3
	51.3	15.8	15.3	16.2	77.5	15.7	6.11	16.3	82.1
	45.7	16.5			11.1	16.3	78.1	16.6	82.0
	47.4	16.9			77.9	16.9	78.6	17.1	82.1

CA POOR QUALITY

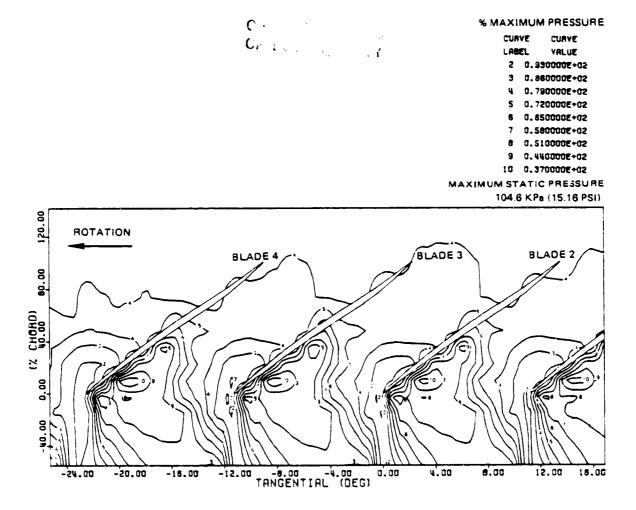


Figure D-18 Steady State Pressure Contours at Blade Tip; Out of Flutter, Transient to Surge, 85 Percent Speed, 77.5 Percent Flow, Pressure Ratio 1.4380

OF POOR QUALITY

TABLE D-31

STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS

85% SPEED

RECORD 283

Inlet Total Pressure = 76,130 N/m^2 (1590 lbf/ft^2)

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
-55.4	0,870
-15.1	0.851
- 3.6	0.867
9.4	0.892
22.2	0.978
34.6	0.999
47.5	1.002
73.4	1.081
99.3	1.101
141.4	1.137

TABLE 0-32

		Ĩ	RECORD 28 MAXIMUM PRESSURE	283 WALL KULI URE SAMPLED =	KULITE STEADY	TSTATE PRESSENT KILOPASCALS	ESSURES LS = 16.88	PSI		PAGE
SAMPLE	# CHORD=	-55.4 MAXIMI	CH	-15.1	₹ CHORD=	-3.6 MAXIMU	% CHURD= TANGENTIAL	9-4 \$HAXIMUM	6 E	22.2 HAXIM
	(DEC.)	ESSU	(DEC.)	PRESSURE	(DEG.)	SS	ڻ ن	RESS	(DFG.)	ω .5
•	-14.7		4	กับ เกิด		. a	. "	o ~	-13.6	51.3
~ 1	<u>.</u>	•	i e	• 0		ه ت ت	17	-	-13.3	S
F) ~	· :	•			۸ ر	52.9	-12.4	3	-13.6	9
p v	•	•	2		~	7.	-12.1	•	-12.4	• (•
· 40		•	2	56.1	:	\$	_	\$.	۲۰11- د د د د د د د د د د د د د د د د د د د	3 1
) r		•	=	85.6	~	9	-	ᅼ.	-11.2	- 4
ø			Ξ.	90.1	-	٠	• 	•		2
0			:	85.3	•	•	٠ د.	20.	٠,٠	7 22
1.0		•	្នំ	6.7.3	3	•	•	- 0	, ,	٠.
11		•	· (2)	54.6	-10.5	•	•	• •	ה ה ה	, ,
12	٠,	•	_ (52.5	<u>ت</u> د	0 1 S	n :		6.6-	
13		-	•	51.5		7 6 6	0.21	•	- 2.5	6
7		. : .	9.5-	9. E. C.			0 0	4 4	, , q-	
15		٠.	•	44.0	0 0	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	-643	, 9	1.0-	•
16		•	•	n = 0		50.00	-5.2	9	6-5-	•
17		٠,	٠,	1 0 d	٠ ‹	9	-4.2		-5-2	47.6
T) (• .	• 2	7.57	, c	٠,	-3.4		-4.3	•
		• -	٠.0	49.2	5-4-	- 60	6.5-	57.0	-4.4	46.6
, <u>, ,</u>		• .'		7.67	S.	B	i	•	9-2-	46.5
י ר.				6.64	-2.7	3	-1.5	89.8	-5.2	52.1
1 6		_:	e)	54.2	-2.3	3	-1.5	~	-2.6	58.1
2.5		_		58	-1.9	8	-1.1	~ ∙	7.1-	•
50		.:		65.23	J. 1	∾ .	7.6-	ν,	0 r	
25		_		65.6	L. ()—	8	ر رو ا		~ • •	
27		_:	:	9.69	4.0-	٠١ (m (0 (٠ ن ا	7 10
a ~		~:	- 3	2.09	٥٠٠	2	0.7	6.24) -	•
62			٠,	96.3	7.	r,	* * C	• -	4 .	0.0
3.0			•	**************************************	1.7		C 7 4	4 1	, ''. • ''.	
31			•	0.00	• •	,,	7.6	• • •	3.7	4.9.1
N 6		• •	° -	56.1	2.2	51.0		45.0	6.7	46.4
'. 7 '. F				54.6	2.8	~	5.0	•	4-2	3.00
, r		_		51.3	3.5	_	5. B.	-	4.6	51.6
36			, • .	51.1	403		4.0	47.2		4,00
37		~:	3.2	5.1.4	4.8	Ġ	7.6	-	5.7	50.61
36	ä	~	3.8	49.7	5.6	Ġ.	4.8	51.9	2.9	200
39	, ;	٠,٠	4.5	6.84	J.C	Ġ.	ထ _္ (٠.	9.0	:
C 7	_:	~	٥	44.5	9.1	င်	ه پ	-• 1	3 (٠.
17	_		5.6	46.3	9.3	54.4		۸,	x	
7.5	_	•	4.1	48.5	÷.	ġ,	: ت	•	•	٠.
43		٠,	6.8	40.2	16.4	m m	30. 0. 1.	;		
7.7	~	~	F•0	40.6		6	11.3		•	ю,
45	r.	j	C1 .	51.2	· · · · · · · · · · · · · · · · · ·		7.71	7.17	o • · · ·	200
46	Ç,	•	6.1	m i	: .			n :	5 · 2 · 5	-
17	c i		6.5	s.			- · · · ·	C - 36		, r
6.4 - 7.4	ď	,	 	Ş. [9	17.0		i en		5.7	

PAGE 2	A MANA MANA MANA MANA MANA MANA MANA MA	
	T CHORDE 10M TANGENTIAL 18E (DEG.) 15.0 15.0 15.4 15.4 16.7 16.7 16.7 17.8 17.8 18.8 19.6	
PSI	RENSIL RENSIL	
ESSURES LS = 16.88	CHORD= AUM TANGENTIAL JUNE (DEG.) 13.7 13.7 14.2 14.2 14.2 14.2 14.2 14.2 14.2 14.2 14.3 16.8 16.8 17.8 18.8	
, STATE PRI KILOPASCAI	-3.6 PREASIMUM PRESSURE 54.0 51.5 51.6 49.0 47.8 49.1 49.1	
RFCORD 233 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 116.5 KILOPASCALS = 16.88	T CHORD= (UN TANGENTIAL 12.6 12.6 13.4 13.4 14.0 14.8 15.6 16.3 17.4 18.0 18.0 18.0 19.5	
233 WALL JRE SAMPLE	-15-1 PREAXIMUM PREAXIMUM 91-1 95-7 61-5 57-6 57-6 55-5 57-6 55-5 56-6	
RFCORD AXIMUM PRESSO	x CHORD= TANGENTIAL 16.7 16.7 11.9 11.9 12.4 12.7 11.9 12.7 11.9 12.4 12.7 13.3	
Î	-55.4 PR:SSURE 65.0 63.7 67.7 67.7 57.4 55.7 55.7 55.7 55.7 52.9	
	TANCENTIAL (OEG.) 13.5 13.5 13.5 15.2 15.2 16.1 16.7 17.1 17.1 17.6	

SAMPLE NUMBER RFCORD 283 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 116.5 KILOPASCALS = 16.88 PSI

														С.		-		k.	**																										
7.	ZHAXIMUM Dof Color	9.	a)	S	ن	76.2 2, 1	o c	٠.	1 4	. ^	Ċ	`	•	(T)	۴. ۱	4	7	•	S	6)	٦,	•	J	7	_	76.9	J	٦,	1 4	4	4	;	\$	(4.2) (4.5)	; ,		۶.	'n	75.9	76.1	76.1	3.	;	74.0	•
CHORD	TANGENTIAL	• -)			_	1 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	•				-6.5			•		به بر ا ا				a	(4)	•	-2.3	-1.9	-1.5	35 A	٠ ٢	y 4		1.9	2.3	2.5	. ن ۱۳۰۰	\$. N	r es		6.5	7.6	6.5	9 * 3	5.2	16.5	12.6	12.9	13.3
	SHAXIMUM BOLCCIIDE	76.0	76.9			76.6	•		. ~		2.	_:	3	_:		•	• •	9	-	φ) (C)	6	11.17	5	ري.	•	74.6	;	د د		7	2.	•	• r= (5.50	•		3	2	•	Š	\$	•	4.6.4		6.5.5
€ CHO	TANGENTIAL	7.5	m	-12.9	7	7.1.	• = J		- 9 - 1	e o	en en	-8 -8	ه.	œ:	اند	9.7-	• ~	-7.2	-6.9	-6.7	4-4-	-6.2	1-5-1	-5.1	7.4.6	ا ان را م	יי ייי יייי	1.7-	200	1.1	1.6	5 ° C	2.1	7.5	7 4	7.2	C.	3.2	3.3	4.5	3.6	4.1	7-7	۲۰۰	4.0
3	ZMAXIMUM Dong Colon	ט ער י	•	76.7	•	1.61	•		76.64		•	68.2	•	٠	•	59.6				67.8		÷	÷	•	2	•		•	. ~	٠	ٺ	9.	•		• •	75.3	•	δ,	_	•		-	69.1	7: •6	· · 12
# CHOR	2 C		4	(٦	÷	-12.7	• -	• -	7.	-13.3	σ	-9.2	-P-6	نه	٠	0.1-	1 - 1	6-5-	L. 5-	-5.5	-5.4	-5.2	1-4-	-4.3	-3.9	4. 6		9 1	-2.2	-2.)	-1.6	-1.2	o•1-	9 0	្រ • (• ()	(EQ	3.6	3.6	3.5	3.8	4.3	C•7	و• و	٤.,	5•9
	WMAX I VUM	64.2	9.59	7.49	65.3	67.1	2.17	72.5	72.5	71.3	68.2	62.5	59.P	53.8	7.8°.	57.1) [62.1	6,.3	56.3	59.6	58.1	4-69	61.3	69.1	د.و۲) c	75.3	71.1	67.5	63.9	69.65	2.65	ر . د د د		, L.O.	50.7	60.4	65.3	76.9	79.5	79.4	77.6	74.4	64.2
# CHOR	Z .		.17	c١	. 7	•	٠.	• _	• •	•	,	σ.	ď		۲.	\$ ·) -	، در ن	4	4		C)	*1	ä	2.	?		•	•			•		•	 	•		•	٥.,	•	•	•		_:	•	c
4	MUNICANDA	4 3 3 3	a)	'n	۲.	3.46		٠,		•	•	Ξ.		~	ċ	œ.	, .	, ,	•	•	زي	÷	٠,	÷	÷.	۲,	•		•	`∼'	ŧ	;	e 1	22.3	, ,	, en			Ġ	٠	٠	٠,	en		.
T CHGRD	TANGENTIAL		14.	6.3	7.1	-12.5	•			· 61			-7.6	-7-1	5.6-	٠ ٠ ٠	٠ ري د د د د د د د د د د د د د د د د د د د	7.7-	- i - 7	-3.4	-2.1	a . [-	a. 7	£.0-	4 · ·	1.2		" (" • \c	1 a:	6.2	£.8	7.5	d • (n 0	. 60	. v.	9.5	5.t	6.6	10.5	11.0	11.4	11.9	12.4	13.1
SAMPLE	NUMBER	-	۰	3	4	w) ,	۰) (۱	- σ	n or	Ö	11	12	13	14	٠ <u>.</u>		- 0	13	٦ <u>٠</u>	21	22	23	72	25	26	72	2	, c) E	35	63	34	5°	36	י מ י ר	· 6	C 7	7	42	£ 3	1,1	4.5	46	7.7	es 25

TABLE 0-32(Contd)

58			RECORD MAXIMUM PRESSU	283 WALL JRE SAMPLE	JRD 283 WALL KULITE STEADY STATE PRESSURES SSURE SAMPLED = 116.5 KILOPASCALS = 16.88	r STATE PRI Kilopascai	ESSURES .S = 16.88	PS1		PAGE 4	
SAMPLE	PLE CHORD=	34.6	CHURD=	47.5	Z CHORD=	73.6	+00001	6			
NUMBER	TANGENT IAL	EMAXIM	UM TANGENTIAL	Z W X X M X	UM TAKGENTIAL	NI AVNA	TANCENTAR NO	9.66	= CHOKD	141.4	
	(086.)	PRESSU	(Dig.)	PRESSI	1016		TANCEN LAL	SHAX IMU	I ANGE ISTIAL		
67	٠. و	7.5.1			() ()	06637	10101	PRESSOR	(DEC.)		
			۲۰۰۱	0.0	¥•8	75.1	<i>م</i> ه	71.0	14-1		
<u> </u>	14.4	C 2 . L	15.7	53.6	9.2	7.00	3.1	7. 2			
21	15.1	60.6	16.6	57.7	, 0		• •	7.71	υ• •		
£ 3	7 9 1		÷ (16.	6.9	73.7	1.03 1.03		
ų (0 • 11	1.6	16.9	62.9	10.9	75.4	7.4	74.7	2 71		
53	.6.3	45.4	17.1	63.6	7 7	7.5	, ,) ·		
24	14.7	47	,		• • •		†	12.	16.3		
	, ,		\$ ·	0,0	12.1	73.4	16.7	75.5	16.7		
0		4.9.8	17.5	6).4	14.8	61.2	11.6	76.0			
95	17.3	52.8	9.0	67.1	- 4		•	•	2.11		
4.7	17.5				1.0	7.70	76	7.5.7	17.6		
		4.00	1 6.3	23.1	16.0	63.7	13.9	64.3	17.9		
מ	7.21	5.3	3° - 3	6.1.9	17.2	71.4	14.7	7 0 7	, ,		
29	19.0	51.6	7 91					500	0 · 0 ·		
4			•	7.10	9.11		15.4	6.99	18.9		
•	7.67	Y . O . Y	1.61	61.4	19.2	73.4	30.5	74. 7	6 31		
							1	•	5.64		

Constitution of the Consti % MAXIMUM PRESSURE CURVE CURVE LABEL VALUE 2 0.930000E+02 3 0.860000E+02 4 0.790000E+02 5 0.720000E+02 6 0.850000E+02 7 0.580000E+02 8 0.510000E+02 9 0.4400000E+02 10 0.370000E+02 MAXIMUM STATIC PRESSURE 116.5 KPa (16.88 PSI)

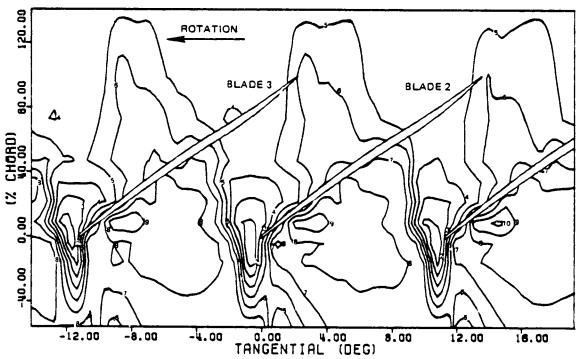


Figure D-19 Steady State Pressure Contours at Blade Tip; Out of Flutter, Low Operating Line, 85 Percent Speed, 85.8 Percent Flow, Pressure Ratio 1.3792

TABLE D-33

STEADY STATE STATIC PRESSURE FOR CONTOUR PLOTS

85% SPEED

RECORD 293

Inlet Total Pressure = 80,680 N/m^2 (1685 lbf/ft^2)

Axial Location (Percent Chord)	Static Pressure to Inlet Total Pressure Ratio
-55.4	0.901
-15.1	0.904
- 3.6	0.914
9.4	0.935
22.2	1.000
34.6	1.096
47.5	1.177
73.4	1.259
99.3	1.302
141.4	1.287

RECORD 293 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 110.5 K1LOPASCALS = 16.01 PSI

	(C	· · · · · · · · · · · · · · · · · · ·	
######################################	5.75 662.3 74.2 8.25.3 8.25.3 8.25.3 7.35.0	2 4 2 2 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1 4 4 W W E ;
TANGENTIAL (UEG.) -25.8 -25.2 -25.2 -25.5 -25.6 -25.6 -25.6 -25.6 -25.6 -25.6 -25.6 -25.6 -25.6 -25.6 -26.5 -26.5 -26.5 -26.5 -26.5 -26.5 -26.5 -26.5 -26.5 -26.5 -26.5 -27.6	115.2 115.2 115.2 115.2 116.2 116.2 116.3 116.3 116.3	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 0 0 0 0	1 M W W W W W W W W W W W W W W W W W W
### ##################################	61 172.6 178.6 96.3 96.3 196.5 196.5	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	54.20 51.30 52.70 52.70 61.90
TANGENTIAL (DEG.) -25.8 -25.8 -25.2 -24.5 -23.7 -21.5 -21			
୍ ବଳ ଅଧିକ ବଳ ବଳ ଅଧ୍ୟ ଦ୍ର ଅଧିକ ଦ୍ର ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ ଅଧିକ		n 2 m n 4 4 m 6 n c 4 c 4 4 m 3	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$
# CHORD# TANGENTIAL TANGENTIAL 1DE6.1 -25.6 -25.6 -22.8 -22.8 -22.5 -22.5 -22.0 -21.3 -21.	111111111111111111111111111111111111111	11 11 11 11 11 11 11 11 11 11	000000000000000000000000000000000000000
# -15.1 #MAXIMUM PRESSURE #9.6 #9.6 #9.6 #9.7 #9.7 #9.7 #9.7 #9.2 #9.2 #9.2 #9.2 #9.3			55.0 50.0 50.0 50.0 50.0 50.0
TANGENIAL TANGENIAL 1066.) 1066.) 125.3 -24.1			
200 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1) 4 4 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	F = K = 8 F S
# CHORD= TANGENTIAL 25.8 -25.8 -25.5	1		2 + 5 3 1 1 1 1 2 2 3 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
mioc.			0 1 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

RECORD 293 WALL KULITE STEADY STATE PRESSURES MAXIMUM PRESSURE SAMPLED = 110.5 KILOPASCALS = 16.01 PSI TABLE 0-34 (Contd)

		C	MAKINUM PRESSI	PRESSURE SANFLED	1	Tree wire vices		•		
3 JAPIE	X CHCRD=	-55.4	# CHURD=	-15.1	CHORD=	-3.6	# CHORD=	4.6	CHORD≈	
MAFR	TANGENTIAL		TALCENTIAL	TMAX IMUM	TANGENTIAL	EMAXIMUM	TANGENTIAL	KHAX IMUM	TANGENTIAL	ZHAX IMUM
•	(DEG.)	PRESSURE	DEG	PRESSURE	(DEG.)	PRESSURE	(0EG.)	PRESSURE	(DEG.)	PRESSURE
07	\$ 4 V	6.5.3	6.9	54.	4.2	54.8	٦.٢	15.8	4.7	51.0
i u	4,6	6.43		9.69	4.0	59.8	8.1	19.9	5.3	54.1
. r	4.6	54.2		89.3	6.1	65.9	9.5	86.3	e. 3	57.1
, ,	, c,	55.6	6.6	5.68	7.1	72.2	16.9	45.64	6. 6	62.6
, נ י		45.06	(6.06	7.9	17.2	11.9	87.4	7.3	2.69
1 4		73.0	11.4	8.5.1	8.7	ਰ•68	12.4	78.1	8.3	75.1
· u	10.0	6.6	11.7	1.69	10.3	7.70	12.7	65.8	4.6	ار د د د
· 4	6.0	40.2	12.3	56.6	10.8	85.9	13.2	47.6	7.6	65.1
, <u>,</u>	101	0.46	12.7	53.4	11.0	76.7	14.0	38.2	15.2	9-83
• •	11.4	0.00	12.9	58.9	11.6	6 P . B	14.9	41.4	11.1	40.5
o or	6-1	8,24	13.8	29.50	11.3	61.4	15.9	49.5	11.9	9 1. 0
: (. : .c	9 6	15.8	14.4	54.3	11.8	51.8	16.5	52.2	12.6	7.76
3 7	13.5	71.9	15.0	52.9	12.3	57.5	17.1	56.2	13.4	6.53
, () 4	13.7	67.4	16.1	52.8	13.6	55.4	17.4	61.1	13.9	73.3
) (14.2	44.6	16.7	52.0	13.6	56.9	17.8	6.59	14.4	0.63
44	14.66	62.2	17.7	53.2	14.3	54.1	17.9	68.U	14.9	48.8
. 6	1,4,1	6 , 5	18.2	56.1	15.1	55.1	18.0	9-67	15.5	52.3
) -Q	60	58.5	18.5	54.8	15.9	54.5	18-1	71.3	16.1	7364
29	1001	57.1	16.7	62.2	17.0	59.5	18.3	73.4	47.3	55.2
6.0	17.4	56.2	18.8	64.3	17.5	64.2	18.5	74.5	17.6	2.9.
69	10.7	55.3	18.9	65.9	18.0	69.1	18.7	75.8	19.3	63.2
0.4	19.1	54.2	19.1	67.2	19.1	73.6	19.1	11.1	19.1	71.3

ONIGHEST PAGE IS OF POOR OUNCER

RECORD 293 WALL KULITE STEADY STATE PRESSURES
MAXIMUM PRESSURE SAMPLED = 110.5 KILOPASCALS = 16.01 PSI

			T.	•	16	KILUPASCAL	u s	I S d		
AMPLE.	H 2	34.6	₹ CHOR	*	CHO	73.4	는 H	99.3	T CHOR	14104
¥ 20 50	OFG.	- S	F 7	PRESSURE	(DEG.)	PRESSURE	I ANGENITAL (DEG.)	EMAXIMUM PRESSIRE	TANGENTIAL	WHAX IMUM PRINCINE
~	a	P 4.2	٠	84.5		95.3	, ω	6.46	Ņ	91.6
~		~	3	86.6	Ġ	•	-75.1	•	-25.2	-
٣			•	89.1		95.7		5	• •	•
•		۳ì	23	8.68	-24.3	Š			-24.2	
Λ,		٠,	<u>.</u>	8°06		(1)		•	r.	•
o 1		<u>.</u>	Ň.	91.2	•	•	-22.2	۲.	~	•
► (Č.	<u>:</u>	91.2	<u>.</u>		-21.4	•		Š
3 0 (D	•	4.00	-22.4	91.1	-26.0	Ġ		1.26
o- 4		m.		٠,٠	<u>.</u>	•	75.07	45.4	G.	. P
c :			<u>.</u>	9.06	-21.5	_	-19.4	٠	w	45.1
((•		Å.	a. 1	6.68	÷.		O.	٠	_	•
<u> </u>		÷.	:	85.7	٠.	92.1	ක		~	'n.
٠. :		÷.	•	٥.	19.	•	~	4.40	•	'n
5 .		₹,	٠.	76.3	= ;	-		•	u١	•
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- 0	• •	:		. I .	پر ۱	94.1	•)		\sim	
a. (_ :	٠.	•	83.1	÷ .		•	•	-11.3	
<u>-</u>	= :	~.		84.4	3.	•	m		٠.	
7.	_ ,	•		96.3	ر ځ	•	-12.1	٠	œ	•
	C.6-	•	•	87.6	-12.2		~	•	፟	•
22	~ ,	•	•	83.5		87.5	20	•	-	;
£ .	- 1	:		89.6	<u>.</u>	-	-10.0	•	-7.4	ë
·	_	ᆣ.		P8.3	ċ	_	-9.3	•	7.9-	2
4. ·	- 	∹.		1.78	Ġ.		8°0'-	•	-6.3	•
91	7.9-	•	•	87.9	8		-8-2	•	-5•3	7
- 6	· · ·	•	•	88.	•	9.7.6	T. L-	•	9.4-	2.
n (12 · 5 ·	•	ພ .	87.2			٠٠٠-		5°**	•
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1 6) · ·	•	, 1	2.0		_	7	1-76	6.	~) :
3 2		• -	•) () (1.5-1		٠ ٠ ٠	5 ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° ° °	*	'n.
. (c	-	• •	2 4	4.77	9.7	0 00	v٠.	40.0	F (•
36	2.4			8 8			٠.	6.00	7 6	; ,
75	3.2	86.3	7.2-	79.6	L. 0-	66.2		0.00		4 4
33	0.4	•	6	80.2	-6.3		104	7-75	2.7	
33	4.6	. •	-2.9	61.6		97.0	2.2	92.7	en en	
4.0	6.4	. •	ç	R2.9			2.7	43.0	. P.	
1,	£. 6 4	. •	_	65.1	1.0		3.6	~	4.1	93.0
25	6.1	•	<u>.</u> -•	86.2	•	_	1.4	92.3	4.6	3
43	6.5	٠	2•3	97.1	•	9::1	5.7	3.	5	Ġ
77	6.9	٠	ر • د	B7.2	•		6.5	ë.	5.4	92.B
4.5	7.2	٠	e -	97.0	٠	÷		,	5.9	2
9 !	3° /	•		P7.4	6.4	•	٧٠,	*	•	2.
1	4 · · ·	•	,; •	8 1 8	•	٠	۲.1	6.26	6.9	•
n 4	5.5	•		86.2	•		4.1		•	2

		r	RECORD MAXIMUM PRESSI	DRD 293 WALL KU ESSURE SAMPLED	DRD 293 WALL KULITE STEADY STATE PRESSURES ESSURE SAMPLED = 110.5 KILOPASCALS =	F STATE PRFS KILOPASCALS	FSSURES LS = 16.61	PSI		PAGE 4
ANDLE .	TANGENTTAL		TANGENTIAL	47.5 EMAXIMEN	Z CHORD≃ TANGENTIAL	73.4 ZMAX IMUM	TANGENTIAL	99.3 ZMAXIMUM	TANGENTIAL	141 c4
	(DEG.)	PRESSURE		PRESSURE	(DEG.)	PRESSURE	(DEG.)	PRESSURE	(DEG.)	PRE SSURE
67	16.2	7 - 9 A	5.0	87.3	6.7	92.5	16.3	95.9	1.9	91.8
ę,	11	30.7	5.t	94.6	7.4	93.3	11.	6-56	B.4	61.6
-4 (V)	12.0	51	ى د د	81.7	7.8	93.6	11.9	96.5	E - 7	92.2
55	.2.9	5.00	6.3	77.3	8.8	4.76	12.7	95.8	5.1	45.6
53	13.8	47.7	\$. 9	76.1	4.6	94.1	15.2	95.5	5.2	65.8
24	14.5	86.7	7.1	79.8	6.6	92.4	15.7	95.2	4.7	93.3
5.5	15.2	P3.4	7.4	e1.0	10.3	89.3	14.3	4.40	16.e	45.9
92	8° u i	73.7	8.1	82.9	10.6	E7.7	14.9	93.6	17,6	93.0
57	16.1	61.2	ۍ• ص	84.7	£0.8	87.1	15.4	43.5	11.5	43 54
6 ;	16.6	51.3	6.6	86.4	11.4	88.3	16.0	43.4	11.7	53.7
20	16.9	6.95	1'.7	69.0	11.7	89.4	10.6	93.7	6.14	94.1
(9	17.2	51.3	11.7	88.3	12.4	0.06	16.9	44.1	12.4	94.5
61	17.5	54.6	15.0	88.6	12.9	9∴•5	17.3	4.46	13.0	2.46
62	17.71	e. 81	14.1	88.7	14.0	5. 06	17.7	6.55	13.8	93.9
63	38.0	62.F	15.6	88.7	14.9	9.68	೧• ೫ (95.1	14.3	93.8
79	18.3	4.99	16.3	87.5	15.8	26.7	18.2	95.2	15.1	93.9
6.5	15.6	0.49	17.1	80.7	16.3	91.6	18.4	95.3	16.0	93.1
66	10.0	71.7	17.5	74.0	16.8	42.7	18.6	45.4	i 6 . 8	92.5
19	1 8 • 3	T2.7	17.3	72.5	17.4	95.9	18.7	45.6	17.3	4.65
9	18.8	73.5	18.3	7.97	18.1	93.5	18.8	95.5	18.2	92.1
63	38.9	74.4	18.5	19.0	18.6	65.6	15.6	95.5	18.7	22.0
7.0	16.1	75.7	19.1	8.1.2	19.1	4.46	19.1	95.5	19.1	92.3

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OF Pur

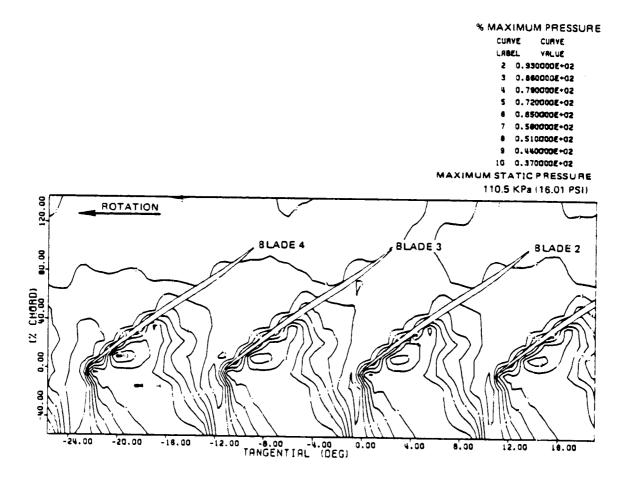


Figure D-20 Steady State Pressure Contours at Blade Tip; Out of Flutter, High Operating Line, 85 Percent Speed, 75.1 Percent Flow, Pressure Ratio 1.4862

OF FULL

APPENDIX D

PART 2

UNSTEADY PRESSURE

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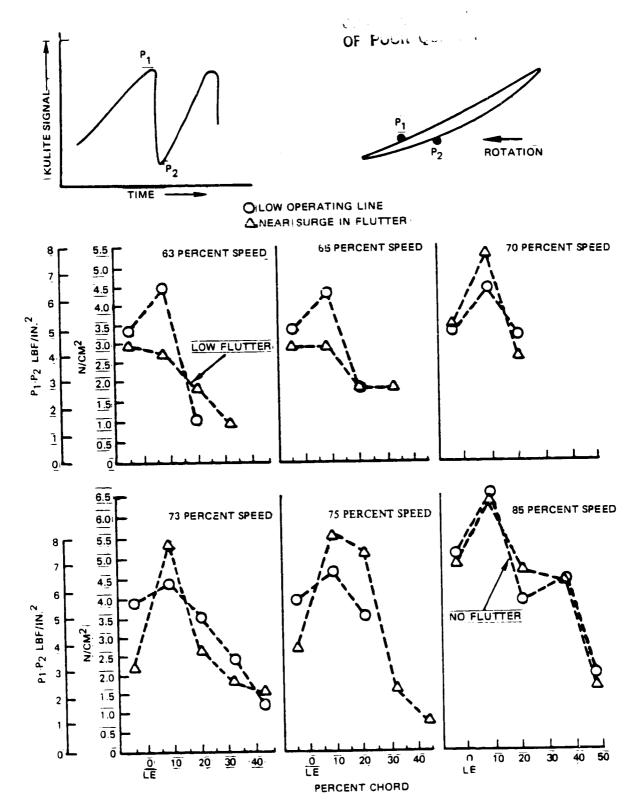


Figure D-21 Steady Pressure Differential Between Pressure and Suction Surfaces at Operating Conditions In and Out of Flutter

BLADE MUNNTED KULITE SENSOR FLUTTER DATA SURVEY

																	C O		ŀ	Ů	•			,							
	Pridse Dolative to	Strain Gage on Blade 3	(Degrees)	,	S	04	18	2 (188 '		205	143	89	336	687	262	e S	•	• •	221	268	297	350	51		1 92	3 '	• 1	11/ 166	, ,	104
1	Unsteady	Amplitude	(lbf/in)	150	120	75	4 4	;	[6 '		٠ رور	27	32	84.	4	120	110	•	•	63		65	60	57		- 260	3 '	•	₩	;	S.
75	Unsteady	Pressure Amplitude	(N/cm)	103.42	82.74	51.71	33.10	06.02	62.74	1	22.00	49.64	22.06	33.10	30.34	82.74	75.84	•	•	59.98	51.02	44.82		39.30		30 021	07.6/1	•	33.10	?	34.47
	Phase	Relative to Strain Gage	(Degrees)	Ŋ	, c	12	37	2	162	•	1 1	195 163	63	324	282	•	•	,	•	220	231	247 247		353 51	•	253	80 I	•	119	/61	120
Percent Speed	Unsteady		(1bf/in)	08.	1 43	4 8	25	36 37	37	I	1 !	185	2 2	36	44	•	•	,		48	34	4 8		25 V	2	3	102	ı !	32	3	508
73	Unsteady	Pressure Amplitude	(N/cm)	55.16	, ,	33 10	35.85	26.89	25.51	•	•	127.55	50.33 16.55	26.89	30.34	•	ı		•	$\overline{33.10}$	23.44	23.44	· • •	35.85	90.77	21.37	70.33	ı (22.06	25.51	143.41
Speed	Phase	Relative to Strain Gage	on Blade 3 (Degrees)	357	1 (νā	46	15	180	•	1	129	131	316	260	•				225	240	273	8	101	c C	•	13	ı	136	178	93
67 Dordont Sp		Pressure Amplitude	(lbf/in)	96	•	92	2° 9	4	32	•	,	62	32	٠ %	2,8	63	74			٠ ٥٢	47	38	90	220	88	•	18	1	. 16	31	52
1.3	Incted	Pressure Amplitude	(N/cm ²)	64.81	; ; ; ;	52.40	38.61	28.27	24.13		•	42.75	25.06	17 03	17.93	73 53	50.34 51.02		1	9 0	32.41	26.20	79.67	151.69	26.20	•	12.41	•	21.37	21.37	17.24
	UC.		Blade Slot and Surface	9,6300	7				2 convex	5	200000	3 COHACA					3 concave		4 concave					4 convex		Z G C C Z					6 convex
:	Sensor Position	Percent Chord From	Leading		. 51	: \$ 2	4 0	88	ي	25	u	ი აქ	52	6 0	5 9 6	}	52		2	15	£ \$	92 9	06	S	25	u	15	\$2	3 4	38	33
	3	Dorron	Span Span From Hub		₹ .														86.3												

TABLE 0-36

RECORD 239 WALL KULITE NONSTEADY PRESSURE AMPLITUDES MAXIMUM PRESSURE SAMPLED = 3.13 KILOPASCALS = 0.454 PSI

PAGE 1

22.2 EMAXIMUM PRESSURE	9-14	æ ;	22.5	36.3	1.44	22.5	9. y	0.4	8	22.5	19.4	26.2	33.6	0.05	4.4	12.6	12.6
# CHORD# TANGENTIAL (DEG.)	-21.03	-18-8	-16.3	-:3.7	-11.2	-8 -8	-7.5	-6.2	-5.0	-3.7	-2.5	-1.2	7.3	1.3	7.6	3.8	5.1
9.4 EMAXIMUM PRESSURE	63.0	22.5	43.8	28.2	31.7	7.9	20.02	6-6	54.9	1.3	6.6	2C •0	20.0	89.2	83.0	41.6	16.5
# CHORD= I TANGENTIAL (DEG.)	-22.9	-26.4	-17.9	-15.4	-12.9	-1 (• • 4	-9.i	6-1-	9-9-	15.4	-4.1	-2.8	9.!-	-0-3	٥- ر	7.2	3.5
-3.6 EMAXIMUM PRESSURE	35.5	1.09	25.1	25.1	35.5	56.2	77.5	25.1	14.1	5.1	14.8	22.5	15.9	39.0	56.2	0.001	22.5
# CHORDS TANGENTIAL (DEG.)	-25.0	-22.4	-19.9	-17.4	-14.9	-12.4	-11.2	6.6-	9.6	-7.4	-4.1	6.4-	-3.6	-2.3	-1.1	0.2	1.4
-15.1 #MAXIMUM PRESSURE	26.9	26.9	26.9	12.1	21.4	32	28.1	9.5	24.0	15.2	16.9	21.4	11.2	13.4	17.0	26.9	8.9
CHORD= TANGENTIAL (DEG.)	-26.4	-23.9	-21.4	-18.9	-16.4	-13.9	-12.6	-11.4	-10.1	80	-7-6	-6.3	-5-1	80	-2.5	-1.3	00
-55.4 #MAXIMUM PRESSURE	29.1	23.6	14.5	16.3	12.6	25.3	14.5	15.9	12.6	22.5	16.7	14.1	5.3	7.1.5	43.8	31.7	12.0
TANGENTIAL (DEG.)	-32.3	8.66-	-27.3	-24°B	-22-3	-19.7		-17.2	-16.0	-14.7	3 - 1 -	-12.2	0,0	7.6-	4, 9-	ر ر -	-5.9
SAMPLE NUMBER		~	•	٠ ٧	٠ ٧٠	٠.	· ~	· œ	. •	. 6	: =		· ~	7 7	· ·	\ <u>\</u>	12

RECORD 239 WALL KULITE NONSTEADY PRESSURE AMPLITUDES MAXIMUM PRESSURE SAMPLED = 3.13 KILOPASCALS = 0.454 PSI

141.4 Emaximum Pressure																	
# CHORD= TANGENTIAL (DEG.)	-4-3	-1.7	a • 0	3.3	5.8	8.3	9.6	10.3	17.1	13.4	14.6	15.9	17.1	16.4	19.6	7: 0	22.1
99.3 ZMAXIMUM PRESSURE																	
# CHORD= TANGENTIAL (DEG.)	-16.4	-7.8	-5.3	-2.4	-(.,3	2.2	4.	4.7	ۍ 9	7.2	¥ ; 60	2.5	11.0	12.2	13.5	14.8	16.0
73.4 Zhax Imum Pressure	23.8	35.2	38.3	37.3	37.0	35.2	38.8	39.6	37.9	35.2	35.2	32.2	29.3	22.2	31.5	31.5	54.9
\$ CHORD= TANGENTIAL (DEG.)	-13.9	-11.4	6.8-	-6-3	-3.8	-1.3	٦٠.	-	2.5	3.7	5.0	6.2	7.5	œ.	10.0	11.3	12.5
47.5 #MAXIHUM PRESSURE	24.0	10.8	33.9	33.9	33.9	17.6	21.6	30.2	26.9	28.9	23.9	33.9	27.5] · · · B	71.4	21.4	18.9
T CHORD= TANGENTIAL (DEG.)	-17.7	-15.2	-12.7	-1, -5	T.T-	-5.1	-3.9	-7.6	-1.4	10.7	1.1	5.4	3.7	6.4	۴.	1.4	h.6
34.6 EMAXIMUM PRFSSURE	•																
T CHORD= TANGENTIAL	-19.4	-16.9	-14.4	8-11-	-9-3	8-9-	-5.5	-4.3	-3•.	8	-0-5	6.0	2.0	3.2	7.4	5.1	7.0
SAMPLE	-	~	, m	. 4	5	•	7	- œu	•	13							1.1

TABLE 0-37

RECORD 239 WALL KULITE NONSTEADY PRESSURE PHASE TO STRAIN GAGE 3

HASAL DEST 32.4.5 35.4.5 35.4.5 35.6.5 36.5 36.5 36.5 36.5 36.5 36.5	
# CHORD= TANGENTIAL 16.03 -1.3 -1.3 -1.3 -1.3 -1.3 -1.3 -1.3 -1.	
99.3 CDEG. D 2888.0 2888.0 307.0 315.0 20.0 27.0 27.0 27.0 81.0 99.0	
# CHORD= # CHORD= # Chord Ch	
73.4 10EG.) 270.0 270.0 270.0 286.0 313.9 351.0 0.0 18.0 18.0 72.0 63.0	
TANGENTIAL 10EG.) 113.9 -113.9 -13.9 -13.9 -13.9 -1.3 -2.3 -1.3	i I
47.5 PHASE 10EG.) 261.0 275.0 275.0 333.0 333.0 353.0 353.0 353.0 353.0 353.0 353.0 353.0 353.0))
CHORD= TANGENTIAL LDEG.) -17.7 -15.2 -17.7 -16.2 -2.6 -3.9 -2.6 -1.4 -0.1 1.1 2.4 9.4) •
34.6 (FEG.) (FEG.) 16.3 2261.0 2261.0 396.0 326.0 326.0 326.0 326.0 326.0 326.0 326.0 326.0	•
CHORD# (FEG.) -19.4 -16.9 -14.4 -14.4 -1.5 -5.5 -5.5 -5.5 -5.5 -6.8 -6.8 -6.8 -6.8 -6.8 -6.8 -6.8 -6.8) • • • • • • • • • • • • • • • • • • •
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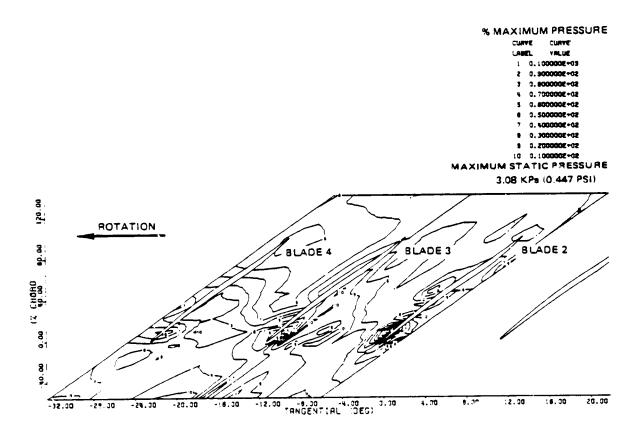


Figure D-22 Nonsteady Pressure Contours at Blade Tip; in Flutter, High Operating Line, 66 Percent Speed, 54.5 Percent Flow, Pressure Ratio 1.260



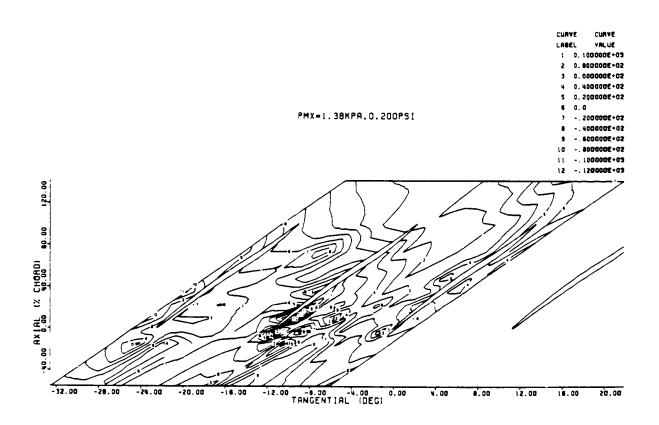


Figure D-23 Nonsteady Real Pressure Contours at Blade Tip; In Flutter, High Operating Line, 56 Percent Speed

OF POOR QUALITY

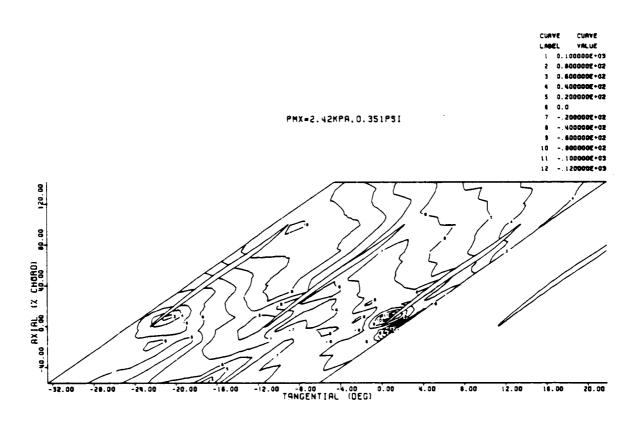


Figure D-24 Nonsteady Imaginary Pressure Contours at Blade Tip; In Flutter, High Operating Line, 66 Percent Speed

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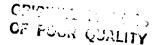
		r	RECORD MAXIMUM PRESSU	220 WALL I	RECORD 220 WALL KULITE NONSTEADY PRESSURE AMPLITUDES Pressure sampled = 5.02 Kilopascals = 0.728	ADY PRESSI Kilopascai	RE AMPLITUDE .S = 0.728	is PSI		PAGE 1
SAMPLE	# CHORD≈		CHORD≠	-15.1	Z CHORD=	-3.6	CHORD=	9.4 MINIX	TANCENTIAL	
NUMBER	TANGENT I AL	EMAXIMUM	TANGENTIAL	MAXINON	TANGENT IAL	ZMAX IMUM	JANGENIJAC 1616			30177100
	(050)	PRESSURE	(OEG.)	PRESSURE	(DEC.)	PRES SUR E	(DEG.)	PRESSURE		12.5
-	4.66-	3.0	-27.1	10.2	-25.5	50.1	-23.7	30.0	917-	
. (. 06 -	7 51	-24-6	9.5	-23.0	47.B	-51.5	100.0	-19.4	21.3
y (2,7	() (-26.5	30.2	-18.7	19.1	-16.8	6.7
~	9.17-		7077			74.1	-16.2	19.1	-14.4	15.0
4	-55.3	13.6	0.31	c•21	- u		-1:1-	25.7	6,1,-	25.5
\$	-22.B	10.2	-17.1	**	C*CT-	7.00		7,7	7-0-	24. B
•	-20.3	8.0	-14.6	10.0	-13.0	35.0	711-	2 1		
,	101-	12.2	-13.4	11.1	-11.8	60-2	6.5-	83.1		0.07
- (7 7	-12.1	12.5	-10.5	10.2	-B.7	41.6	6.9-	14.6
B (r .		0 0 0	, c	-6.5	14.4	-7.4	17.3	-5.6	9
~	9.01	19.0	K - 17	9 0		7.6	-6.2	16.3	-4.3	12.0
0[5.0.	E 4	7 7 7	, ,	4	10.4	6-4-	15.8	-3.1	10.7
[]	1.41-	0.21				15.1	-3.7	12.0	-1.9	19.0
21	9.71-	7.71			7-7-	13.5	-2.4	26.2	9.0	15.8
13	-11.6	:	F .	•			-1.7	30.2	9•0	16.5
14	-10.3	6.4	9.4-	9.	0 0			300	6.	16.9
15	7.6-	9°8	# · m	7. • •	0 1	1.0		7 67		14.9
16	-7.8	6.2	1-2-1	0.01		25.1	1.03	0.10	1 .	, ,
17	9-9-	10.4	6.3-	14.4	7.0	19.1	5.6	9.	£.	£2.53

		I	RECORD 220 WALL KULITE NONSTEADY PRESSURE MAXIMUM PRESSURE SAMPLED = 5.02 KILOPASCALS	220 WALL I URE SAMPLEI	KULITE NONSTE	ADY PRESSI KILOPASCAL	JRE AMPLITUDES	ES PSI			
31447	# CHORD=	34.6	# CHORD=	47.5	# CHORD=	73.4	# CHORO=	99.3	CHURD=	141.4	
NUMBER	TANCENTIAL	SMAXIMUM Springer	TANGENTIAL	# ā	TANGENTIAL (DEG.)	MAXIMUM PRESSURE	TANGENTIAL (DEG.)	EHAXIMUM PRESSURE	(DEG.)	PRESSURE	
•	1 DEC.	16.5	-18-3	5.6	-14.6	80.83	-11.0	23.4	-5-1	19.0	
۰ ،	4 6 4		8.51-	13.5	-12.2	8	-6.5	22.8	-7.6	16.9	
v (o d		23.4	7.6-	11.1	3.9-	21.7	ب ۲	10.4	
۰,	1000			30.5	-7.1	4.8	-2.5	19.8	5.4	12.9	
•	0.77-	6.13		26.1	7	7.0	-1.0	19.8	6. 4	14.4	
Λ,		200	7 (u	13.0	-2.1	6.7	1.5	15.8	7.4	15.1	
ء م	0 -	7 6	3 - 7 -		6 0	0.9	2.7	17.7	F • J	15.1	
~ (•	• 0	ריי	17.3	0.3	4. 8	0.4	19.0	6.6	12.2	
1 0 (4 6 6 6		֓֞֞֜֜֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	7.1.	9	7.6	5.3	17.7	11.2	12.5	
~ ;	* · · ·		- C	14.7	- C	6.7	6.5	17.3	12.5	15.1	
2:	9.7-	15.		18.5	4.1	6.3	1.1	17.7	12.7	12.0	
- († •			5.0	5.4	7.0	0.6	17.3	14.4	12.9	
71:	- -	100	- 3	15.1	9 9	9.0	16.3	14.0	16.2	12.0	
:	(0 6	` · ·	14.7	7.8	9.9	11.5	16.9	17.4	12.0	•
•	***	2 2 2	• •	۲,	9.1	6.4	12.8	17.7	18.7	13.5	
<u>.</u>	e •		-	0	10.4	2.5	14.0	15.8	19.9	4.5	
9 [6-1	- *	. J.	E	11.6	6.3	15.2	17.7	21.2	9.5	

OF FULL -

																			`	Ji	٠	-																						
22.2 PHASE	(DEG.)	0.411	0.676	276.6	0 200	201.00	0-107	7,44) · · · ·	131.0	32.0	36.0	24.0	27.0	16.0	328.0	297.0	53.0)))					141.4	PHA SE	(DE G.)	360.0	315.0	333.0	0 (2	0.00	26.0	0.0	0.4	ر د د د د د د د د د د د د د د د د د د د	65.J	91.0	o. %	45.0	6. ک	158.0	95.0	
TANGENTIAL	(Of 6.)	9-17-		7.71-			* • •		6.9	-5.6	-4.3	-3.1	-1.9	9°9-	9•0	1.9	3.1	4-7	•					# CHORD=	T ANGENTIAL	(DEG.)	-5-1	-2.6	Y	2.4	5. 1	* (.	6° 6	11.2	17.5	13.7	14.4	16.2	17.4	18.7	19.0	•	
9.4 PHASE	(DEG.)	7,50	162.0	0.100	2000	0-882	0.012	225.0	0.631	29.0	135.0	0.0	45.0	348.0	351.0	333.0	288.0	233 0	•				M	99.3	PHASE	(DEG.)	285.0	301.3	303.0	315.0	333.0	0-4	18.0	12.0	18.0	79.0	27.0	36.0	~	3	65.0	0.36	0.66	
TANGENTIAL	(DEG.)	7-53-1	7.17-	-18-	7.01-	-61-	2.11-	6.6-	-e-1	-7.4	-0.2	6.4-	-3.7	-2.4	-1.2	0.1	1.3	•						★ CHORD=	5	(066.)	٠١١-،	-8.5	0.9-	-3.5	J. 1-	S	2.7	4.0	5.3	6.5	1.1	ن 6	17.3	11.5	12.8	14.0	15.2	
-3.6 PHA SE	(DEG.)	208.0	0.171	338 0.00	0.212	279.0	773.0	234.0	72.0	27.0	216.0	20.0	351.0	0.0	ن • ن ن	18.0	342.0							73.4	PHASE	(DEC.)	259.0	294.0	296.0	297.0	315.0	318.0	351.0	0.0	351.0	o• 6	27.0	27.0	36.0	27.0	27.0	83.0	95.0	
# CHORD= TANGENTIAL	(DEG.)	-25.5	-23.0	-20 - 5	0.81	-15.5	-13.0	-11.8	-10.5	-9.2	0.8-	-6.8	-5.5	-4.3	-3.0	66	ا ا ا	,	•				TEADY PRESSURI		TANGENTIAL	(050.)	-14.6	-12.2	T.6-	-7.1	-4.7	-2.1	٠٥-	0°3	1.6	2.8	4.1	5.4	9•9	7.8	9.1	10.4	11.6	
-15.1 PHASE	(DEG.)	173.0	193.6	153.0	131.0	180.0	288.0	272.0	261.0	234.0	201.0	225.0	234.0	315.0	0.0		0 876	0.00	•				LITE NONS	5-17	PHASE	(OEC.)	216.0	289.0	279.0	288.0	289.0	565.0	63.0	5°0	9.0	9.0	0.6	0.0	Ç.0	0	333.0	144-0		
T CHORD=	(DEG.)	-27.1	-24.6	-22.2	9.61-	-17.1	-14.6	-13.4	-12.1	_		•	-7.1	6.6-	4.4-	4 -	•	v	6.0-				220 WALL	a CH	TANGENTIAL	(066.1	٣.	-15.8	-13.3	-10.8	-8.3	-5.R	-4.5	-3.3	-2.1	-0.8	0.5	1.7	9.0	4.2	408	6.7	: :: :::	
-55.4 PHASE	(086.)	•	S	149.0	179.0	93	~	S	127.0	203.0	257.0	241.0	0.075	256.0	261.0	372.0	0.016	0.017	0.922				RECOR	4	DH A CE		225.0	108.0	272.3	279.0	288.0	270.0	162.3	54.0	72.0	•		0.6	C C		351.0	270.0		
CHORD=	(DEG.)	-32.8	-30.3	-27.8	-25,3	-22.8	-20.3	-19.1	-17.8	-16.6	-15.3	-14.1		•			7 6	D.	٠							(DEG.)		-17.6	-15.1	-17.6	-10.1	-7.6	4.9-	-5-1	, c,	-2.6	4, 1		-	7 6	, ,		• (
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TABLE 0-39



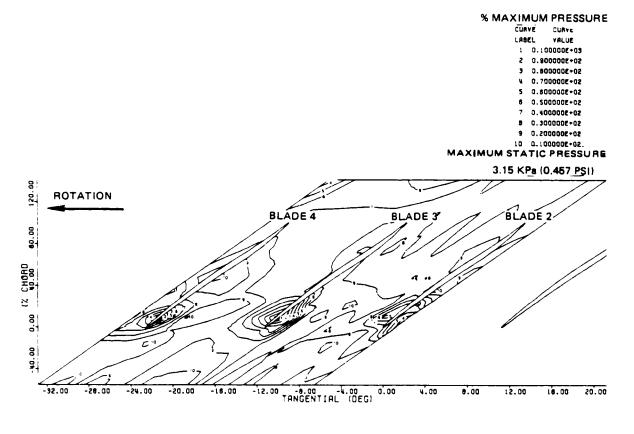


Figure D-25 Nonsteady Pressure Contours at Blade Tip; In Flutter, High Operating Line, 70 Percent Speed, 56.5 Percent Flow, Pressure Ratio 1.2978



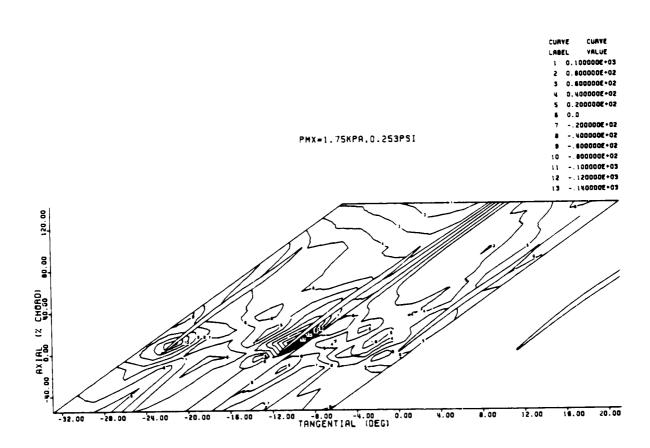


Figure D-26 Nonsteady Real Pressure Contours at Blade Tip; In Flutter, High Operating Line, 70 Percent Speed

Of For

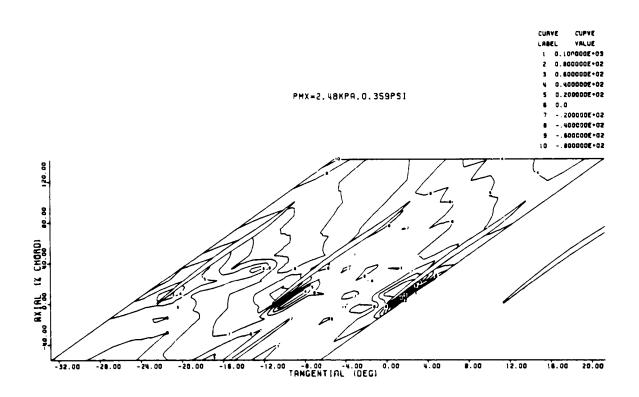


Figure D-27 Nonsteady Imaginary Pressure Contours at Blade Tip; In Flutter, High Operating Line, 70 Percent Speed

PAGE 1	22.2	PRESSURE	31.5	15.9	19.9	22.1	44.7	3.0.5	31.5	10.1		14.1	6.61	35.6	35.6	31.5	10.1	7.2	14.1
	# CHORD=	(DEG.)	-21.5	-19.0	-16.5	-14.	-11.5	C. 6-	T.1-	اد.۶	-5.2	-3.9	-2.7	4-1-	-0-2	1.1	2.3	3.6	4.5
is PSI	4.6	PRESSURE	1-44	56.4	8.9	13.9	19.9	39.8	63.3	7. 6	15.9	39.3	4.5	22.4	17.9	39.8	100.0	44.7	10.1
RE AMPLITUDES S = 0.447	X CHORD=	(DEG.)	-23.2	-20.7	-16.2	-15.7	-12.1	-11.9	4.6-	-8-1	6-9-	-5.6	4.4-	-3.1	-1.9	9•0-	9•0	5.1	3.1
ADY PRESSURILLOPASCAL	-3 .6 -4 . 4 . 4 . 4 . 4 . 4 . 4 . 4 . 4 . 4 .	PRES SURE	25.1	25.1	31.5	17.9	25.1	39.3	50.1	7.2	35.6	8.1	8.1	19.9	10.1	11.2	50.1	14.1	79.4
CORD 105 WALL KULITE NONSTEADY PRESSURE AMPLITUDES RESSURE SAMPLED # 3.08 KILOPASCALS * 0.447	CHORD=	(DEC.)	-25.2	-22-1	-20.1	-17.6	-15.1	-12.6	-11.4	-10.1	-8-9	-7.6	4.9-	-5.1	-3.8	-2.6	-1.3	٠,	1.2
105 WALL I	-15.1	PRESSURE	22.4	34.8	19.5	28.2	22.4	21.5	31.5	35.6	22.4	22.4	19.9	17.9	10.1	17.9	27.4	35.6	28.2
RECORD 105 WALL KUN MAXIMUM PRESSURE SAMPLED	TANCENTAL	(066.)	-26.7	-24.2	-21.7	-19.1	-16.6	-14.1	-12.9	-11.6	-10.4	1.6-	-7.8	9-9-	-5.3	1.4-1	-2.8	-1.6	-0-3
Ì	-55.4	PRESSURE	8.9	6.7	28.2	22.4	10.1	5.6	7.2	44.7	21.5	44.7	31.5	31.5	17.9	12.5	7.2	8.9	15.9
	# CHORD=	(DFG.)	-32.5	0.05-	-27.5	-25.0	-22.5	2002-	-11.7	-17.4	-16.2	6.4:-	-13.7	-12.4	-11.2	6.6-	-8-6	7.4	-6.1
280	SAMPLE	N S C C C C C C C C C C C C C C C C C C		7	m	4	Ś	•9	^	ພ	•	0.	11	12	13	7.	15	16	17

RECORD 105 WALL KULITE NONSTEADY PRESSURE AMPLITUDES
MAXIMUM PRESSURE SAMPLED * 3.08 KILOPASCALS * 0.447 PSI

	141.4	MAXINGM	RESSURE		65-6	62.9		67.0 45.4 48.4	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0 4 4 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	**************************************	**************************************	๑๕๘๖๒๔๖๑๒๒ ๙๙๙๛๛๛๛ ๛๛๛๛๛๛๛๛๛ ๛๛๛๛๛๛๛๛๛๛๛๛๛๛	๑๕๘๓๓๓๓๓ ๑๘๘๒๓๓ ๑๘๘๒๓๓๓๓๓๓๓ ๛	๛๛๛๛๛๛๛๛๛๛๛๛๛ ๛๛๛๛๛๛๛๛๛๛๛๛๛ ๛๛๛๛๛๛๛๛๛๛	๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ ๛๛๛๛๛		๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ ๛๛๛๛๛	៰៹៹៳៹៹៳៙៙៙៰៸៰៸៰៳៙៙៸ ៴៴៶៴៙៹៹៶៰៳៳៹៶៰៳៰៹៸៰៸៴៰៳៙ ៰៹៹៹៹៸៰៶៰៶៰៶៰៶៰៶៰៰៰៰៰៰៰៰៰៰៰៰៰៰៰៰៰៰៰៰៰៰៰
	# CHORD=	IN TANGENTIAL	(DEC.)	-4.5	-2.0	۳. د د	3.0	5.5	9	9.3	10.5	11.8	13.1	14.3	15.6	16.3	18.1	19.3	20.6	
•	99.3	EMAXIM	PRESSUR	53.5	67.3	69.0	60.09	53.5	42.5	37.8	47.5	42.5	42.5	37.9	37.8	47.5	37.8	42.5	42.5	
	# CHORD=	I TANGENTIAL	(DEG.)	-10.6	-8-1	9-5-	0.6-	-0.5	2.0	3.2	4.5	5.7	7.0	8.2	5.6	10.7	12.0	13.2	14.5	
	73.4	EMAX IMUM	PRESSURE	6.65	55.9	51.0	55.9	6.64	22.4	22.4	44.5	35.3	38.3	44.5	36.9	31.5	35.3	26.2	25.1	
	CHORD=	TANGENTIAL	(DFG.)	-14.2	-11.7	-9.1	9-9-	4.1	-1.6	-0-3	9.0	2.2	3.4	4.7	5.9	7.2	4.8	4.4	10.9	
	47.5	EHAXIMUM	PRESSURE	25.1	19.9	31.5	50.1	50.1	19.9	7.8	22.4	22.4	31.5	39.8	31.5	35.3	5.9	19.9	19.9	1
	ä	TANGENTIAL																		
	34.6	EMAXIMUM	PRESSURE	44.7	15.9	11.2	44°1	56.4	44.1	14.1	6.6	15.9	22.4	39.8	35.5	34.3	39.8	44.7	19.9	
	X CHORD=	R TANGENTIAL	(OFG.)	-19.5	-17.1	-14.6	-12.1	9.6-	-7.1	-5.8	9.4-	-3.3	-2.1	و. د	7. 0	1.7	5.9	4.2	5.4	•
	SAMPLE	NUMBER		-	7	٣	4	S	•0	^	e n	٠	10						16	

TABLE 0-41

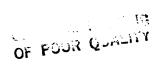
RECORD 105 WALL KULITE NONSTEADY PRESSURE PHASE TO STRAIN GAGE 3

PAGE 1

22.22	PHASE	(DEG.)	162.0	124.0	198.0	252.0	276.0	347.0	180.0	3(14.0	124.0	315.0	351.0	279.0	324.0	306.0	279.0	345.0	0°0
# CHORD=	TANGENTIAL	(DEG.)	-21.5	-19.0	-16.5	-14.)	-11.5	0.6-	-7.7	-6.5	-5.2	-3.9	-2.7	-1.4	-0-2	7.7	2.3	3.6	6.4
4.6	PHASE	(DEG.)	163.0	0.66	158.0	225 •0	270.0	248.0	208.0	36.0	18.0	18.0	279.0	333.0	0.0	306.0	279.0	270.0	72.0
₹ CHORD=	TANGENTIAL	(066.)	-23.2	L-02-	-18.2	-15.7	-13.1	-11.9	4.6-	-8-1	6.9-	9-6-	4.4-	-3.1	-1.9	9.0-	900	1.9	3.1
													_						81.0
# CHORD=	TANGENTIAL	(056.)	-25.2	-22.7	-20-1	-17.6	-15.1	-12.6	4.1	-10-	6 6 6	-7-6	4.9-	-5.1	-3-8	-2.6	-1 -3		1.2
																			306.0
CHORD#	TANGENTIAL	(DFG.)	-26.7	-24-2	-21.7	1 01-	-14.4	7 7 7	-12.0	4-11-	\$ - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -		8-1-	4	- C	1.7-	A . C -	90	-0.3
-55.4	PHASE	(DEG.)	20.00	7 7 2		20077	7	45.0	7 4	200	144 0	20 4 6	216.0	236.0	225.0	250.0	279.3	0.075	207.0
# CHORD#	TANGENTIAL	() ()	-22.5	(VE -	- FC		3 661	0 00		7 7 7		7071	- F - F - I	7 2 1	-11-	0	` •	7.6-	 •
9	MARKE		-	٦,	۰, ۲	n •	• 4	n 4	o r	- 0	υq	•) <u>-</u>	: <u>:</u>					17

RECORD 105 WALL KULITE NONSTEADY PRESSURE PHASE TO STRAIN GAGE 3

141.4	PHASE	(DEG.)	292.0	315.0	324.0	359.0	0.1	21.0	36.0	36.0	47.3	24.0	85.0	45.0	0.06	94.0	0.02	108.0	0.801	
CHORD=	TANGENTIAL	(DEC.)	w• †	-2.0	Ç.5	3.0	5.5	ο°3	9.3	10.5	11.8	13.1	14.3	15.6	16.8	18.1	19.3	20.6	21.8	3 • 1 9
66.3	PHASE	(056.)	270.0	279.0	288.0	297.0	315.0	351.0	351.0	355.0	C-3	9. 0	0.6	18.0	36.0	54.0	91.0	0.06	2	•
₹ CHORD=	TANGENTIAL	(DEG.)	-10.6	-8-1	-5.6	-3.0	-0.5	2 - ر	3.2	4.5	5.7	7.0	6.2	9.5	16.7	12.	13.2	14.5	L	1.01
73.4	PHA SE	(DEG.)	243.0	270.0	270-3	243.0	287.0	324.0	324.0	324.0	333.0	342.0	0.0	9 ° 6	0.6	27.0	55.0	6.06		D. CO
CHORD=	TANGENTIAL	(DEC.)	-14.2	-11.7	-9.1	9-9-	1.4.1	-1.6	-0-3	6°0	2,2	3.4	4.7	5.9	7.2	8.4	7.6	10.9		7.71
47.5	HS WEG	(050)	199.0	736.0	243.0	275.0	289.0	225.0	333.0	288.0	306.0	315.0	333.0	342.0	351.0	342.0	315.0	23.0		0./2
Z CHORDE	TANGENTIAL	(DEG.)	-17.9	-15-4	-12.9	-16.4	-7.9	-5.4	-4-1	6-2-	9-1-	4-0-	0	2.2	3.6	4.7	5.9	7.7	•	7.
		COFG																		
ECOURT &	TANGENTIAL	(1)66.1	-19.6	-17.1	-14-6	-12-1	9.01	-7-1	4 · 6 · 1	4		-2.1	4 6	•	1.7	2.0	(· ·	7 4		6.7
0 1077	MIMBED	4 1000	-	۰ ۸	i fr	٠ ٦	٠ ٧٠	۰.۰	۰, ۲	- α	• •	` [2 =			7				



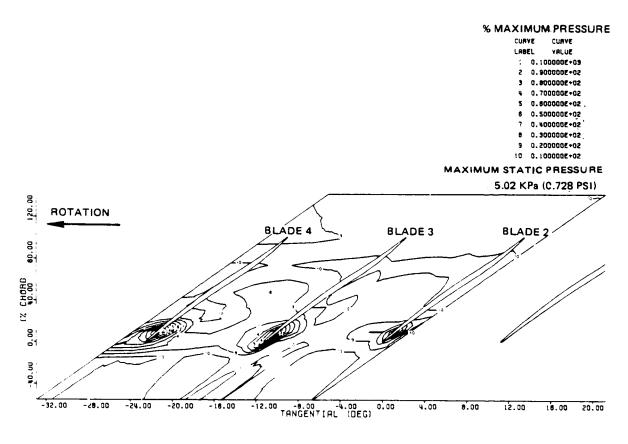


Figure D-28 Nonsteady Pressure Contours at Blade Tip; In Flutter, High Operating Line, 73 Percent Speed, 60 Percent Flow, Pressure Ratio 1.3317

C. (c)

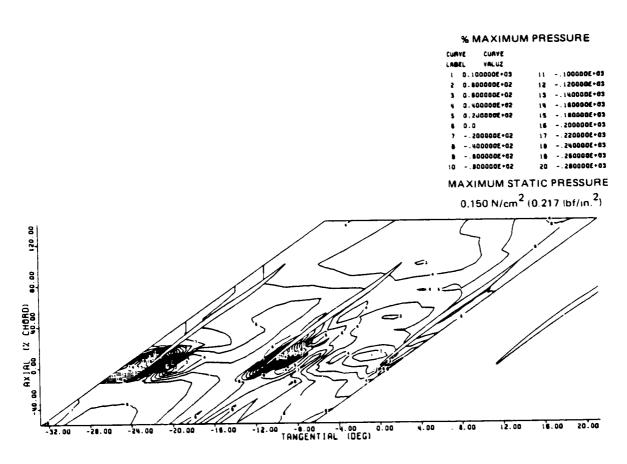
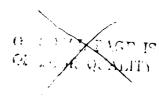


Figure D-29 Nonsteady Real Pressure Contours at Blade Tip; In Flutter, High Operating Line, 73 Percent Speed





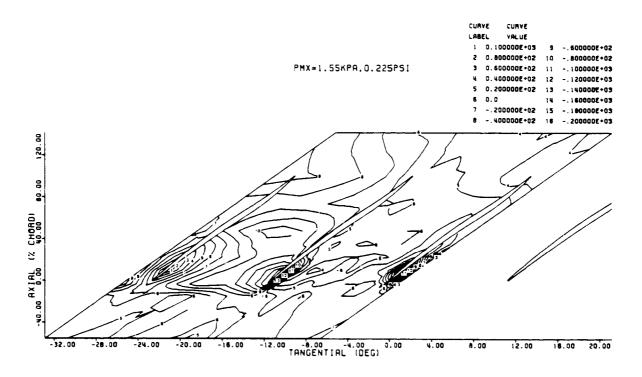


Figure D-30 Nonsteady Imaginary Pressure Contours at Blade Tip; In Flutter, High Operating Line, 73 Percent Speed

RECORD 199 WALL KULITE NONSTEADY PRESSURE AMPLITUDES MAXIMUM PRESSURE SAMPLED # 3.15 KILOPASCALS # 6.457 PSI

		•	٠.																					•	•		٠.
		•	,	_																							31.7
	T CHORDS	TANGENTIAL	1067	1000	-21.9	7.01-		¥-10-4	-14.4	A 11-		***	187		٨٠٥-	-5.6		3.5	-3.2	6-1-		7.9	9•0	•	N • • • • • • • • • • • • • • • • • • •	3.1	4.4
121	40	THAXIMUM	DDECCIOE	2000	78.2	89.1		•	17.7	25.2		2	100.0	. 77		14.2	75.3	7.67	14.2	28.2		7.41	23.2	0.19		2.00	79.4
101 10110 1 03	# CHORD=	M TANGENTIAL	(056.)		-63.1	-21.2	-18 7		-16.2	-13.7	-11	7 1 1 0 5	6.6-	6	- 1	200	-47	7.0	0.5-	-3.7		c• >-	-1.2	0-0		F • =	2.4
י יייייייייייייייייייייייייייייייייייי	-3.6	EMAXIMUM	PRESCURE			38.9	10		24.5	26.9	7 7 7 2	7	38.4	0.4.		15.5	10.0		17.3	0°0	7	2	24.5	15.5	90		1.69
	# CHORD=	TANGENTIAL	(DEG.)	1 4 6	0.0	-23.0	-20.5		0-81-	-15.6	-1 4-1		-11.8	-16.5		-4-3	-8-0		20.0	-5.5	F-4-	7 .	-3.1	-1.8	4 0		0.7
	-15.1	#MAXIMUM	PRESSURE	14.2	3.07	17.3	7.4	9	7-17	15.5	25.6	, ,	42.6	24.5	4 4	10.0	17.3		617	15.5	10.9		2	15.5	27.6		2109
	# CHORD=	TANGENTIAL	(DEG.)	-27.2	4 f	1.47-	-22.1	- 10 J		-17.2	-14.7	7	4.61	-12.2	9 311	10.01	-9.6	7 0 1	* (-1.2	-5.9	. , , ,		10.4	-2.3		ו01
	= -55.4	EMAXIMUM	PRESSURE	12.5	֓֡֜֝֜֜֝֓֜֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֓֡֓֓֓֓֓֡֓֜֓֡֓֡֓֡֓֡	:	36.3	3.46	•	, x	2.2	-	1.7	21.9	17.3		27.0	12.0		C**7	0°0	2 4) u	0.0	60 60	, ,	t •
		<u>ب</u>	(DFG.)																								
	SAMPLE	NUMBER		_	•	•	m	4	u	•	٥	•	- (20	ø	•	c. ₹		: :	71	13	7 (7	16	17	•

RECORD 199 WALL KULITE NONSTEADY PRESSURE AMPLITUDES
MAXIMUM PRESSURE SAMPLED = 3.15 KILOPASCALS = 0.457 PSI

	7 171	ZMAXIMIM		PRES SURE	77.2	0 07		0	0.54	5,6.0		V.V.	7. 77		1.76	44.4	3 17		35.2	25.2	40.6		0.7	39.6	0 7 3	4.1.7	ر من تاو
	# CHORGE	UM TANGENTIAL	1066	1.000	-5-1	-2.6			7.7	6.4	, ,	*:	F - 3	; o		11.2	12.4		33.0	14.9	16.1	, ,	F	14.0	2		21.2
Z	66	ZHAXIH	PRESCH		2/5	35.2	45.0		13.6	31.5	2 8 6		24.9	28.0		31.5	31.5		9.0	36.3	22.3	000	•	54.9	24.9		23.9
Jest Michaella = 0.457 FSI	CHORD=	M TANGENTIAL	(DFG.)		0.11-	-8.5	0-9-		0.00	J. C	_		2.7	4.0	• 1	2.6	6.5			0.6	16.2	11 4	•	12.7	14.0	, (7.01
N 1 L U N N 2 C N	73.4	EMAX IMU	PRES SUR	26.3	7.00	23.9	35.2	26.0	7	35.2	18.6		6.61	31.5		6.02	32.2	0.76		31.5	54.9	10.0		14.0	20.8		-
}	# CHORD≈	TANGENTIAL	(DEG.)	-14 7		-12.2	-6-J	-7-2	4 I	1.5	-2.2		7.51	o•3		0:1	2 . 8	4.1		5.3	۲.5	7.8		9.1	10.3	7	0.11
	47.5	ZMAXIMU	PRESSUR	74.5	•	0.	17.3	34.6		33.	34.6		Y = 2 T	22.3	21.0	2 . 4 . 7	24.5	27.6		n (19.5	30.9		6.12	17.3	3 70	7
	CHORD=	TANGENTIAL	(DEG.)	-18.3		8-61-	-13.3	-10.8		10.1	-5.8	* /-	3	-3.3	-2-1	* (6.1	4.0		- (6.7	4-2	``		6.7	7 0	•
	34.6	ZHAXIN	PRESSURE	43.5		0 • 0 1	17.3	33.1	7 9 6	0 1	30.6	26.5	•	12.3	17.3		0 · c	16.6	210		3.0	3°02	3.70	6.	6.3	14.7	
	# CHORD=	INGENTIAL	1066.1	-20.5	7 21-		2.61-	-:2.6	2-61-	7 1	1.1-	79-		7.6-	-3.9		1 . 3 -	-1.4	1,0-			2.3	7-1	9 •	æ	6.1	•
	SAMPLE	NOTHER	•		•	u 1	n	*	6	١.	٥	~		י מ	•	•		1	12		2 :	<u>*</u>	~		0		•

TABLE D-43 record 199 wall kulite nonsteady pressure phase to strain gage 3

22.2 100.2 1144.0 1144.0 1144.0 1135.0 234.0 234.0 234.0 237.0 276.0 276.0 276.0	148.4 100.6 10
#ANGENTIAL LINES - 1 1 1 4 - 4 4 4 4 4 4 4 4 4 4 4 4 4 4	TANCENTIAL (DEG.) -5.1 -5.1 -2.6 -2.6 -2.6 -2.6 11.2 11.2 11.2 11.2 11.2 11.2 11.2
9.4 PHASE (DEG.) 180.0 1144.0 225.0 225.0 225.0 225.0 225.0 225.0 333.0 270.0 81.0	
# CHORD= TANGENTIAL (DEG.) -23-7 -23-7 -13-7 -13-7 -13-7 -13-7 -13-7 -13-7 -13-7 -13-7 -13-7 -13-7 -13-7 -13-7 -13-7 -13-7 -13-7 -23-7 -2-5 -2-5 -2-5 -2-5 -1-2 -1-2 -1-2 -1-2	►
MANUAL CO. C.	74 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
TANGENTIAL POFES, 1 1-25.6 1 1-25.6 1 1-20.5 1 1	# CHORD= TANGENTIAL (DEG.) -14.7 -12.2 -9.7 -7.2 -6.9 (C.3 1.6 5.3 6.5 1.6 6.5 1.6 1.6 1.6 1.6 1.6
-15.1 1066.) 1086.1 1086.1 162.0 342.0 225.0 225.0 248.0 248.0 216.0 315.0 315.0	CHORD= 47.5
11111111111111111111111111111111111111	6 #0011111111111111111111111111111111111
255.4 PHASE (DEG.) 72.0 72.0 45.0 117.0 117.0 117.0 117.0 117.0 117.0 117.0 125.0 243.0 273.0 273.0	RECORD 34.6 PHASE (DEG.) 191.0 99.0 261.0 270.0 270.0 270.0 342.0 333.0 333.0 342.0
## CHORD= TANGENTIAL (DEG.) 120.3 120.3 120.4 120.6 120.6 110.6 110.6 100.3 100.3	### CHORD# TANGENTIAL TANGENTIAL DEG. -20.2 -17.7 -15.2 -17.7 -15.2 -2.7 -2
SAM NCAM NCAM 11 11 11 11 11 11 11 11 11 11 11 11 11	SAMPLE NUMBER 12 13 13 13 14 17

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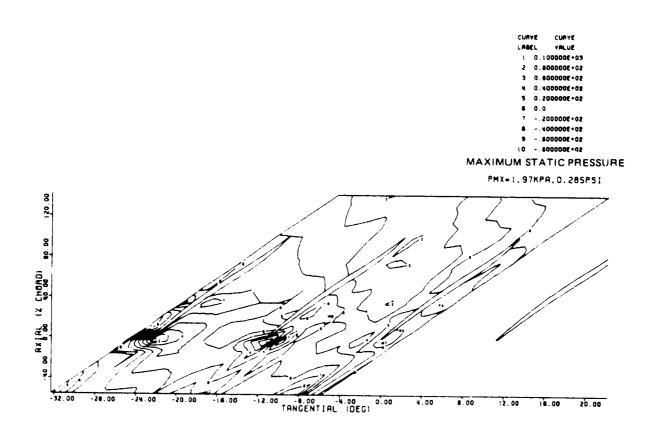


Figure D-31 Nonsteady Real Pressure Contours at Blade Tip; in Flutter, High Operating Line, 75 Percent Speed

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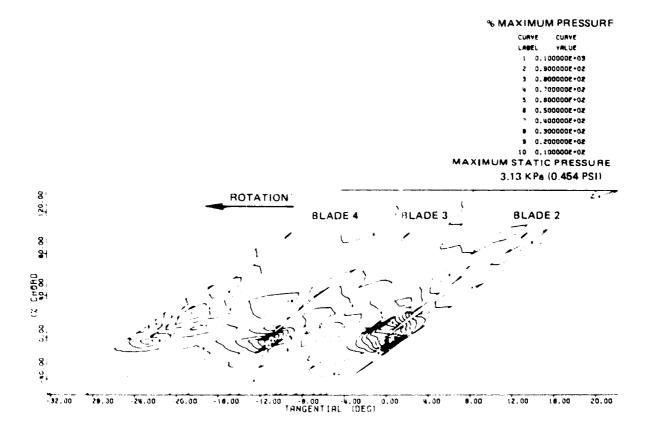


Figure D-32 Nonsteady Pressure Contours at Blade Tip; in Flutter, High Operating Line, 75 Percent Speed, 60.3 Percent Flow, Pressure Ratio 1.3369

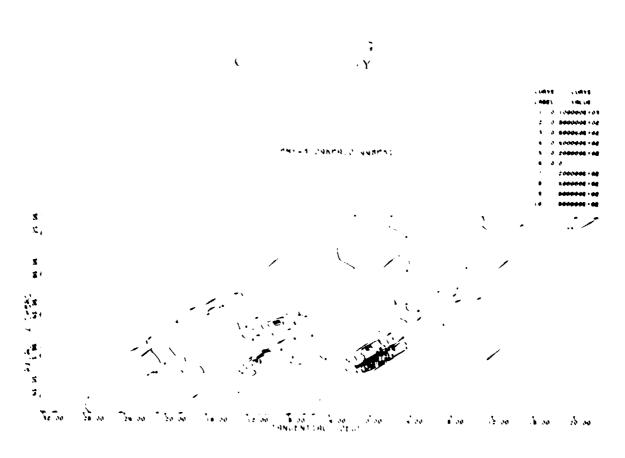
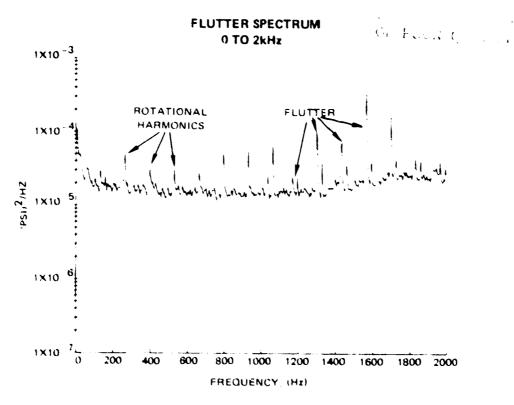


Figure 0-33 Nonsteady Imaginary Pressure Contours at Blade Tip; In Flutter, High Operating Line, 75 Percent Speed



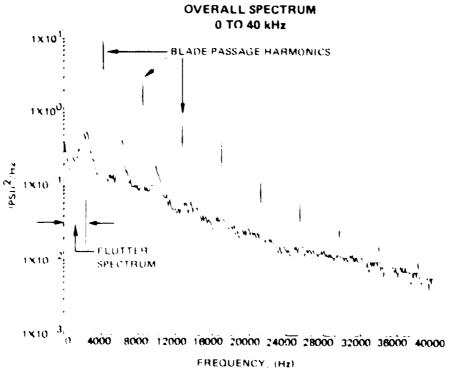
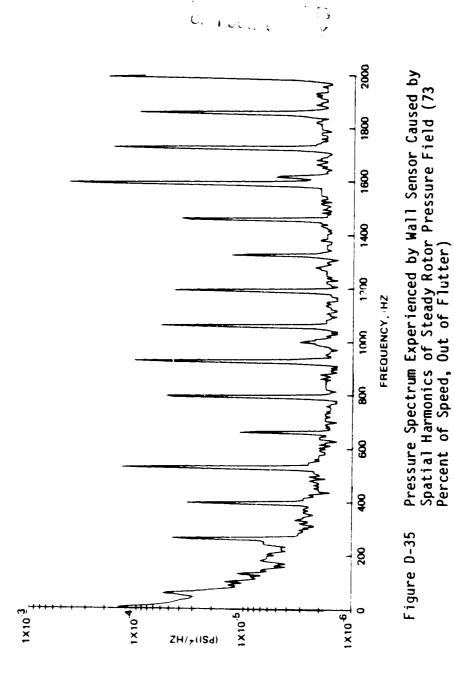
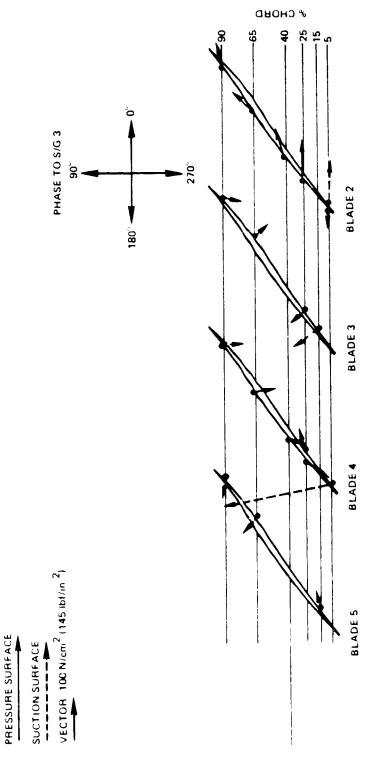
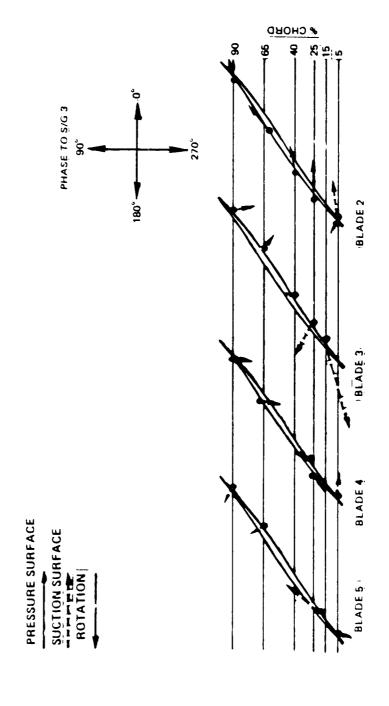


Figure D-34 Spectra of Vibratory Wall Pressure Showing Relationship of Flutter Frequencies to Harmonics of Rotor Steady Pressure Field

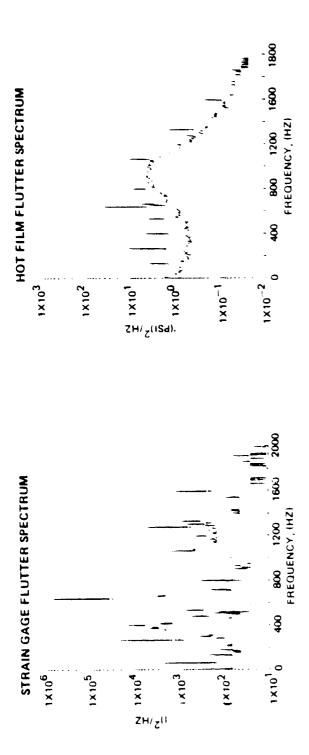


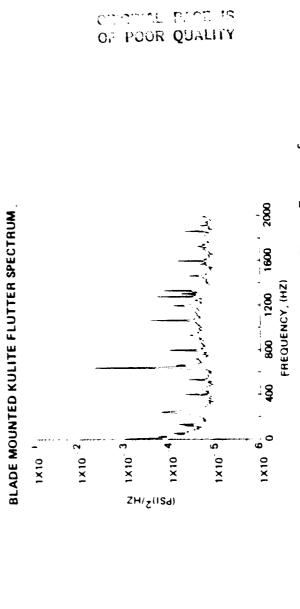


Local Oscillating Pressures on Blade Surfaces at 67 Percent Speed (Vector Plot of Real Versus Imaginary With Origin on Point of Application) Figure D-36



Local Oscillating Pressures on Blade Surfaces at 73 Percent Speed (Vector Plot of Real Versus Imaginary With Origin on Point of Application) Figure D-37





Comparison of Flutter Spectra From Three Types of Sensors on Same Blade; 73 Percent Speed, 638 Hz Flutter Frequency Figure 0-38

294

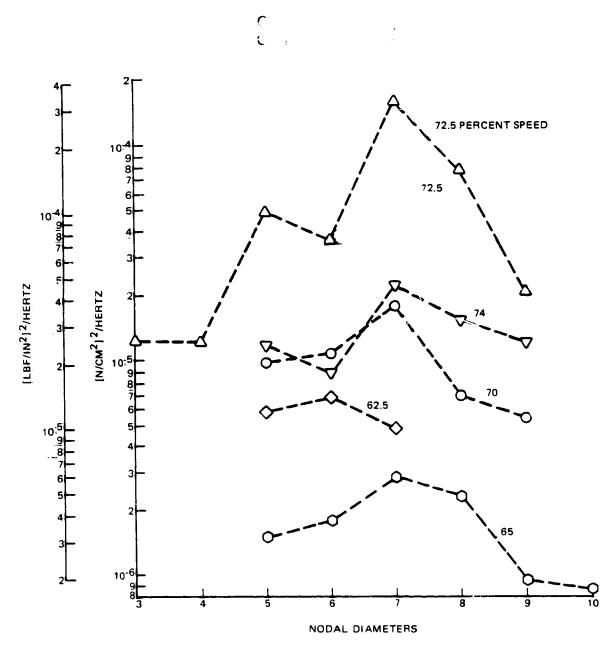


Figure D-39 Spectral Comparison of Vibratory Rotor Pressure
Amplitudes in Terms of Distribution Among Spatial
Harmonics (Stationary Sensor Over Path of Blade Trailing Edge)

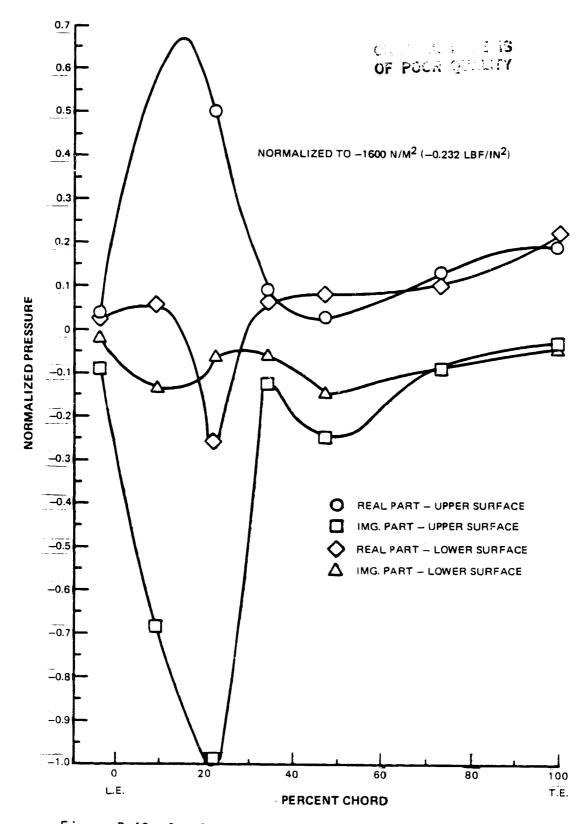


Figure D-40 Complex Pressures Used in Damping Calculations, Five Nodal Diameters

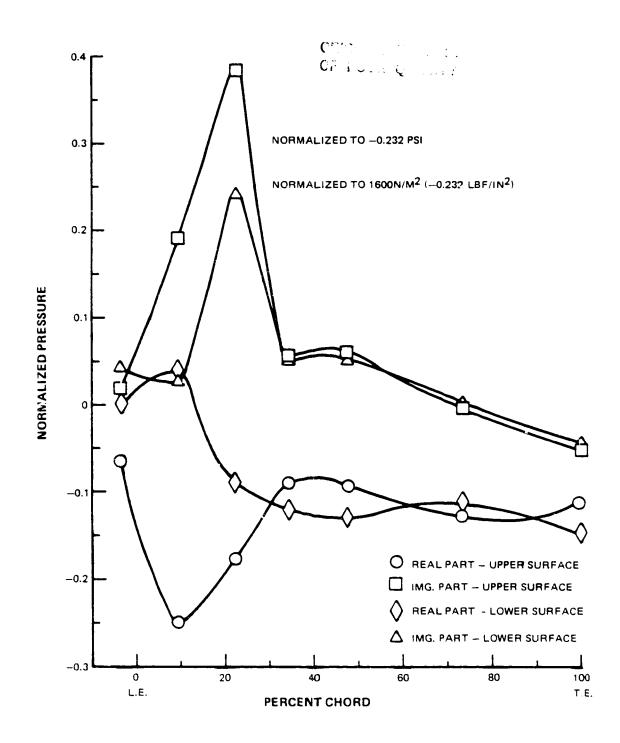


Figure D-41 Complex Pressures Used in Damping Calculations, Seven Nodal Diameters



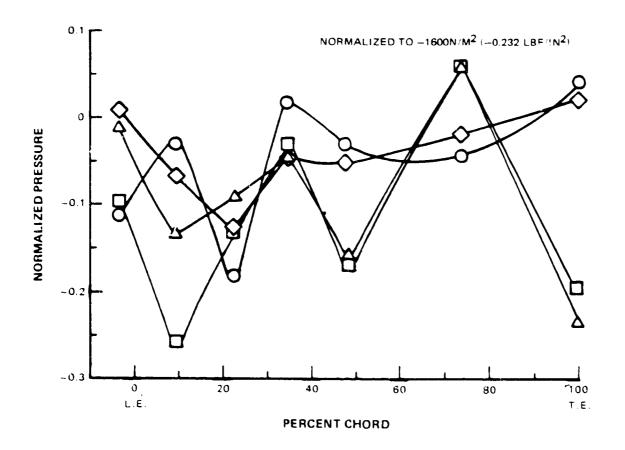


Figure D-42 Complex Pressures Used in Damping Calculations, Nine Nodal Diameters

APPENDIX E HOT FILM DATA

TABLE E-1
BLADE MOUNTED HOT FILMS
(Amplitude and Phase)

	Position (Percent		66% Spe	ed	73% Spe	ചർ	75% Speed				
<u>Blade</u>	Chord)	Surface	Amplitude	Phase	Amp lituue	Phase	Amplitude	Phase			
20	5	concave	1.0	252	1.0						
	40		1.0	317	0.37	255 359	-	267 314			
	5	convex	0.11	186	0.55	359	0.41				
	40		0.13	1 34	0.14	134	0.42	134 141			
21	5	convex	-	-	•	_					
	15		0.03	150	0.10	127	0.03	147			
	25		0.28	114	1.0	96	0.28	147			
	40		1.0	80	_	104	1.0	114			
	05		0.35	68	0.17	146	0.35	137			
	90		0.65	207	0.18	135	0.33	138			
22	5	concave	1.0	83	1.0	49	1.0	vo.			
	40		0.07	293	0.31	234	0.22	90			
	5	convex	-	173	-	45	-	105 16			
	40		0.08	94	0.17	104	0.25	υ5			
23	5	convex	0.65	166	0.7	339	0.28	67			
	15		0.44	329	0.31	95	1.0	179			
	25		0.07	38	1.0	307	0.81	48			
	40		1.0	239	0.26	297	0.00	48 48			
	05		0.62	327	0.17	31	0.50	352			
	90		0.98	103	0.28	36	0.00	285			

Phase is relative to strain gage on blade 3.

Amplitude is ratio to local maximum for each blade.



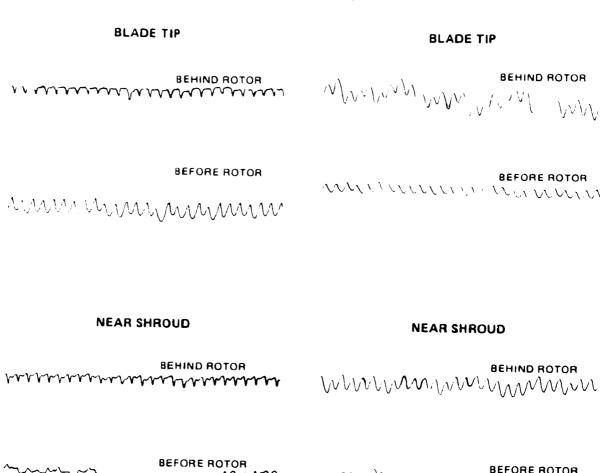








Figure E-1 Signal Enhanced Wave Forms of Hot Film Probes at 73 Percent Speed (Noncalibrated Amplitudes)

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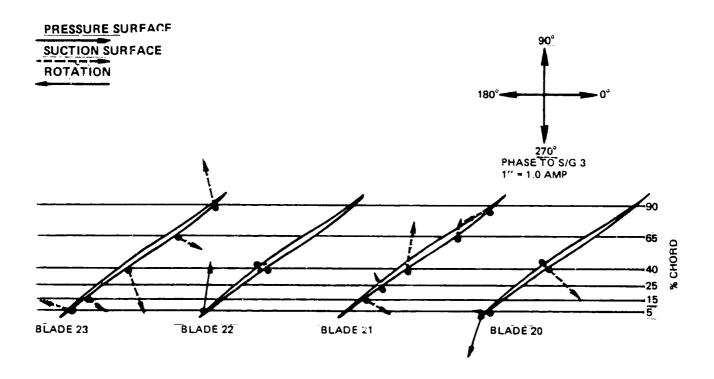
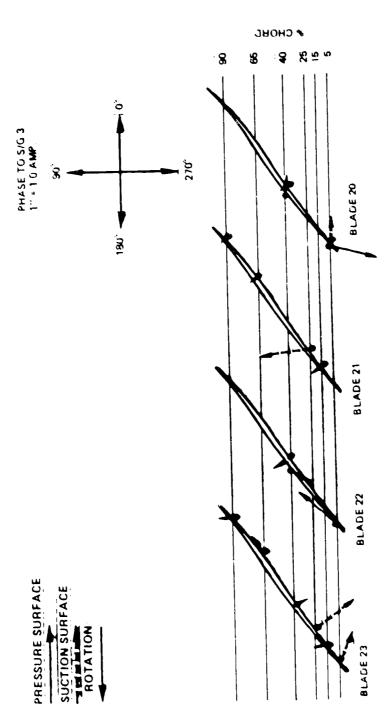


Figure E-2 Local Oscillating Hot Film Signals on Blade Surfaces at 67 Percent Speed (Vector Plot of Real Versus Imaginary With Origin on the Point of Application)



Local Oscillating Hot Film Signals on Blade Surfaces at 72 Percent Speed (Vector Plot of Real Versus Imaginary With Origin on the Point of Application) Figure E-3

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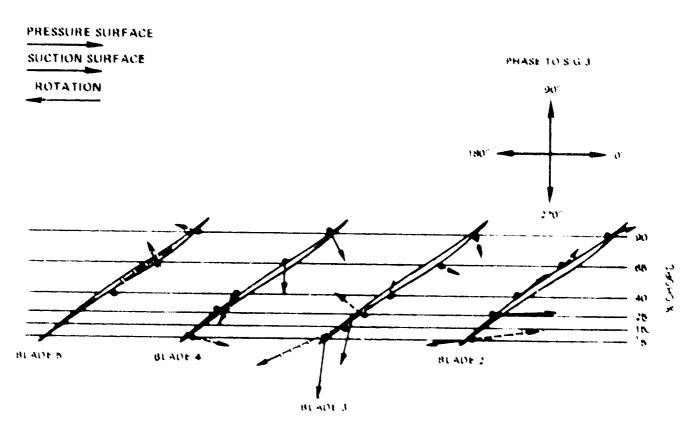
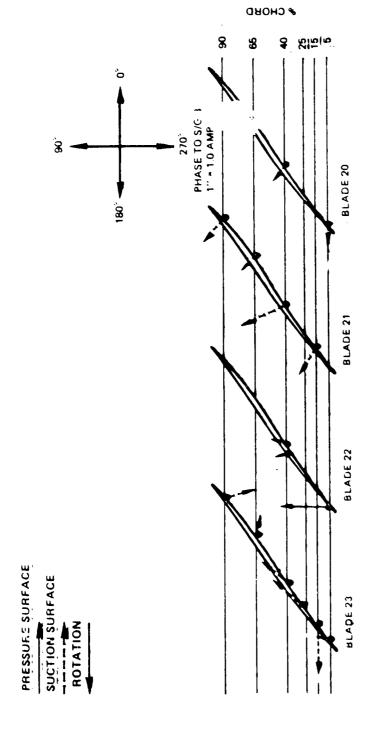


Figure E-4 Local Oscillating Hot Film Signals on Blade Surface at 75 Percent Speed Shown as Vectors (Vector Plot of Real Versus Imaginary With Origin on Point of Application)



Local Oscillating Velocities on Blade Surfaces at 75 Percent Speed (Vector Plot of Real Versus Imaginary With Origin on the Point of Application) Figure E-5